TECHNICAL MEMORANDUM – EXISTING TRAFFIC CONDITIONS US 101 / MAIN STREET INTERCHANGE

| Date: | July 1, 2011 | | |
|---------------|--|----------------|----------------------|
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| Subject: | Summary of traffic conditions with existing | traffic volume | s at the US 101 / Ma |

- Subject: Summary of traffic conditions with existing traffic volumes at the US 101 / Main Street interchange, in San Luis Obispo County. Memorandum includes the following:
 - 1.) Introduction
 - 2.) Site description
 - 3.) Existing geometric conditions
 - 4.) AM and PM Level of Service analysis
 - 5.) Queuing Analysis
 - 6.) Review of historical accident data
 - 7.) Evaluation of proposed short-term mitigation measures





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1.0 INTRODUCTION

As requested by the County of San Luis Obispo, Rick Engineering Company (RICK) has prepared this technical memorandum analyzing the existing traffic conditions at the US 101 / Main Street Interchange in the Templeton Community of unincorporated San Luis Obispo County. **Exhibit 1** shows a vicinity map with the study interchange and the surrounding roadway network system.

This technical memorandum has been initiated by the County of San Luis Obispo in response to the findings of several area circulation studies that have identified the US 101 / Main Street interchange as failing to meet Caltrans and the County of San Luis Obispo "Level of Service" (LOS) standards, both under existing conditions and future build-out conditions.

These studies, which will be referenced in this memorandum as supporting documents and for background information, include the following:

- 1. Templeton Circulation Study, 2009 Comprehensive Update (Omni-Means, Ltd.)
- 2. Project Study Report for Main Street / SR 101 Interchange, dated November, 2006 (California Department of Transportation)

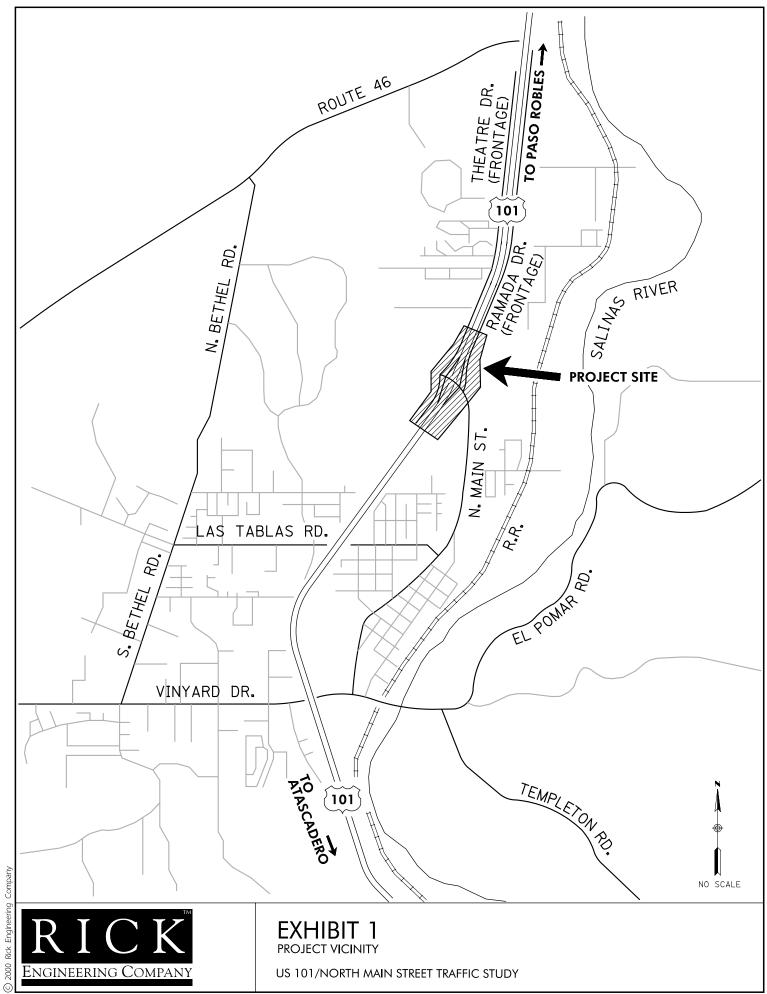
However, while the County has recognized that this interchange is currently problematic with regard to area traffic flow, the various studies listed above have differed in their conclusions as to the extent of the congestion. This memorandum utilizes the most recent traffic count data and the current geometric layout to quantify the existing traffic conditions. The evaluation of existing conditions includes an analysis of LOS, accident rates, and vehicle queues at the four (4) study intersections. Several proposed short-term mitigation measures are also analyzed to determine whether they would noticeably impact traffic flow in either a positive or negative manner.

2.0 EXISTING ROADWAY NETWORK

The following is a brief description of the local roadway network within the project study area.

<u>US 101</u> is a north-south freeway in the project area with two lanes in each direction, a divided median and a posted speed limit of 65 miles per hour (mph). Access between US 101 and Main Street is provided via northbound and southbound on- and off-ramps. The north and southbound off-ramps are stop sign controlled at Main Street.

<u>Main Street</u> is a north-south arterial through the Templeton community. Main Street parallels US 101 and serves the local downtown commercial areas. Main Street has more of an east-west alignment near the US 101 interchange. The existing bridge over US 101 has a single lane in each direction, with a roadway width of approximately 30' and a 5' wide sidewalk on the south side. Main Street also provides access to Ramada Drive and Theatre Drive. West of Theatre Drive, Main Street narrows and serves as an access road for a local lumberyard, the Caltrans maintenance station, and a private residence. Main Street has a posted speed limit of 45 mph south of the US 101 interchange.



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<u>Theatre Drive</u> is a north-south collector road that serves as a frontage road along the west side of US 101. As noted in previous studies, due to congestion at the US 101 / State Route (SR) 46 West interchange (next interchange to the north) many drivers use the US 101 / Main Street interchange and Theatre Drive to access the local residential and commercial uses on the west side of US 101. Theatre Drive has a posted speed limit of 45 mph north of Main Street. South of Main Street, Theatre Drive provides access for a local lumberyard and residences. Theater Drive terminates approximately 800 feet south of Main Street. Future plans include extending Theatre Drive to the south to connect with Las Tablas Road. Currently, the four-legged intersection of Theatre Drive and Main Street has three-way stop sign control, with free traffic movements allowed for westbound traffic on Main Street.

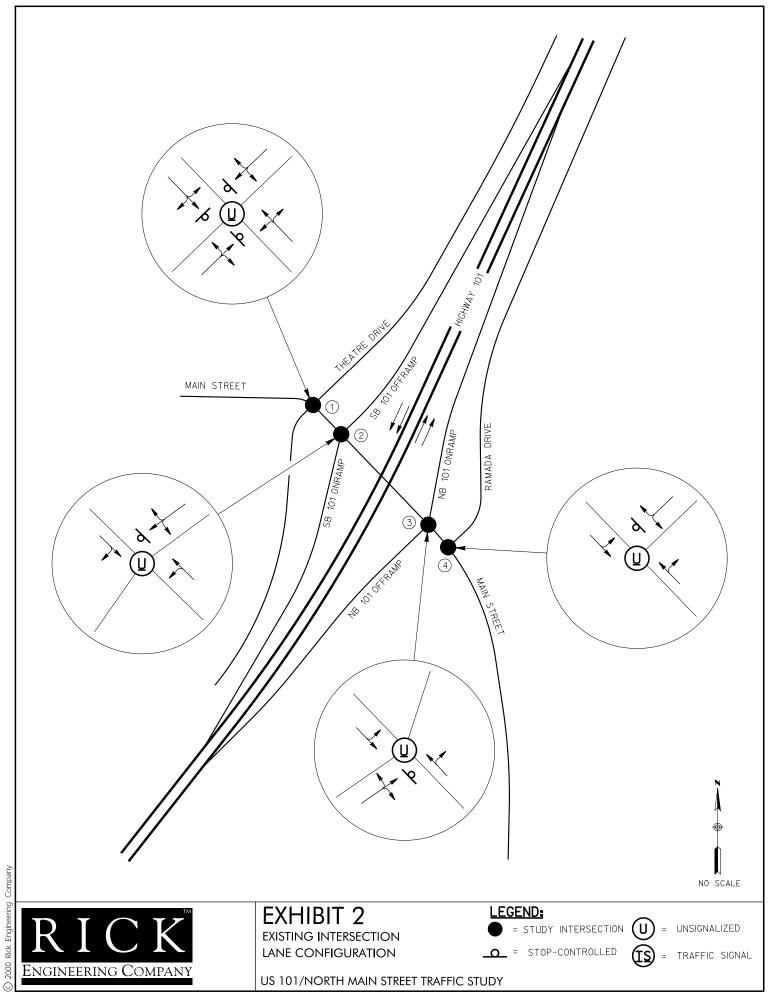
Discussions with Caltrans staff indicated that to the north, Theatre Drive south of SR 46 West is currently under construction. This project will close the portion of Theatre Drive between SR 46 West (opposite Vine Street) and Alexa Court (access road for Hampton Inn and La Bellasera Hotel). Traffic on Theatre Drive with a destination to SR 46 West will be re-routed to Gahan Place. This construction project also includes the installation of traffic signal control at the SR 46 West and Gahan Place intersection.

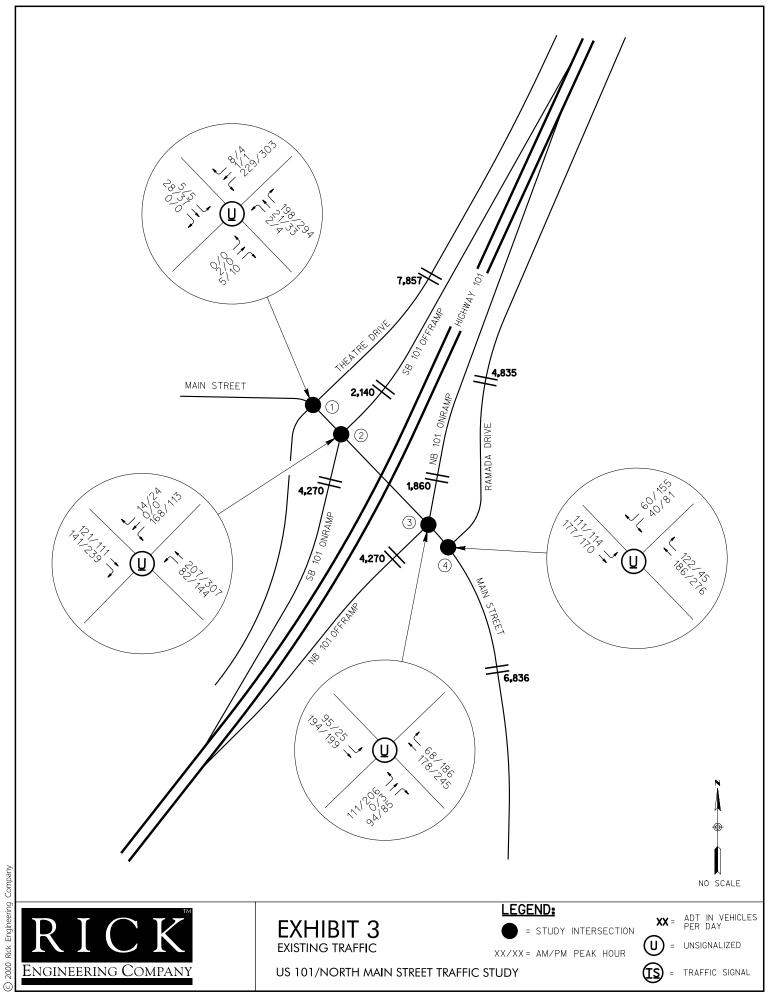
<u>Ramada Drive</u> is a north-south collector road with a single travel lane in each direction. Ramada Drive serves as a frontage road along the east side of US 101. Main Street is the southern terminus of Ramada Drive, with a mix of commercial, industrial and agricultural developments to the north. Ramada Drive also provides access to the US 101 / SR 46 West interchange. The posted speed limit on Ramada Drive is 45 mph in the vicinity of the project site. Currently, the three-legged intersection of Ramada Drive and Main Street is stop controlled only at Ramada Drive, with free traffic movements allowed for east and westbound traffic on Main Street.

Exhibit 2 shows the existing intersection lane configurations of the study intersections. It should be noted that the northbound approach on Theatre Drive, the US 101 southbound and northbound off-ramps, and the southbound approach on Ramada Drive are flared at their intersection with Main Street. This widening of the approach effectively creates a short separate lane for vehicles making right turns from the cross street provided that the queue for the left turn and through movements (shared lane) is not backed up beyond the limits of the flare (approximately 50').

3.0 EXISTING TRAFFIC VOLUMES

Existing morning (7:00-9:00 AM) and afternoon (3:00-6:00 PM) peak period turning movement traffic count data was collected at the 4 study intersections by Metro Traffic Data, on September 16, 2009. The traffic count data was analyzed on both sides of US 101 to balance the volumes and determine the common peak periods for the 4 study intersections. Average daily traffic (ADT) for Main Street, Ramada Drive and Theatre Drive near the project area was obtained from County traffic count data (September 2009). ADT on each of the four (4) freeway ramps was obtained from Caltrans published ramp data (2007). Segment ADT are shown as part of this memorandum for informational purposes only. **Exhibit 3** shows the existing peak hour turning movement volumes and ADTs in the project study area. **Appendix A** contains the traffic count data for the study intersections, as well as the roadways.





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4.0 INTERSECTION ANALYSIS METHODOLOGY

The analysis of existing peak hour operations at the 4 study intersections was performed using methodologies contained in the Highway Capacity Manual (HCM2000), and modeled with the "Synchro" and "SimTraffic" software (Version 7). To accurately model existing operations the appropriate peak hour factor (PHF) adjustments were applied. The software estimates vehicle delays for the overall peak hour operations as an "average" and for each "critical" movement (i.e.: stop sign controlled approach, main line left-turns, etc).

It should be noted that the Main Street and Theatre Drive intersection is currently three-way stop sign controlled, which cannot be modeled correctly using Synchro. RICK determined that modeling the existing intersection as a two-way stop rather than an all-way stop would more closely approximate actual conditions. Since traffic westbound on Main Street currently flows freely, modeling this movement as stop-controlled would inaccurately estimate vehicle delays and queues. Eastbound traffic entering the intersection comprises a relatively small portion of the total intersection volume. In addition, conflicting movements between east and westbound traffic are minimal. Therefore, it was decided that a more accurate representation of actual operations would be obtained by utilizing the two-way stop controlled methodology.

As discussed in Section 2.0 (Existing Roadway Network), the northbound approach on Theatre Drive, the US 101 southbound and northbound off-ramps, and the southbound approach on Ramada Drive are flared at their intersection with Main Street. These flares essentially create a short separate lane that vehicles use to make right turns when the left-through movement queues do not backed up beyond the limits of the flare. Therefore, the analysis of these approaches assumes a single lane approach with a short 50' turn lane for right turn movements.

5.0 LEVEL OF SERVICE METHODOLOGY

5.1 Level of Service Ratings

LOS ratings are quantitative descriptions of intersection operations and are reported using an "A" through "F" letter rating system to describe vehicle delays and congestion. LOS A indicates freeflow conditions with little or no delay and LOS F indicates forced-flow conditions with excessive delays and queues. See **Table 1** for the LOS characteristics. **Appendix B** contains the HCM2000 tables illustrating the LOS-to-delay relationship data for intersection operations (i.e.: two-way stop controlled, all-way stop controlled and signalized intersections).

The peak hour LOS values for each intersection are based on the estimated "average" vehicle delays. The LOS values are also reported for the various critical movements (i.e.: stop sign approach, main line left-turns, etc.), which are based on the estimated delays for the individual approach and/or movement. Typically, Caltrans uses the "average" control delay for reporting an intersection Measure of Effectiveness (MOE). However, the LOS analyses performed for this technical memorandum utilize the lowest performing critical movement LOS for determining when improvements are warranted, consistent with County methodology used in the Templeton Circulation Study.

| TABLE 1 | | | | | | |
|----------------------------------|--|--|--|--|--|--|
| LEVEL OF SERVICE CHARACTERISTICS | | | | | | |

| LOS | Characteristics |
|-----|--|
| А | Free flow conditions exist. Each individual driver is virtually unaffected by the presence of others in the traffic stream. |
| В | Stable traffic flow exists. The individual drivers have the freedom to select a desired speed, but encounter a slight decline in the freedom to maneuver. |
| С | Stable and acceptable flow exists, but speed and maneuverability are somewhat restricted due to higher traffic volumes. The individual driver will be significantly affected by the presence of others. |
| D | High density but stable flow will occur. The individual driver will experience a generally poor level of comfort and convenience. Small increases in traffic flow will cause operational problems and restrict driver maneuverability. |
| Е | Speeds are low, but relatively uniform. The individual driver's ability to maneuver becomes extremely difficult with high frustration. The traffic volume on the road is near capacity. |
| F | Forced or breakdown flow has occurred. The individual driver is stopped for long periods due to congestion. |

Source: Highway Capacity Manual, Transportation Research Board (TRB), 2000 Edition.

5.2 Level of Service Standards

The County of San Luis Obispo has adopted LOS C threshold as the minimum standard for rural roadway operations and LOS D or better for roadways within the boundary of the Templeton Urban Reserve Line (URL). Since the US 101 / Main Street interchange is located within the URL, LOS D is the minimum acceptable standard for peak hour operations at the intersections of Main Street with Ramada Drive and Theatre Drive. For the two intersections of Main Street with the northbound and southbound US 101 ramps, this study uses the standards found in the Caltrans traffic study guidelines (Guide for the Preparation of Traffic Impact Studies, December 2002). These traffic guidelines state that Caltrans endeavors to maintain a target LOS at the transition between LOS C and D range. Therefore, at the intersection of Main Street with the two US 101 intersections, LOS C will be considered the minimum acceptable standard for peak hour operations.

6.0 EXISTING INTERSECTION OPERATIONS

6.1 Intersections Operations

The following 4 intersections were studied as part of this traffic analysis:

- 1) Main Street & Theatre Drive
- 2) Main Street & US 101 SB Ramps
- 3) Main Street & US 101 NB Ramps
- 4) Main Street & Ramada Drive

Table 2 summarizes the intersection LOS analysis under Existing Conditions.**Appendix C**contains the intersection LOS worksheets for Existing Conditions.

| Study Intersection | Critical | 2009 Existing Traffic | | |
|---|---|-----------------------|-----|--|
| | Movement Delay (Sec AM Peak (Avg.) 6.2 EB 1.2 NB 9.3 SB 12.4 PM Peak (Avg.) 7.0 EB 2.2 NB 8.8 SB 14.5 AM Peak (Avg.) 7.1 WB 2.8 SB 24.1 PM Peak (Avg.) 7.2 WB 4.1 SB 35.5 AM Peak (Avg.) 5.7 EB 3.2 NB 16.1 PM Peak (Avg.) 8.4 EB 1.1 NB 26.4 | Delay (Sec.) | LOS | |
| Main Street & Theatre Drive (TWSC) | AM Peak (Avg.) | 6.2 | А | |
| | EB | 1.2 | А | |
| | NB | 9.3 | А | |
| | SB | 12.4 | В | |
| | PM Peak (Avg.) | 7.0 | Α | |
| | EB | 2.2 | А | |
| | NB | 8.8 | А | |
| | SB | 14.5 | В | |
| Main Street & US 101 SB Ramps (TWSC) | | | | |
| | AM Peak (Avg.) | 7.1 | Α | |
| | WB | 2.8 | А | |
| | | 24.1 | С | |
| | PM Peak (Avg.) | 7.2 | Α | |
| | WB | 4.1 | А | |
| | SB | 35.5 | E | |
| Main Street & US 101 NB Ramps (TWSC) | | | | |
| | AM Peak (Avg.) | 5.7 | Α | |
| | EB | 3.2 | А | |
| | | | С | |
| | PM Peak (Avg.) | | Α | |
| | EB | 1.1 | А | |
| | NB | 26.4 | D | |
| Main Street & Ramada Drive (TWSC) | | | | |
| | AM Peak (Avg.) | 3.4 | Α | |
| | EB | 3.8 | А | |
| | SB | 12.8 | В | |
| | PM Peak (Avg.) | 5.5 | Α | |
| | EB | 4.0 | А | |
| V V Pold Data Popresents Total Average V | SB | 14.8 | В | |

TABLE 2EXISTING INTERSECTION LOS ANALYSIS

X.X – Bold Data Represents Total Average Vehicle Delays During the Peak Hour LOS = Level of Service; Average Delay in seconds.

TWSC = Two-Way Stop Controlled Intersection

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

The data in **Table 2** indicates that average vehicle delays at the 4 study intersections are currently within acceptable limits during the AM and PM peak hours (LOS C or better at the ramp intersections, and LOS D or better at the frontage road intersections). However, delays for the US 101 north and southbound off-ramps are within the LOS D-E range during the PM peak hour. While alternative traffic control measures may bring the LOS for the off-ramp movements up to minimum LOS standards, the overall functionality of the entire intersection may actually

decrease as a result (i.e.: average delays may increase). See Section 7 for analysis of traffic control mitigation measures.

Although the LOS values in **Table 2** are slightly different than the findings of the Templeton Circulation Study, the patterns of vehicle delays are consistent with their findings. Updated peak hour traffic counts, as well as small differences in how the geometrical street layout was drawn, slightly influenced the LOS results. In order to check the computed LOS, field observations were conducted during the PM peak hour on January 24, 2011, to verify estimated delay times and queue lengths. Both minor street delays and queue lengths observed were consistent with the findings summarized in **Table 2** and **Table 4**.

6.2 Collision Analysis

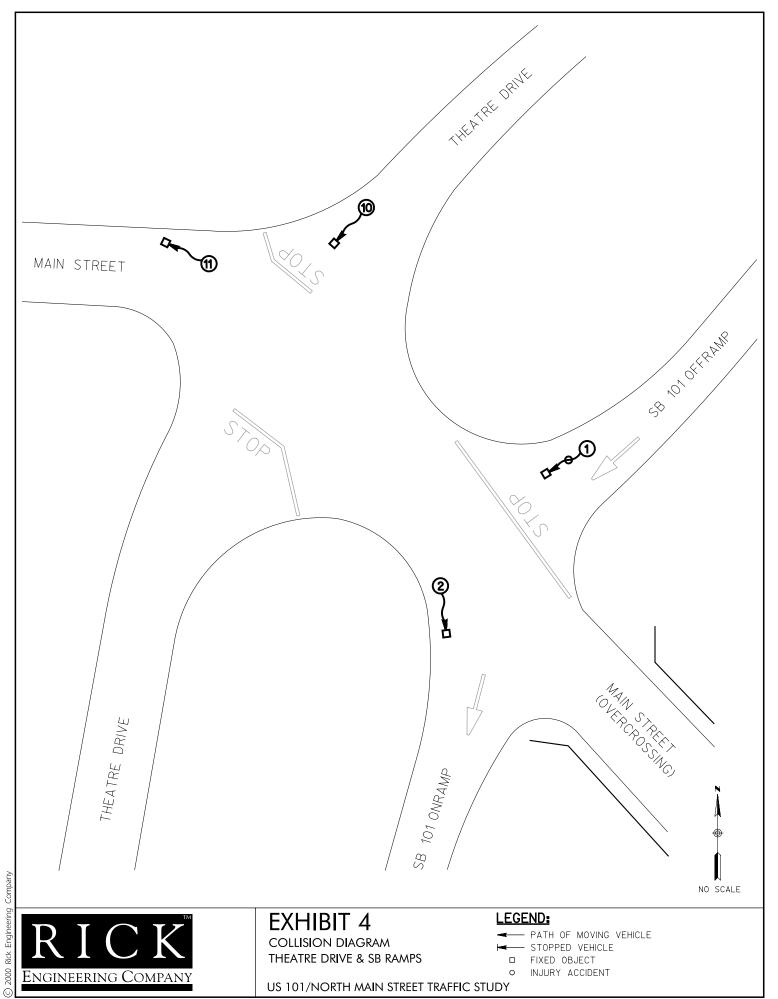
Traffic collision data for the project area was obtained from the County records and the Caltrans Traffic Accident Surveillance and Analysis System (TASAS). The compiled accident records, accident rate calculations, and Caltrans published Statewide average intersection accident rates are contained in **Appendix D**. The data has been reduced to the most recent three-year study period available, which occurred between January 1, 2007 and December 31, 2009. During the 3 year period for which data was provided there were a total of 16 reported accidents at the 4 study intersections, which are shown graphically on **Exhibit 4** and **Exhibit 5**. Of the 16 accidents, 3 of the accidents (19%) involved injuries, and the remaining 13 (81%) accidents were reported as Property Damage Only (PDO). None of the accidents involved fatalities. The 4 intersections had accident rates ranging from 0.18 to 0.56 accidents per million entering vehicles during the study period. For comparison purposes, the Statewide average rates for similar type intersections throughout the State of California, as reported by Caltrans, are also shown in **Table 3**.

| | No. of Accidents | | | Total MEV | Accident Rates | | | | | | |
|-----------------------------|------------------|------|------|--------------|----------------|------|--------------------|-------|-------|------|-------|
| Study Intersection | | | | | Existing | | Statewide Averages | | | | |
| | Total | Inj. | Fat. | F+I | NIL V | Fat. | F+I | Total | Fat. | F+I | Total |
| Main Street & Theatre Drive | 2 | 0 | 0 | 0 | 8.50 | 0.00 | 0.00 | 0.23 | 0.008 | 0.16 | 0.33 |
| Main St. & US101 SB Ramps | 2 | 1 | 0 | 1 | 11.11 | 0.00 | 0.09 | 0.18 | 0.008 | 0.16 | 0.33 |
| Main St. & US101 NB Ramps | 7 | 2 | 0 | 2 | 12.56 | 0.00 | 0.16 | 0.56 | 0.008 | 0.16 | 0.33 |
| Main Street & Ramada Drive | 5 | 0 | 0 | 0 | 9.55 | 0.00 | 0.00 | 0.52 | 0.004 | 0.10 | 0.22 |

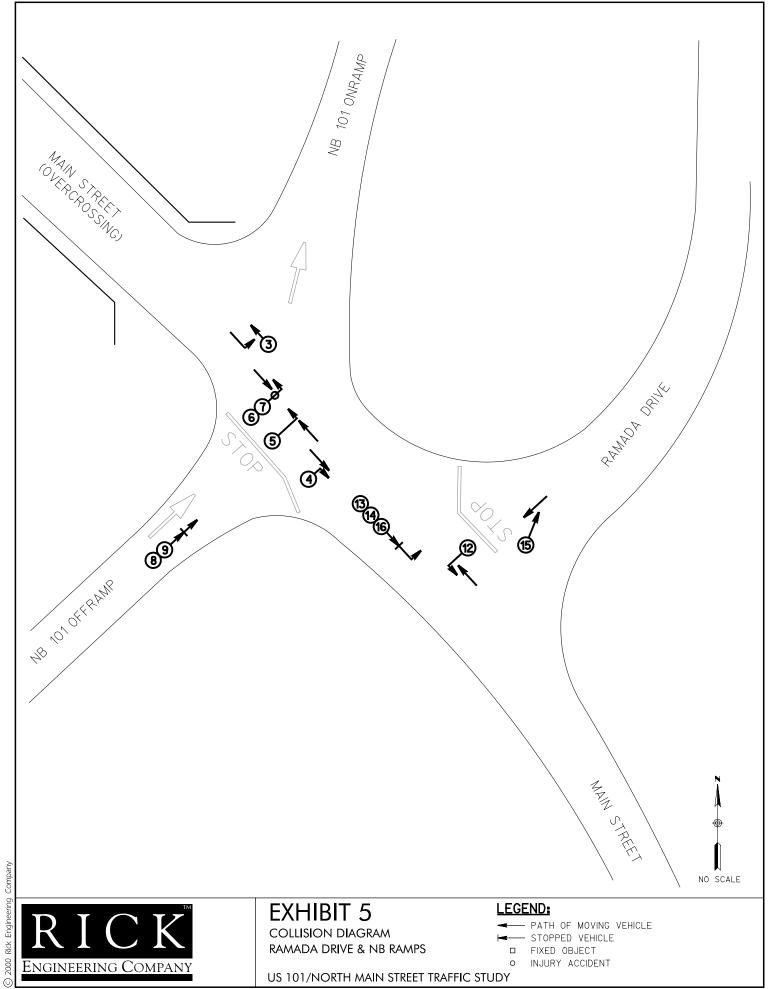
TABLE 3ACCIDENT RATE SUMMARY

As shown in **Table 3**, rates for accidents resulting in injuries and/or fatalities were lower than or equal to the Statewide averages at all 4 study intersections. However, the total accident rate at 2 of the study intersections are actually higher than the Statewide average. Of particular note, 7 of the 12 accidents occurring at the 2 intersections east of US 101 involved eastbound traffic on Main Street either colliding with traffic entering Main Street from the US 101 northbound offramp or rear-ending traffic waiting to turn left onto Ramada Drive. It is likely that this may be a result of eastbound drivers accelerating across the bridge in anticipation of the 45 mph speed limit on Main Street south of US 101.

It is suggested that mitigation measures be considered by the County to slow eastbound through traffic on Main Street until the vehicles have passed Ramada Drive. Several methods are available for slowing this traffic, including posting warning signage or by adding All-Way stop control or a signal at the NB 101 Ramps intersection. Additionally, lowering the posted speed limit may be a possibility, but would require a speed survey at this location demonstrating that observed 85th percentile traffic speeds would warrant this action. Please see Sections 7.3 and 8.3 for additional discussion regarding traffic control at this intersection, and **Appendix J** for recently completed speed surveys in the area.



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6.3 Queuing Analysis

To analyze queuing lengths under existing conditions, simulations were run using the SimTraffic software within SYNCHRO. The only modification made to the network was to lower the AM peak hour truck volumes on Ramada Drive in order to more accurately reflect observed field conditions. **Table 4** summarizes the intersection queuing analysis results under Existing Conditions and **Appendix H** contains the SimTraffic queuing data.

| Study Intersection | Critical Movement (Exist. PHV) | Existing Storage Length (feet) | 95th Percentile Queue Length (feet) | Storage Length Sufficient / Insufficient | |
|------------------------------------|-----------------------------------|--------------------------------------|---|--|--|
| Main Street & Theatre Drive (TWSC) | | | | | |
| | AM Peak | | | | |
| | NB LTR | - | 34 | Sufficient | |
| | SB LTR | - | 112 | Sufficient | |
| | PM Peak | | | | |
| | NB LTR | - | 24 | Sufficient | |
| | SB LTR | - | 103 | Sufficient | |
| Main Street & US 101 SB Ramps (TW | VSC) | | | | |
| | AM Peak | | | | |
| | WB LT | 335 | 335 66 | | |
| | SB LT | 1000 | 102 | Sufficient | |
| | PM Peak | | | | |
| | WB LT | 335 | 108 | Sufficient | |
| | SB LT | 1000 | 78 | Sufficient | |
| Main Street & US 101 NB Ramps (TW | VSC) | | | | |
| | AM Peak | | | | |
| | EB LT | 335 | 113 | Sufficient | |
| | NB LT | 800 | 98 | Sufficient | |
| | PM Peak | | | | |
| | EB LT | 335 | 56 | Sufficient | |
| | NB LT | 800 | 99 | Sufficient | |
| Main Street & Ramada Drive (TWSC) | | | | | |
| | AM Peak | | | | |
| | EB LT | 40¹ | 55 | Insufficient | |
| | SB L | - | 46 | Sufficient | |
| | PM Peak | | | | |
| | EB LT | 40 ¹ | 42 | Insufficient | |
| | SB L | - | 92 | Sufficient | |

TABLE 4

EXISTING INTERSECTION QUEUE ANALYSIS (CRITICAL MOVEMENTS)

¹Measured clear distance between adjacent intersections.

TWSC = Two-Way Stop Controlled Intersection

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

L = Left turn movement, T = Through movement, R = Right turn movement

All of the study intersections currently have adequate storage capacity for the 95th percentile queue length on all approach legs, except the eastbound lane on Main Street at the Ramada Drive intersection. On this approach, traffic waiting to turn left from Main Street to northbound Ramada Drive will occasionally block the northbound ramps intersection. The highest 95th percentile queuing values estimated were between approximately 100' and 120', or 4 to 5 cars in length. Field observation found these lengths to reflect actual conditions. All approach legs are adequate to accommodate generated queues, and as such, existing queue lengths do not necessitate roadway improvements at any of the 4 intersections.

7.0 INTERSECTION OPERATIONS WITH ALL-WAY STOP MITIGATION

As a part of this technical memorandum, an evaluation was conducted for the feasibility of utilizing all-way stop control as a short-term mitigation measure to alleviate traffic congestion at the US 101 / Main Street interchange and adjacent intersections. These measures are designed to be implemented under existing traffic volume and geometric layout conditions, and include all-way stop control at either one or both of the aforementioned intersections.

Note that the Synchro software utilizes the HCM methodology to compute the control delays and LOS (Shown in Table 2). Since this method treats the intersections separately, delays generated at one intersection will not be reflected at an adjacent intersection within close proximity. As such, increased average delays and decreased LOS are not shown by the Synchro software at the frontage road intersections. Although all-way stop control at the ramp intersections will almost certainly affect operations at the Theatre Drive and Ramada Drive intersections. However, these impacts are clearly seen when utilizing the SimTraffic simulation for the queuing analysis. The microlevel analysis found within SimTraffic is better able to accurately demonstrate the likely affects of the mitigation measures at the US 101 ramp intersections and at the adjacent frontage road intersections.

In addition, there was a discussion with County staff regarding analyzing the west side of the freeway as one intersection (US 101 southbound ramps and Theatre Drive combined) and the east side of the freeway as another intersection (US 101 northbound ramps and Ramada Drive combined). In order to optimize traffic flow and minimize queues, vehicles would need to be allowed free movements between the ramp and frontage road intersections. However, allowing free movements would create driver confusion, particularly for left turn turning vehicles with multiple options (i.e.: left turn at northbound on-ramp or at the Ramada Drive). In addition, on the west side of the freeway there would be 2 southbound approaches (Theater Drive and US 101 southbound off-ramp), which would also create driver confusion. A review of existing conditions indicate that the distance between the east and westbound limit lines on Main Street would be at least 200' on either side of the freeway. Due to the operational and safety concerns, it was decided that the east and west intersections should not be grouped together for the all-way stop control mitigation analysis. The installation of all-way stop control at all 4 study intersections is not considered a viable alternative, as significant vehicle queues would be experienced along Main Street.

7.1 Intersections Operations

The short-term mitigation measure scenarios were run in Synchro to determine the affects of adding all-way stop control at the Main Street and US 101 northbound ramps intersection only (Short-Term Measure #1), at the Main Street and US 101 southbound ramps intersection only (Short-Term Measure #2), and at both intersections simultaneously (Short-Term Measure #3). Currently, these intersections have stop control only for the off-ramp approaches. It should be noted that the evaluation of short-term mitigation measures focuses on the analysis of PM peak hour operations only, as this period represents the "worse case" scenario. The results of the LOS analysis for the short-term mitigation scenarios are presented in **Table 5**, with the LOS worksheets included in **Appendix E**.

| | | Vehicle Delay - LOS Value | | | | | | |
|---------------------------------------|-----------------------------------|---------------------------|-------------------------------------|-------------------------------------|---|--|--|--|
| Study Intersection Main Street at: | Critical Movement (PM Peak) | Existing | STM #1 US 101 NB Ramps | STM #2 US 101 SB Ramps | STM #3 US 101 NB & SB Ramps | | | |
| Theatre Drive | Average | 7.0 - A | 7.0 - A | 7.0 - A | 7.0 - A | | | |
| | EB | 2.2 - A | 2.2 - A | 2.2 - A | 2.2 - A | | | |
| | NB | 8.8 - A | 8.8 - A | 8.8 - A | 8.8 - A | | | |
| | SB | 14.5 - B | 14.5 - A | 14.5 - B | 14.5 - B | | | |
| US 101 SB Ramps | Average | 7.2 - A | 7.2 - A | 15.4 - C | 15.4 - C | | | |
| | EB | N/A | N/A | 12.0 - B | 12.0 - B | | | |
| | WB | 4.1- A | 4.1 - A | 19.1 - C | 19.1 - C | | | |
| | SB | 35.5- E | 35.5 - E | 10.6 - B | 10.6 - B | | | |
| US 101 NB Ramps | Average | 8.4 - A | 15.4 - C | 8.4 - A | 15.4 - C | | | |
| | EB | 1.1 - A | 12.6 - B | 1.1 - A | 12.6 - B | | | |
| | WB | N/A | 18.7 - C | N/A | 18.7 - C | | | |
| | NB | 26.4 - D | 12.8 - B | 26.4 -D | 14.4 - B | | | |
| Ramada Drive | Average | 5.5 - A | 5.5 - A | 5.5 - A | 5.5 - A | | | |
| | EB | 4.0 - A | 4.0 - A | 4.0 - A | 4.0 - A | | | |
| | SB | 14.8 - B | 14.8 - B | 14.8 - B | 14.8 - B | | | |

 TABLE 5

 INTERSECTION LOS ANALYSIS WITH ALL-WAY STOP MITIGATION

- Delays and Level of Service (LOS) calculated utilizing the methodologies described in Chapters 16 and 17 of the 2000 Highway Capacity Manual (HCM).

X.X – Data Represents Total Average Peak Hour Volume

LOS = Level of Service; Average Delay in seconds.

TWSC = Two-Way Stop Controlled Intersection

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

The data in **Table 5** indicates that the installation of all-way stop control at either ramp intersection would significantly reduce delays for the off-ramp movements (STM #1, STM #2 or STM #3). The LOS for the southbound off-ramp would meet the minimum LOS threshold standards under STM #2 and STM # 3, and the LOS for the northbound off-ramp would meet minimum LOS threshold standards under STM #1 and STM #3. However, delays would increase significantly for the east and westbound approaches on Main Street. Increased delays for vehicles on Main Street would also result in longer vehicle queues.

As previously stated, the Synchro software treats the 4 study intersections separately. Therefore, the increase of delays on the east and westbound approaches of Main Street are not reflected at the adjacent frontage road intersections when installing all-way stop control at either ramp intersection. If all-way stop control is installed at the southbound ramps intersection delays would increase significantly on the southbound approach of Theatre Drive. In a similar manner, if all-way stop control is installed at the northbound ramps intersection delays would increase significantly on the southbound approach of Ramada Drive and westbound approach of Main Street. The impacts associated with these short-term mitigation measure alternatives are more clearly seen using the SimTraffic simulation. The queuing analysis using SimTraffic also better demonstrates the impacts associated with installing all-way stop control at either one or both the ramp intersections.

7.2 Queuing Analysis

An analysis of queuing results from SimTraffic shows that adding all-way stop control at the two US 101 ramp intersections on Main Street would result in additional queuing through the adjacent intersections with the frontage roads. See **Table 6** for summarized queuing results for the all-way stop controlled short-term mitigation scenarios, and **Appendix I** for the full SimTraffic queuing computations.

| | - | | | | | | | |
|---------------------------------------|--|----------|--|-------------------------------------|-------------------------------------|---|--|--|
| | | | 95 th Percentile Queue Length | | | | | |
| Study Intersection Main Street at: | Critical Existing Movement Storage (Exist. PHV) Length | | Existing | STM #1 US 101 NB Ramps | STM #2 US 101 SB Ramps | STM #3 US 101 NB & SB Ramps | | |
| Theatre Drive | PM Peak | | | | | | | |
| | NB LTR | | 24 | 24 | 24 | 24 | | |
| | SB LTR | | 103 | 116 | 117 | 122 | | |
| US 101 SB Ramps | PM Peak | | | | | | | |
| _ | EB RT | 40^{1} | N/A | N/A | 57 | 56 | | |
| | WB LT | 335 | 108 | 95 | 110 | 99 | | |
| | SB LT | 1000 | 78 | 69 | 52 | 51 | | |
| US 101 NB Ramps | PM Peak | | | | | | | |
| | EB LT | 335 | 56 | 50 | 42 | 44 | | |
| | WB RT | 40^{1} | N/A | 49 | N/A | 50 | | |
| | NB LT | 800 | 99 | 73 | 114 | 80 | | |
| Ramada Drive | PM Peak | | | | | | | |
| | EB LT | 40^{1} | 42 | 44 | 44 | 44 | | |
| | WB TR | | N/A | 271 | 26 | 329 | | |
| | SB L | | 92 | 711 | 69 | 697 | | |

 TABLE 6

 INTERSECTION QUEUE LENGTHS WITH ALL-WAY STOP MITIGATION

¹Measured clear distance between adjacent intersections.

AWSC = All-Way Stop Controlled Intersection

TWSC = Two-Way Stop Controlled Intersection

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

The implementation of all-way stop control at the northbound ramps (STM #1) would reduce vehicle queues on the off-ramp by about 25%. However, due to the close proximity of the US 101 ramp intersections longer queues would be experienced on the southbound Ramada Drive approach (8 times existing) and westbound Main Street approach. Longer queues on the southbound Ramada Drive approach would also increase delays for vehicles currently making right turns, as the queue would back up beyond the flared roadway section. If all-way stop control is utilized as a near-term mitigation measure at the northbound ramps intersection, (STM #1), it would be necessary to install "KEEP CLEAR" pavement markings on North Main Street within the limits of the Ramada Drive and Main Street intersection in order to keep the westbound queue from blocking the eastbound and southbound left turn movements. In addition, westbound through traffic stopped at the northbound ramps will block the line-of-sight for vehicles making the southbound left turns from Ramada Drive to eastbound Main Street, potentially impacting safety at this intersection.

The implementation of all-way stop control at the southbound ramps (STM #2) would reduce vehicle queues on the off-ramp by about 35%. However, longer queues would be experienced on the southbound Theatre Drive approach. The westbound queue on Main Street would exceed the storage capacity between the Theatre Drive and ramps intersections, which would backup traffic past the southbound ramps intersection and onto the bridge. It would be necessary to install "KEEP CLEAR" pavement markings on Main Street within the limits of the southbound ramps and Main Street intersection to keep the westbound queue from blocking the southbound left turns from the off-ramp. At this location, line-of-sight could be impacted for the northbound Theatre Drive traffic. However, these traffic volumes are minimal, and do not pose the same safety concerns as at the Ramada Drive intersection.

The implementation of all-way stop control at both ramp intersections (STM #3) would reduce queues on both the north and southbound off-ramps (10-35%). However, longer queues would be experienced on the southbound approaches of Ramada Drive (7.5 times existing) and Theatre Drive (1.2 times existing), and on the westbound approach of Main Street at Ramada Drive. As discussed under STM #1 and STM #2, "KEEP CLEAR" pavement markings would be required on Main Street for westbound traffic at Ramada Drive and the southbound ramps intersection.

7.3 Conclusion: All-Way Stop Control feasibility

The analysis of queuing associated with STM #1, STM #2 and STM #3 alternatives indicates that the installation of all-way stop control at either one or both ramp intersections could reduce queuing on the US 101 off-ramps. However, stopping east-west free-flowing traffic on Main Street would increase queues on Main Street at the US 101 ramp and for adjacent frontage road intersections. In addition, since current queuing on the off-ramps has not been identified as a problem and utilizes less than 20% of the available capacity (see **Table 4**), it is <u>not</u> <u>recommended</u> that all-way stop control be considered as a viable short-term mitigation measure. However, as future traffic volumes increase on the off-ramps and queuing backs up toward the freeway main-line the implementation of all-way stop control may become a more viable alternative. The analysis of future year "2030" buildout demands may show a greater benefit to these short-term mitigation measure alternatives.

8.0 INTERSECTION OPERATIONS WITH TRAFFIC SIGNAL MITIGATION

This section evaluates the feasibility of utilizing traffic signals as a short-term mitigation measures to alleviate traffic congestion at the US 101/ Main Street interchange and adjacent intersections. These measures are designed to be implemented under existing traffic volume and geometric layout conditions.

As previously stated, the Synchro software treats the intersections separately, and therefore, delays generated at one intersection may not be reflected at an adjacent intersection within close proximity. For the scenarios where only the ramp intersections are signalized, there will be impacts on the traffic operations at the Theatre Drive and Ramada Drive intersections, although these impacts are not necessarily shown in the Synchro output.

Additionally, it should be noted that for the two scenarios where the intersections on the west side and the intersections on the east side are grouped, (STM #7 and STM #8), there is some difficulty in accurately modeling expected traffic conditions with Synchro software. At the eastern intersections, it was decided in discussions with County staff that the most accurate way of modeling the two intersections as a single system would be to run the two intersections as a single intersection (node) with five legs. At the western intersections, due to the more complex roadway geometry, the decision was made by County staff to model the intersections as separate intersections with two coordinated signal systems. While efforts were made to approximate actual traffic conditions with both intersections signalized, Synchro software is limited because it will not treat the two intersections as one. It is possible that at both the east and west intersection groups, actual field conditions would be better than those shown in **Table 7** and **Table 8** with optimized signal timing and striping layout.

8.1 Intersection Analysis

The short-term mitigation measure scenarios were run in Synchro to determine the affects of adding traffic signals at the Main Street and US 101 northbound ramps intersection only (Short-Term Measure #4), at the Main Street and US 101 southbound ramps intersection only (Short-Term Measure #5), and at both intersections simultaneously (Short-Term Measure #6). Two additional signal scenarios were also analyzed. First, a scenario was run with both intersections west of US 101 signalized and grouped as one traffic signal system, and the intersections east of US 101 configured as a single-node, five-legged intersection with a traffic signal (Short Term Measure #7). Secondly, a scenario was analyzed with the northbound ramps and Ramada Drive intersections configured as a single-node, five-legged intersection with a traffic signal, and an signal at the southbound ramps intersection only on the west side of US 101 (Short Term Measure #8). Currently, all intersections have stop control only on the minor streets. It should be noted that the evaluation of short-term mitigation measures focuses on the analysis of PM peak hour operations only, as this period represents the "worse case" scenario. The results of the LOS analysis for the short-term mitigation scenarios are presented in **Table 7**, with the LOS worksheets included in **Appendix E.**

| | | Vehicle Delay - LOS Value | | | | | | | |
|---------------------------------------|-----------------------------------|---------------------------|-------------------------------------|-------------------------------------|---|---|--|--|--|
| Study Intersection Main Street at: | Critical Movement (PM Peak) | Existing | STM #4 US 101 NB Ramps | STM #5 US 101 SB Ramps | STM #6 US 101 NB & SB Ramps | STM #7 Western & Eastern Intersections | STM #8 Eastern Intersections & US 101 SB Ramps | | |
| Theatre Drive | Average | 7.0 - A | 7.0 - A | 6.3 - A | 6.5 - A | 19.3 – B | 6.5 - A | | |
| | EB | 2.2 - A | 2.2 - A | 2.2 - A | 2.2 - A | 53.7 - D | 2.2 - A | | |
| | WB | N/A | N/A | N/A | N/A | 2.4 - A | N/A | | |
| | NB | 8.8 - A | 8.8 - A | 8.7 - A | 8.7 - A | 46.9 - D | 8.7 - A | | |
| | SB | 14.5 - B | 14.5 - B | 13.1 - B | 13.5 - B | 33.4 - C | 13.5 - B | | |
| US 101 SB Ramps | Average | 7.2 - A | 7.2 - A | 5.2 - A | 6.6 - A | 56.7 - E | 9.0 - A | | |
| | EB | N/A | N/A | 2.9 - A | 3.3 – A | 2.9 - A | 2.9 - A | | |
| | WB | 4.1 - A | 4.1 - A | 54.3 - A | 5.0 - A | 91.4 - F | 5.3 - A | | |
| | SB | 35.5 - E | 35.5 - E | 13.8 - B | 20.0 - C | 67.7 - E | 36.5 - D | | |
| US 101 NB Ramps | Average | 8.4 - A | 7.0 - A | 8.4 - A | 9.3 – A | 47.7 - D ¹ | $36.9 - D^1$ | | |
| | EB | 1.1 - A | 4.6 - A | 1.1 - A | 5.3 - A | 60.0 – E | 32.2 – C | | |
| | WB | N/A | 5.2 - A | N/A | 6.0 - A | N/A^1 | N/A ¹ | | |
| | NB | 26.4 - D | 11.4 - B | 26.4 -D | 17.4 - B | 37.6 -D | 37.1 – D | | |
| Ramada Drive | Average | 5.5 - A | 5.5 - A | 5.5 - A | 5.5 - A | N/A ¹ | N/A ¹ | | |
| | EB | 4.0 - A | 4.0 - A | 4.0 - A | 4.0 - A | N/A ¹ | N/A ¹ | | |
| | SB | 14.8 - B | 14.8 - B | 14.8 - B | 14.8 - B | 49.9 - D | 36.6 – D | | |
| | WB | N/A | N/A | N/A | N/A | $46.7 - D^1$ | $40.4 - D^1$ | | |

 TABLE 7

 INTERSECTION LOS ANALYSIS WITH SIGNALIZED MITIGATION

¹For STM #7 and #8, the northbound ramps and Ramada Drive are modeled as one intersection. Westbound delays are shown only at Ramada Drive, and eastbound delays are shown only for the northbound ramps intersection.

- Delays and Level of Service (LOS) calculated utilizing the methodologies described in Chapters 16 and 17 of the 2000 Highway Capacity Manual (HCM).

X.X – Data Represents Total Average Peak Hour Volume

LOS = Level of Service; Average Delay in seconds.

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

As with the all-way stop control alternatives, adding traffic signal control on Main Street at either ramp intersection would reduce the off-ramp delays and improve the LOS at that intersection. The LOS at the southbound off-ramp would meet the minimum LOS standards with STM #5 or STM #6 in place. The LOS at the northbound off-ramp would meet the minimum LOS standards with STM #4 or STM #6 in place.

When both intersections were signalized on the west side of US 101 and the eastern intersections were grouped into a single node and signalized (STM #7), overall LOS for both the Theatre Drive intersection and the southbound ramps intersection worsened significantly. Of particular note is the worsening of eastbound and westbound traffic across the bridge, and at the Ramada Drive intersection. Under STM #7, both the southbound ramps intersection and the eastern intersection failed to meet the County and Caltrans LOS minimum. At the eastern intersection, (Ramada Dr. and northbound ramps intersections), split-phase timing was used for all approaches at the request of the County. This method will provide the greatest level of safety in

an intersection with multiple potential turning conflicts, but it also worsens the overall intersection LOS and queuing lengths.

With both intersections on the east side of US 101 grouped and signalized and just the southbound ramps intersection signalized on the west side of US 101, (STM #8), overall LOS and queuing was worse than existing conditions, although the impacts were primarily restricted to the east side US 101. Under this mitigation measure, the eastern intersection fails to meet the County and Caltrans LOS minimum.

As previously stated, the Synchro software treats the 4 study intersections independently. Therefore, the stopping of east-west vehicles on Main Street does not affect delays at the adjacent frontage road intersection (i.e.: the northbound ramps and Ramada Drive). If traffic signal control is installed at the southbound ramps intersection, delays may increase on the southbound approach of Theatre Drive. In a similar manner, if traffic signal control is installed at the northbound ramps intersection delays may increase on the southbound approach of Ramada Drive and westbound approach of Main Street. The impacts associated with these short-term mitigation measure alternatives are more clearly seen using the SimTraffic simulation. The queuing analysis using SimTraffic also better demonstrates the impacts associated with installing traffic signal control at either one or both the ramp intersections.

8.2 Queuing Analysis

An analysis of queuing results from SimTraffic shows that adding traffic signal control at the US 101 ramp intersections on Main Street would in some cases reduce queuing on the north or southbound off-ramps. However, queuing would increase at other approaches as a result. See **Table 8** for summarized queuing results for the traffic signal short-term mitigation scenarios, and **Appendix I** for full Synchro queuing computations.

Constructing traffic signals at the northbound and/or southbound ramps intersections would result in similar queuing patterns to the all-way stop control mitigation. The implementation of traffic signal control at the northbound ramps (STM #4) would increase vehicle queues on the southbound approach of Ramada Drive. Longer queues on the southbound Ramada Drive approach would also increase delays for vehicles currently making right turns, as the queue would back up beyond the flared roadway section. The westbound queue on Main Street would also exceed the available capacity between the ramp intersection and Ramada Drive. "KEEP CLEAR" pavement markings would be required on Main Street within the limits of the intersection with Ramada Drive in order to keep the westbound queue from blocking the east and southbound left turn movements through that intersection. Similar to the discussion for alternative STM #1 (all-way stop control at northbound ramps), westbound through traffic stopped at the northbound ramps may block the line-of-sight for vehicles making the southbound left turns from Ramada Drive to eastbound Main Street.

| | | | | | 95 th Percent | ile Queue L | ength | |
|---------------------------------------|-----------------------------------|-------------------------------|----------|-------------------------------------|-------------------------------------|---|---|--|
| Study Intersection Main Street at: | Critical Movement (PM Peak) | Existing Storage Length | Existing | STM #4 US 101 NB Ramps | STM #5 US 101 SB Ramps | STM #6 US 101 NB & SB Ramps | STM #7 Western & Eastern Intersections | STM #8 Eastern Intersections & US 101 SB Ramps |
| Theatre Drive | PM Peak | | | | | | | |
| | NB LTR | | 24 | 25 | 24 | 24 | 46 | 37 |
| | SB LTR | | 103 | 106 | 105 | 107 | 324 | 370 |
| | EB LTR | | N/A | N/A | N/A | N/A | 39 | N/A |
| | WB LTR | 40^{1} | N/A | N/A | N/A | N/A | 72 | N/A |
| US 101 SB Ramps | PM Peak | | | | | | | |
| | EB RT | 40^{1} | N/A | N/A | 53 | 68 | 77 | 66 |
| | WB LT | 335 | 108 | 115 | 167 | 129 | 393 | 277 |
| | SB LT | 1000 | 78 | 79 | 93 | 72 | 143 | 210 |
| US 101 NB Ramps | PM Peak | | | | | | | |
| | EB LT | 335 | 56 | 78 | 49 | 86 | 232^{3} | 401 ³ |
| | WB RT | 40^{1} | N/A | 43 | N/A | 42 | N/A ³ | N/A ³ |
| | NB LT | 800 | 99 | 147 | 82 | 132 | 508 | 98 |
| Ramada Drive | PM Peak | | | | | | | |
| | EB LT | 40^{1} | 42 | 43 | 42 | 42 | N/A ³ | N/A ³ |
| | WB TR | | N/A | 72 | N/A | 72 | 295 ³ | 371 ³ |
| | SB L | | 92 | 176 | 143 | 177 | 472 | 188 |

TABLE 8 INTERSECTION QUEUE LENGTHS WITH SIGNALIZED MITIGATION

¹Measured clear distance between adjacent intersections.

³ For STM #7 and #8, the northbound ramps and Ramada Drive are modeled as one intersection. Westbound queues are shown only at Ramada Drive, and eastbound queues are shown only for the northbound ramps intersection.

NB = Northbound, SB = Southbound, EB = Eastbound, WB = Westbound

The implementation of signal control at the southbound ramps (STM #5) or at both ramp intersections (STM #6) would increase queues on the westbound approach of the southbound ramps intersection (1.2-1.5 times existing). The eastbound queue on Main Street would also exceed the available capacity between the ramp intersection and Theater Drive. Additionally, the southbound queues on Theatre Drive and Ramada Drive would not be improved.

Signalizing both intersections on the west side of US 101 and creating a single-node, five-way signalized intersection on the east side, (STM #7) would increase queues at nearly all approaches. Of particular importance, southbound Theatre Drive traffic turning left onto Main Street and westbound traffic on Main Street at the intersection with the northbound ramps would have significantly increased queue lengths. Since these movements comprise the majority of the traffic volumes through these two intersections, overall queuing at the intersections would be increased as a result of this mitigation measure.

Grouping and signalizing the intersections on the east side of US 101 and signalizing the southbound ramps intersection (STM #8), would increase queue lengths at nearly all approaches.

In particular, 95th percentile eastbound traffic queues at the northbound ramps intersection would exceed the storage capacity on the bridge.

It should be noted that comparing the queue lengths for both STM #7 and STM #8 with the existing condition and the other short-term mitigation measures is not exact, since the configuration of the eastern intersections was modeled as a single node in Synchro for these two mitigation measures to better reflect actual operational conditions.

8.3 Conclusion: Traffic Signal feasibility

Given existing traffic volumes and geometrical layout, for the first three short term mitigation measures (STM #4, #5 and #6), vehicle delays and LOS are not significantly better using traffic signals than those achieved using all-way stop control, and queuing is actually worse, on average.

On the east side of US 101, one signal warrant was met, (see Section 9.0 below). However, LOS was not improved significantly and queuing was worse, on average, when a signal was placed at the northbound ramps intersection (STM #4). Due to these considerations and the substantial additional costs associated with installation and maintenance of traffic signals as compared with all-way stop control, it is **not recommended** that signalization be considered as a short-term mitigation measure at the northbound US 101 ramps only.

Given that no signal warrants were met for the southbound ramps intersection, (see Section 9.0 below), and the considerable additional costs associated with installation and maintenance of traffic signals as compared with all-way stop control, it is **not recommended** that signalization be considered as a short-term mitigation measure at the southbound US 101 ramps intersection only (STM #5).

When both ramps were signalized and coordinated, (STM #6), LOS was improved for minor street approaches, but did not significantly improve overall LOS at the four intersections. On average, queues increased under this scenario. Due to the fact that conditions were not significantly improved, only a single warrant was met at for the northbound ramps intersection, and the substantial additional costs associated with installation and maintenance of traffic signals as compared with all-way stop control, it is **not recommended** that signalization be considered as a short-term mitigation measure at the southbound and northbound US 101 ramps.

With the western two intersections signalized and coordinated, and the eastern intersections grouped as a single node and signalized (STM #7), both LOS and queuing were significantly worse than under existing conditions. Thus, it is **not recommended** that signalization be considered as a short-term mitigation measure at the southbound and northbound US 101 ramps.

Similarly, with the eastern intersections grouped as a single node and signalized, and the southbound ramps intersection signalized (STM #8), both LOS and queuing were significantly worse than under existing conditions. It is **not recommended** that signalization be considered as a short-term mitigation measure at the southbound and northbound US 101 ramps. However, it should be noted that STM #7 and STM #8 would likely be more viable options with increased traffic volume. (See Deliverable 2)

9.0 SIGNAL WARRANT ANALYSIS

As part of this technical memorandum, an analysis of the feasibility of signalizing either one or both of the US 101 ramp intersections with Main Street as a short-term mitigation measure was completed in Section 8.0. However, since these intersections are within the limits of Caltrans right-of-way, they must also meet the justification for the installation of a traffic signal at an intersection, which is based on the eight warrants provided in the Caltrans Manual on Uniform Traffic Control Devices (CAMUTCD). Figures 4C-101 through 4C-4 in the CAMUTCD were used to analyze the traffic signal warrants based on existing average daily traffic and peak hour traffic volumes, and lane geometry.

There are a total of eight warrants that evaluate the need for a traffic signal based on many reasons including excessive delay to minor street traffic, large pedestrian volumes, a school crossing, signal progression, accident experience and excessive delay during the peak hour. When the 85th percentile speed of traffic on the major street exceeds 40 mph in either an urban or rural area, or when the intersection lies within the built-up area of an isolated community having a population of less than 10,000, the location is considered rural. See below for justification for roadway categorization:

- 1. Main Street is posted 45 mph to the south of the project limits, and speed surveys completed by the County on March 8, 2011 and May 3, 2011 indicate that the observed speeds are consistent with this posting. (See Appendix J)
- 2. The study location is considered to be within an isolated community with a population of less than 10,000.

The rural designation for signal warrants is meant to lower the traffic volume requirements for signalization in those areas were a significant amount of traffic will be entering the main street from minor streets in an otherwise rural area. At the ramp intersections, this situation is present. As such, the "rural" designation has been chosen for traffic signal warrant analysis. However, for comparison, an analysis was also completed for the "urban" warrants. See **Table 9** for a summary of the traffic signal warrant analysis and **Appendix F** for the signal warrant figures and tables.

As shown in the table below, under existing traffic conditions the only signal warrant which is met is Warrant #2, (Four-Hour Vehicular Volume), at the northbound ramps intersection with Main Street.

| Traffic Signal Warrant | Main St. / NI | B 101 Ramps | Main St. / Sl | B 101 Ramps |
|-------------------------------|--------------------|--------------------|--------------------|--------------------|
| | Rural ³ | Urban ³ | Rural ³ | Urban ³ |
| #1: 8-Hour Volumes | N/A ¹ | N/A ¹ | N/A ¹ | N/A ¹ |
| #2: 4-Hour Volumes | Yes | No | No | No |
| #3: Peak Hour | No | No | No | No |
| - Part A | No | No | No | No |
| - Part B | No | No | No | No |
| #4: Pedestrian Volume | No ² | No ² | No ² | No ² |
| #5: School Crossing | No | No | No | No |
| #6: Coordinated Signal System | No | No | No | No |
| #7: Crash Experience | No | No | No | No |
| #8: Roadway Network | No | No | No | No |

TABLE 9 TRAFFIC SIGNAL WARRANT SUMMARY

¹No 8-hour traffic counts have been completed at the study intersections.

²No observed pedestrian traffic during any field visits.

³See paragraph above for description of rural and urban designation. (Applicable for warrant #2 and #3)

10.0 SIGNALIZED INTERSECTING LANE VEHICLES (ILV) CAPACITY ANALYSIS

In addition to an analysis of traffic signal warrants, Caltrans utilizes the Signalized Intersection Capacity method in the Highway Design Manual to determine the traffic volume to intersection capacity relationship. The Intersection Lane Vehicles (ILV) method is a rough approximation of the functionality of a signalized intersection given traffic volumes. In general, with an ILV/hr of less than 1200, the signalized intersection would be expected to operate with minimal delay. (See **Table 10** ILV characteristics) Both intersections, during both AM and PM peak hours, are expected to have an ILV/hr of considerably less than 1200. (See **Appendix G** for the ILV method calculation sheets)

TABLE 10ILV TRAFFIC FLOW CHARACTERISTICS

| ILV/hr | Description |
|-----------|---|
| < 1200 | Stable flow with slight, but acceptable delay. Occasional signal loading may develop. Free midblock operations. |
| 1200-1500 | Unstable flow with considerable delays possible. Some vehicles occasionally wait two or more cycles to pass through the intersection. Continuous backup occurs on some approaches. |
| > 1500 | Stop-and-go operation with severe delay and heavy congestion. Traffic volume is limited by maximum discharge rates of each phase. Continuous backup in varying degrees occurs on all approaches. Where downstream capacity is restrictive, mainline congestion can impede orderly discharge through the intersection. |

Source: Highway Design Manual, Table 406, California Department of Transportation.

APPENDIX A

TRAFFIC COUNT DATA



Metro Traffic Data Inc.

310 N. Irwin Street - Suite 20 Hanford, CA 93230

800-975-6938 Phone/Fax

www.metrotrafficdata.com

| LOCATION Main Street/Theater Drive/US 101 SB |
|--|
|--|

| COUNTY | San Luis Obis |
|--------|---------------|
| | |

| | | | LUCATION | Main S | treet/ I neate | er Drive | e/US 101 SB | | | | | | | | | | | | | LAIIIUDE | | | | | | _ |
|-------------------|---|--------|--------------|-----------|----------------|----------|-------------|-------|---------|------|-------|--------|---------------|---------------|--------------|--------|----|---------|-----------|------------|--------|-----------|------------|-----|-----|--------|
| | | | COUNTY | | San Luis | s Obisp | 00 | | | | | | | | | | | | | LONGITUDE | | | | | | |
| | | COLLEC | TION DATE | | 9/16/ | /2009 | | | | | | | | | | | | | | WEATHER | | Cle | ar | | | _ |
| | | Nor | thbound (The | eater Dr) | | | Southbound | (Thea | ter Dr) | | | | Southbound | d (SB 101 OFF |) | | | | Eastbou | und | | | Westbou | und | | |
| Time | L | т | R(Main) | R(SB 101) | Trucks | L | L(SB 101) | т | R Tru | ucks | L T(S | B 101) | R (Theater S) | R (Main) | R(Theater N) | Trucks | L | T(Main) | T(SB 101) | R(Theater) | Trucks | L(SB 101) | L(Theater) | Т | R | Trucks |
| 7:00 AM - 7:15 AM | 0 | 0 | 0 | 0 | 0 | 15 | 13 | 0 | 1 | 2 2 | 27 | 0 | 0 | 0 | 3 | 1 | 0 | 3 | 0 | 0 | 1 | 17 | 0 | 0 | 25 | 7 |
| 7:15 AM - 7:30 AM | 0 | 0 | 1 | 1 | 1 | 26 | 35 | 0 | 2 | 1 4 | 41 | 0 | 0 | 0 | 4 | 1 | 1 | 1 | 5 | 0 | 2 | 19 | 0 | 1 | 34 | 4 |
| 7:30 AM - 7:45 AM | 0 | 0 | 1 | 1 | 1 | 31 | 28 | 0 | 4 | 3 3 | 37 | 0 | 0 | 0 | 2 | 2 | 1 | 3 | 8 | 0 | 4 | 17 | 0 | 6 | 38 | 6 |
| 7:45 AM - 8:00 AM | 0 | 0 | 0 | 1 | 0 | 33 | 26 | 0 | 0 | 1 4 | 47 | 0 | 1 | 1 | 4 | 5 | 2 | 1 | 6 | 0 | 3 | 20 | 0 | 4 | 50 | 9 |
| 8:00 AM - 8:15 AM | 0 | 2 | 0 | 0 | 1 | 22 | 26 | 1 | 2 | 0 4 | 41 | 0 | 1 | 0 | 1 | 4 | 1 | 0 | 4 | 0 | 0 | 23 | 0 | 8 | 60 | 9 |
| 8:15 AM - 8:30 AM | 0 | 0 | 1 | 0 | 1 | 23 | 26 | 0 | 0 | 0 2 | 26 | 0 | 1 | 0 | 6 | 2 | 1 | 2 | 0 | 0 | 0 | 24 | 0 | 3 | 35 | 4 |
| 8:30 AM - 8:45 AM | 0 | 0 | 1 | 0 | 0 | 11 | 23 | 0 | 2 | 3 1 | 19 | 0 | 0 | 0 | 4 | 4 | 1 | 1 | 2 | 0 | 1 | 17 | 0 | 0 | 52 | 7 |
| 8:45 AM - 9:00 AM | 0 | 0 | 0 | 3 | 0 | 13 | 31 | 0 | 1 | 0 3 | 31 | 0 | 0 | 0 | 4 | 2 | 3 | 4 | 4 | 0 | 3 | 18 | 0 | 5 | 36 | 9 |
| TOTAL | 0 | 2 | 4 | 6 | 4 | 174 | 208 | 1 : | 12 1 | LO 2 | 69 | 0 | 3 | 1 | 28 | 21 | 10 | 15 | 29 | 0 | 14 | 155 | 0 | 27 | 330 |) 55 |

| | | Nor | thbound (The | ater Dr) | | | Southbound | (Thea | ater Dr) | | | Southboun | d (SB 101 OFI | F) | | | | Eastbou | und | | | Westbou | Ind | | |
|--------------------|----------|-----|--------------|-----------|--------|-----|------------|-------|----------|-----|-----------|---------------|---------------|--------------|--------|----|---------|-----------|------------|--------|-----------|------------|-----|-----|--------|
| Time | L | т | R(Main) | R(SB 101) | Trucks | L | L(SB 101) | Т | R Trucks | L | T(SB 101) | R (Theater S) | R (Main) | R(Theater N) | Trucks | L | T(Main) | T(SB 101) | R(Theater) | Trucks | L(SB 101) | L(Theater) | т | R | Trucks |
| 3:00 PM - 3:15 PM | 0 | 0 | 2 | 1 | 0 | 33 | 46 | 0 | 2 2 | 32 | 0 | 0 | 0 | 6 | 3 | 1 | 0 | 2 | 0 | 0 | 41 | 0 | 4 | 73 | 6 |
| 3:15 PM - 3:30 PM | 0 | 1 | 1 | 1 | 0 | 21 | 34 | 0 | 1 2 | 26 | 0 | 2 | 1 | 1 | 0 | 2 | 2 | 1 | 0 | 0 | 31 | 0 | 1 | 72 | 3 |
| 3:30 PM - 3:45 PM | 0 | 0 | 1 | 0 | 1 | 36 | 47 | 0 | 1 2 | 28 | 0 | 0 | 0 | 9 | 2 | 0 | 1 | 6 | 0 | 0 | 37 | 0 | 5 | 68 | 3 |
| 3:45 PM - 4:00 PM | 0 | 0 | 1 | 3 | 0 | 22 | 55 | 1 | 1 2 | 23 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 1 | 0 | 0 | 49 | 0 | 8 | 52 | 3 |
| 4:00 PM - 4:15 PM | 0 | 0 | 0 | 4 | 0 | 17 | 59 | 0 | 1 3 | 31 | 0 | 2 | 0 | 4 | 1 | 1 | 4 | 7 | 0 | 0 | 20 | 0 | 7 | 68 | 0 |
| 4:15 PM - 4:30 PM | 0 | 0 | 0 | 1 | 0 | 20 | 45 | 0 | 1 0 | 29 | 0 | 1 | 0 | 4 | 0 | 1 | 4 | 11 | 0 | 0 | 33 | 0 | 11 | 77 | 5 |
| 4:30 PM - 4:45 PM | 0 | 0 | 1 | 0 | 0 | 26 | 45 | 1 | 5 1 | 31 | 0 | 1 | 0 | 4 | 1 | 3 | 1 | 5 | 0 | 0 | 31 | 0 | 5 | 57 | 5 |
| 4:45 PM - 5:00 PM | 0 | 0 | 1 | 3 | 0 | 25 | 66 | 1 | 0 1 | 31 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 1 | 0 | 0 | 24 | 0 | 0 | 58 | 2 |
| 5:00 PM - 5:15 PM | 0 | 2 | 2 | 2 | 0 | 41 | 47 | 1 | 0 0 | 22 | 0 | 1 | 0 | 5 | 3 | 0 | 3 | 5 | 0 | 0 | 34 | 0 | 1 | 80 | 4 |
| 5:15 PM - 5:30 PM | 0 | 0 | 1 | 0 | 0 | 46 | 32 | 0 | 0 0 | 23 | 0 | 0 | 0 | 4 | 1 | 0 | 1 | 2 | 0 | 0 | 14 | 0 | 0 | 76 | 2 |
| 5:30 PM - 5:45 PM | 0 | 0 | 0 | 0 | 0 | 27 | 53 | 0 | 0 1 | 27 | 0 | 0 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 65 | 2 |
| 5:45 PM - 6:00 PM | 0 | 0 | 0 | 1 | 0 | 29 | 53 | 1 | 0 2 | 25 | 0 | 0 | 0 | 3 | 1 | 0 | 1 | 0 | 0 | 0 | 17 | 0 | 0 | 72 | 3 |
| TOTAL | 0 | 3 | 10 | 16 | 1 | 343 | 582 | 5 | 12 16 | 328 | 0 | 8 | 2 | 50 | 17 | 11 | 23 | 41 | 0 | 0 | 347 | 0 | 42 | 818 | 38 |
| TOTAL Peak Hour | <u> </u> | 3 | 10 | 16 | 1 | 343 | 582 | 5 | 12 16 | 328 | 0 | 8 | 2 | 50 | 17 | 11 | 23 | 41 | 0 | 0 | 347 | 0 | 42 | - | 318 |

| i eak noui | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|---|---|---|---|---|-----|-----|-----|---|-----|---|---|---|----|----|---|----|----|---|---|-----|---|--------|----|
| 7:15 AM - 8:15 AM | 0 | 2 | 2 | 3 | 3 | 112 | 115 | 1 8 | 5 | 166 | 0 | 2 | 1 | 11 | 12 | 5 | 5 | 23 | 0 | 9 | 79 | 0 | 19 182 | 28 |
| 3:30 PM - 4:30 PM | 0 | 0 | 2 | 8 | 1 | 95 | 206 | 1 4 | 7 | 111 | 0 | 4 | 1 | 19 | 5 | 5 | 12 | 25 | 0 | 0 | 139 | 0 | 31 265 | 11 |
| | | | | | | | | | | | | | | | | | | | | | | | | |

| | AM | PM |
|--------|-------|-------|
| PHF | 0.94 | 0.97 |
| Trucks | 7.74% | 2.91% |

Turning Movement Report

Prepared For:

Michelle Olmsted-Matson, PE County of San Luis Obispo Department of Public Works (805) 788-2830



Metro Traffic Data Inc. 310 N. Irwin Street - Suite 20

Hanford, CA 93230 800-975-6938 Phone/Fax

www.metrotrafficdata.com

Turning Movement Report

Prepared For:

Michelle Olmsted-Matson, PE County of San Luis Obispo Department of Public Works (805) 788-2830

| | | | LOCATION | | Main Stree | et/Ramada Drive/ | 'US 101 NB | | | | LATITUDE | | | | | | |
|-------------------|-----|------|-------------|---------|------------|------------------|------------|---------|--------|---------|-----------|------|--------|-------|---------|-----------|--------|
| | | | COUNTY | | | San Luis Obispo |) | | | | LONGITUDE | | | | | | |
| | | COLL | ECTION DATE | | | 9/16/2009 | | | | | WEATHER | | | Clear | | | |
| | | | Northbound | 1 | | | Southb | ound | | | Eastbo | ound | | | West | bound | |
| Time | L | т | R(Ramada) | R(Main) | Trucks | L | R(Main) | R(101N) | Trucks | L(101N) | L(Ramada) | Т | Trucks | т | R(101N) | R(Ramada) | Trucks |
| 7:00 AM - 7:15 AM | 17 | 0 | 11 | 3 | 1 | 4 | 1 | 13 | 7 | 13 | 12 | 17 | 3 | 21 | 3 | 21 | 10 |
| 7:15 AM - 7:30 AM | 22 | 0 | 21 | 0 | 3 | 10 | 2 | 15 | 7 | 22 | 12 | 35 | 6 | 33 | 3 | 43 | 9 |
| 7:30 AM - 7:45 AM | 33 | 0 | 18 | 5 | 11 | 10 | 4 | 10 | 8 | 26 | 8 | 43 | 11 | 42 | 3 | 26 | 5 |
| 7:45 AM - 8:00 AM | 38 | 0 | 18 | 13 | 6 | 9 | 2 | 14 | 10 | 40 | 10 | 28 | 8 | 51 | 4 | 36 | 11 |
| 8:00 AM - 8:15 AM | 21 | 0 | 11 | 8 | 6 | 11 | 1 | 13 | 3 | 8 | 14 | 47 | 9 | 49 | 6 | 17 | 8 |
| 8:15 AM - 8:30 AM | 26 | 0 | 18 | 4 | 4 | 3 | 0 | 22 | 6 | 1 | 23 | 31 | 4 | 46 | 8 | 14 | 2 |
| 8:30 AM - 8:45 AM | 30 | 0 | 27 | 6 | 8 | 2 | 2 | 16 | 7 | 4 | 0 | 27 | 6 | 37 | 11 | 4 | 1 |
| 8:45 AM - 9:00 AM | 21 | 0 | 10 | 1 | 1 | 4 | 0 | 6 | 1 | 2 | 16 | 34 | 1 | 12 | 3 | 8 | 0 |
| TOTAL | 208 | 0 | 134 | 40 | 40 | 53 | 12 | 109 | 49 | 116 | 95 | 262 | 48 | 291 | 41 | 169 | 46 |
| | | | | | | | | | | | | | | | | | |

| | | | Northbound | 1 | | | South | ound | | | Eastbo | ound | | | West | bound | |
|-------------------|-----|---|------------|---------|--------|-----|---------|---------|--------|---------|-----------|------|--------|------|---------|-----------|--------|
| Time | L | т | R(Ramada) | R(Main) | Trucks | L | R(Main) | R(101N) | Trucks | L(101N) | L(Ramada) | Т | Trucks | т | R(101N) | R(Ramada) | Trucks |
| 3:00 PM - 3:15 PM | 60 | 0 | 12 | 8 | 5 | 20 | 7 | 36 | 7 | 7 | 13 | 49 | 2 | 69 | 17 | 15 | 1 |
| 3:15 PM - 3:30 PM | 53 | 2 | 14 | 7 | 7 | 23 | 5 | 34 | 3 | 7 | 10 | 30 | 2 | 55 | 16 | 4 | 1 |
| 3:30 PM - 3:45 PM | 47 | 0 | 21 | 2 | 4 | 12 | 10 | 31 | 7 | 7 | 13 | 41 | 3 | 48 | 20 | 9 | 1 |
| 3:45 PM - 4:00 PM | 54 | 1 | 20 | 1 | 1 | 26 | 11 | 24 | 8 | 4 | 12 | 34 | 3 | 49 | 8 | 17 | 0 |
| 4:00 PM - 4:15 PM | 45 | 0 | 8 | 11 | 4 | 21 | 6 | 30 | 3 | 10 | 11 | 25 | 4 | 56 | 17 | 10 | 0 |
| 4:15 PM - 4:30 PM | 48 | 0 | 9 | 8 | 3 | 14 | 6 | 25 | 2 | 9 | 8 | 30 | 2 | 38 | 14 | 5 | 0 |
| 4:30 PM - 4:45 PM | 64 | 1 | 11 | 5 | 7 | 14 | 14 | 32 | 4 | 6 | 9 | 50 | 0 | 42 | 10 | 11 | 1 |
| 4:45 PM - 5:00 PM | 41 | 0 | 15 | 1 | 3 | 15 | 5 | 35 | 2 | 7 | 6 | 44 | 3 | 45 | 17 | 9 | 0 |
| 5:00 PM - 5:15 PM | 35 | 0 | 5 | 7 | 2 | 12 | 6 | 28 | 3 | 10 | 9 | 55 | 0 | 43 | 9 | 6 | 0 |
| 5:15 PM - 5:30 PM | 49 | 0 | 19 | 7 | 0 | 9 | 5 | 29 | 5 | 3 | 11 | 46 | 2 | 52 | 20 | 6 | 0 |
| 5:30 PM - 5:45 PM | 66 | 1 | 7 | 9 | 2 | 9 | 0 | 18 | 0 | 4 | 13 | 35 | 2 | 35 | 14 | 5 | 0 |
| 5:45 PM - 6:00 PM | 48 | 0 | 7 | 5 | 2 | 12 | 3 | 13 | 1 | 4 | 13 | 33 | 2 | 30 | 13 | 6 | 0 |
| TOTAL | 610 | 5 | 148 | 71 | 40 | 187 | 78 | 335 | 45 | 78 | 128 | 472 | 25 | 562 | 175 | 103 | 4 |
| | | | | | | | | | | | | | | | | | |
| Peak Hour |] | | | | | | | | | | | | | | | | |
| | | • | 60 | | 26 | | | | | | | 450 | | 4.75 | 4.6 | 400 | |

| 3:00 PM - 4:00 PM 214 3 67 18 17 81 33 125 25 25 48 154 10 221 61 45 | 7:15 AM - 8:15 AM | 114 | 0 | 68 | 26 | 26 | 40 | 9 | 52 | 28 | 96 | 44 | 153 | 34 | 175 | 16 | 122 | 33 |
|--|-------------------|-----|---|----|----|----|----|----|-----|----|----|----|-----|----|-----|----|-----|----|
| | 3:00 PM - 4:00 PM | 214 | 3 | | | 17 | 81 | 33 | 125 | 25 | 25 | | 154 | 10 | 221 | 61 | 45 | 3 |

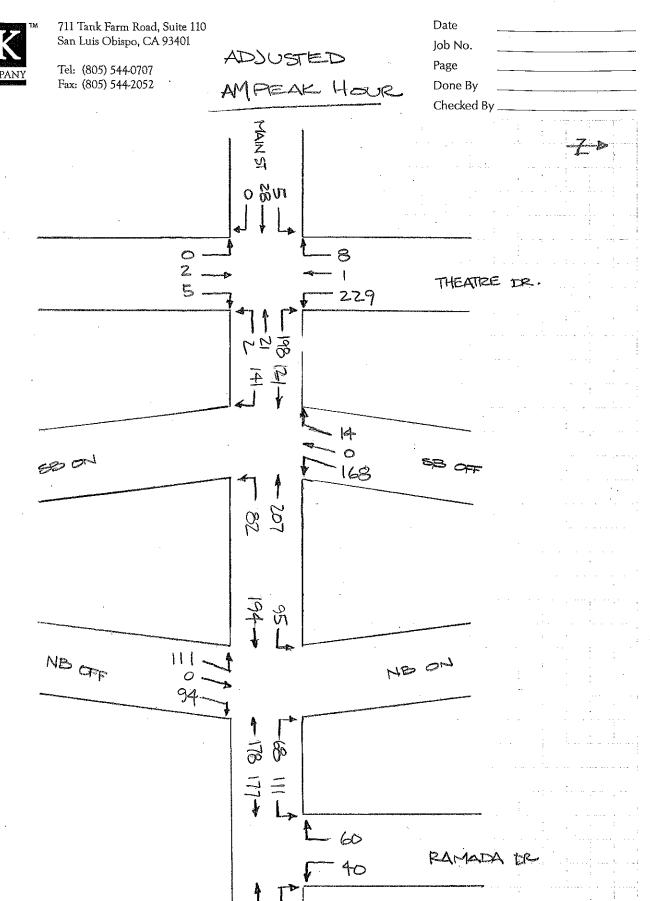
| | AM | PM |
|--------|--------|-------|
| PHF | 0.87 | 0.87 |
| Trucks | 13.22% | 5.02% |

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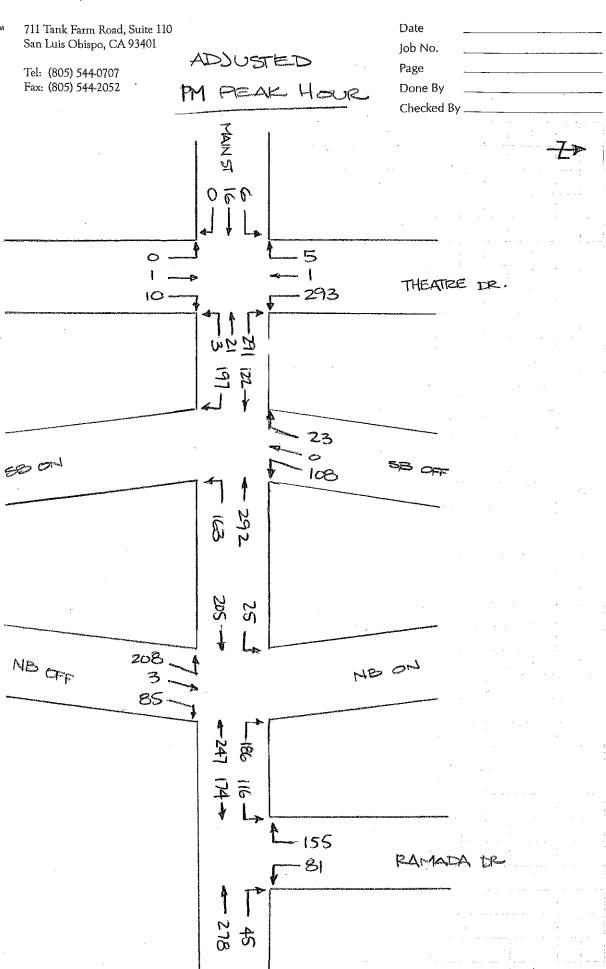
| 33 | |
|----|--|
| 3 | |

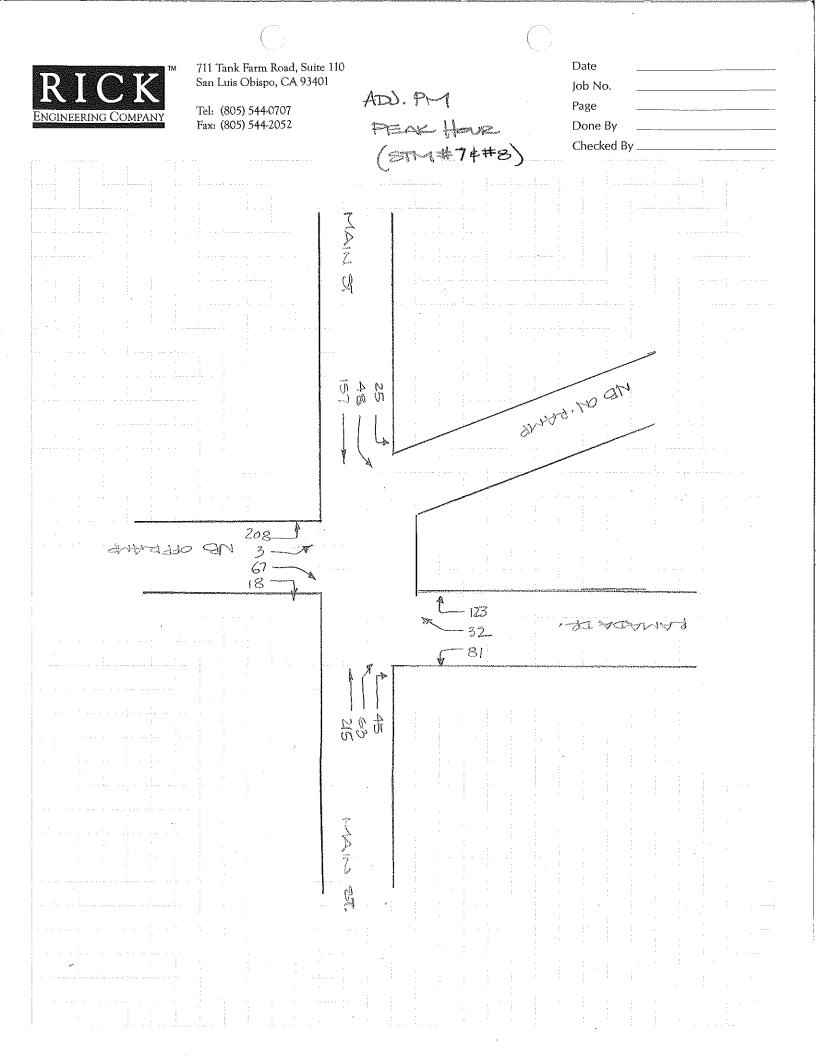




ł <u>go</u> 122







| | | | | | | | | | |)) F/ | |
|------------------|----------------------------|-------------|-------------|-------------|-------------|-------------------------|-------------|-------------|-------------|--------------|----|
| 9:18:11 | | Ц Ц | PRINT FILE | FOR RAMP | AADT | 2009 CALTRANS | 11221 | o rand | Ħ | | |
| | | | 05 | 05-SLO-101 | | | | | | | |
| P POST P MILE | P S DESCRIPTION | 2000 ADT | 2001 ADT | 2002 ADT | 2003 ADT | 200 4 ADT | 2005 ADT | 2006 Adt | 2007 ADT | 2008 ADT | •• |
| 049.120 | SAN RAMON NE OFF | μ | 850 | | | 860 | | | 1280 | | |
| 049.190 | SAN RAMON SB ON | | 750 | | | 750 | | | 1040 | | |
| 049.250 | SAN RAMON NB ON | | 2600 | | | 1800 | | | 2320 | | |
| 049.300 | SAN RAMON SB OFF | | 1250 | | | 1430 | | | 1870 | | |
| 050.480 | VINEYARD SB ON | | 3500 | | | 3930 | | | 4620 | | |
| 050.510 | VINEYARD NB OFF | | 3700 | | | 4030 | | | 4810 | | |
| 050.630 | VINEYARD SB OFF | | 1050 | | | 1480 | | | 1560 | | |
| 050.770 | VINEYARD NB ON | | 1200 | | | 1400 | | | 1760 | | |
| 051.310 | LAS TABLAS SB ON | | 2700 | | | 3180 | | | 3530 | | |
| 051.350 | LAS TABLAS NB OFF | | 2950 | | | 3150 | | | 3520 | | |
| 051.560 | LAS TABLAS SB OFF | | 2850 | | | 3400 | | | 3260 | | |
| 051.600 | LAS TABLAS NB ON | | 3000 | | | 3530 | | | 3260 | | |
| 052.340 | MAIN SB ON | | 3000 | | | 3800 | | | 4270 | 124 | |
| 052.350 | MAIN NB OFF | | 2750 | | | 3430 | | | 4270 4 5 | * 55% | |
| 052.590 | MAIN NB ON | | 1800 | | | 1900 | | | 1860 V | | |
| 052.620 | MAIN SB OFF | | 1950 | | | 2000 | | | 2140 | | |
| 053.956 | S JCT 101/46 SB ON | | | | | 1130 | | | • | 1100 | |
| 053.980 | S JCT 101/46 NB OFF | | 1500 | | | 1800 | | | | 2350 | |
| 054.260 | S JCT 101/46 SB OFF | | 5350 | | | 6550 | | | | 7000 | |
| 054.270 | S JCT 101/46 NB ON | | 5300 | | | 6530 | | | | 6700 | |
| 055.288 | S PASO ROBLES NE OFF | | 11200 | | | | | | | 12000 | |
| 055.650 | SO PASO ROBLES NB OFF RAMP | | | | | 12900 | | | | مر | |

ADT

| | | | | | | BACK PEAK LHOUR | BACK PEAK MANTH | BACK | AHEAD PEAK | AHEAD FEAK MONTH | AHEAD AADT | |
|----------|------------|------------|---|------------------|---|-----------------------|-----------------------|------------------|----------------|------------------------|------------------|--|
| | 101 | SLO | | 12.521 | ARROYO GRANDE, BRIDGE ST INTERCHANGE | 6,000 | 55,000 | 51,000 | 5,800 | 52,000 | 48,000 | |
| 05 | 101 | SLO | | 13.173 | ARROYO GRANDE, JCT. RTE. 227 N, GRAND AVE | 5,800 | 52,000 | 48,000 | 6,500 | 57,000 | 53,000 | |
| | 101 | SLO | | 13.747 | ARROYO GRANDE, BRISCO RD INTERCHANGE | 6,500 | 57,000 | 53,000 | 6,900 | 60,000 | 56,000 | |
| | 101 | SLO | | 14.613 | PISMO BEACH, OAK PARK RD INTERCHANGE | 6,900 | 60,000 | 56,000 | 8,400 | 72,000 | 67,000 | |
| | 101 | SLO | | 15.579 | PISMO BEACH, PISMO OAKS INTERCHANGE | 8,400 | 72,000 | 67,000 | 8,400 | 71,000 | 66,000 | |
| | 101 | SLO | | 16.398 | PISMO BEACH, SOUTH PISMO BEACH (VILLA CREEK) | 8,400 | 71,000 | 66,000 56,000 | 7,100 | 60,000 | 56,000 58,500 | |
| 05 | 101 | SLO | Б | 17.756 | PISMO BEACH, JCT. RTE. 1 SOUTH | 7,100 7,300 | 60,000 | 56,000 | 7,300 | 63,000 70,000 | 58,500 | |
| | 101 | SLO | R | 19.812 | NORTH SHELL BEACH INTERCHANGE AVILA RD INTERCHANGE | 7,300 7,400 | 63,000 | 58,500 | 7,400 | 70,000 | 64,000 62,000 | |
| | 101 101 | SLO SLO | R | 21.105 22.289 | NORTH AVILA RD INTERCHANGE | 7,400 7,000 | 70,000 68,000 | 64,000 62,000 | 7,000 7,000 | 68,000 71,000 | 65,000 | |
| 05 05 | 101 | SLO | R | 22.209 | SANTA FE | 7,000 | 71,000 | 65,000 | 6,200 | 68,000 | 60,000 | |
| | 101 | SLO | N | 25.911 | SAN LUIS OBISPO, LOS OSOS RD | 6,200 | 68,000 | 60,000 | 5,700 | 62,000 | 56,000 | |
| | 101 | SLO | | 27.501 | SAN LUIS OBISPO, MADONNA RD | 5,700 | 62,000 | 56,000 | 6,300 | 67,000 | 62,000 | |
| | 101 | SLO | | 28.088 | SAN LUIS OBISPO, JCT. RTE. 227, MARCH ST | 6,300 | 67,000 | 62,000 | 5,600 | 60,000 | 55,000 | |
| | 101 | SLO | | 29.067 | SAN LUIS OBISPO, JCT. RTE. 1 NORTH | 5,600 | 60,000 | 55,000 | 4,700 | 49,000 | 45,000 | |
| | 101 | SLO | | 29.375 | SAN LUIS OBISPO, CALIFORNIA BLVD INTERCHANGE | 4,700 | 49,000 | 45,000 | 4,200 | 44,000 | 40,000 | |
| | 101 | SLO | | 29.767 | SAN LUIS OBISPO, GRAND AVE INTERCHANGE | 4,200 | 44,000 | 40,000 | 3,900 | 40,000 | 37,000 | |
| 05 | 101 | SLO | | 29.985 | SAN LUIS OBISPO, BUENA VISTA INTERCHANGE | 3,900 | 40,000 | 37,000 | 4,600 | 48,000 | 43,000 | |
| 05 | 101 | SLO | | 30.36 | SAN LUIS OBISPO, NORTH CITY LIMITS | 4,600 | 48,000 | 43,000 | 4,700 | 48,000 | 43,000 | |
| 05 | 101 | SLO | | 37.863 | JCT. RTE. 58 EAST, SANTA MARGARITA | 4,700 | 48,000 | 43,000 | 4,600 | 47,000 | 42,000 | |
| 05 | 101 | SLO | | 42.268 | SANTA BARBARA RD INTERCHANGE | 4,600 | 47,000 | 42,000 | 4,600 | 48,000 | 43,000 | |
| 05 | 101 | SLO | | 44.008 | SANTA ROSA RD INTERCHANGE | 4,600 | 48,000 | 43,000 | 5,200 | 54,000 | 49,000 | |
| 05 | 101 | SLO | | 44.841 | CURBARIL AVE INTERCHANGE | 5,200 | 54,000 | 49,000 | 5,600 | 58,000 | 53,000 | |
| 05 | 101 | SLO | | 45.572 | ATASCADERO, JCT. RTE. 41 | 5,400 | 58,000 | 53,000 | 6,200 | 66,000 | 60,000 | |
| 05 | 101 | SLO | | 45.957 | TRAFFIC WAY INTERCHANGE | 6,200 | 66,000 | 60,000 | 6,200 | 66,000 | 60,000 | |
| 05 | 101 | SLO | | 46.867 | SAN ANSELMO RD INTERCHANGE | 6,200 | 66,000 | 60,000 | 5,900 | 63,000 | 58,000 | |
| 05 | 101 | SLO | | 48.331 | DEL RIO RD INTERCHANGE | 5,900 | 63,000 | 58,000 | 6,100 | 65,000 | 60,000 | |
| 05 | 101 | SLO | | 49.319 | SAN RAMON RD INTERCHANGE | 6,100 | 65,000 | 60,000 | 6,300 | 67,000 | 62,000 | |
| 05 | 101 | SLO | | 50.644 | VINEYARD DR INTERCHANGE | 6,300 | 67,000 | 62,000 | 5,800 | 61,000 | 57,000 | |
| 05 | 101 | SLO | | 51.447 | LAS TABLAS AVE INTERCHANGE | 5,800 | 61,000 | 57,000 | 5,800 | 60,000 | 57,000 | |
| 05 | 101 | SLO | | 52.44 | TEMPLETON, MAIN ST | 5,800 | 60,000 | 57,000 | 5,700 | 58,000 | 54,000 | |
| 05 | 101 | SLO | | 54.116 | JCT. RTE. 46 WEST | 5,700 | 58,000 | 54,000 | 6,400 | 63,000 | 61,000 | |
| 05 | 101 | SLO | | 55.674 | SOUTH PASO ROBLES INTERCHANGE | 6,400 | 63,000 | 61,000 | 4,000 | 38,000 | 37,000 | |
| 05 | 101 | SLO | | 56.88 | PASO ROBLES, 13TH ST INTERCHANGE | 4,000 | 38,000 | 37,000 | 3,300 | 31,000 | 30,000 | |
| 05 | 101 | SLO | | 57.92 | PASO ROBLES, JCT. RTE. 46 EAST | 3,300 | 31,000 | 30,000 | 2,600 | 24,000 | 23,000 | |
| 05 | 101 | SLO | | 58.762 | PASO ROBLES, NORTH PASO ROBLES INTERCHANGE | 2,600 | 24,000 | 23,000 | 2,600 | 25,000 | 23,000 | |
| 05 05 | 101 | SLO | | 60.98 63.735 | HUEY-EXLINE RD SAN MARCOS RD | 2,600 2,300 | 25,000 22,000 | 23,000 | 2,300 | 22,000 | 20,000 | |
| 05 05 | 101 101 | SLO SLO | | 63.735 65.082 | SAN MARCOS RD SOUTH SAN MIGUEL INTERCHANGE | 2,300 | 22,000 | 20,000 19,000 | 2,200 2,000 | 21,000 20,000 | 19,000 17,500 | |
| 05 05 | 101 | SLO | | 65.082 65.557 | SOUTH SAN MIGUEL INTERCHANGE SAN MIGUEL, 10TH ST INTERCHANGE | 2,200 | 20,000 | 19,000 | 2,000 | 20,000 | 17,500 | |
| 05 | 101 | SLO | | 67.228 | NORTH SAN MIGUEL INTERCHANGE | 2,000 | 20,000 | 17,000 | 2,000 | 20,000 | 17,000 | |
| 05 | 101 | SLO | R | 67.712 | SOUTH CAMP ROBERTS INTERCHANGE | 2,000 | 20,000 | 17,000 | 2,000 | 20,000 | 17,000 | |
| 05 | 101 | SLO | R | 69.322 | SAN LUIS OBISPO/MONTEREY COUNTY LINE | 2,000 | 20,000 | 17,400 | <u>_</u> ,000 | - 1,000 | 17,100 | |
| 05 | 101 | MON | R | 00.022 | SAN LUIS OBISPO/MONTEREY COUNTY LINE | _,000 | _,, | 113100 | 2,200 | 19,200 | 17,400 | |
| 05 | 101 | MON | R | 0.836 | CAMP ROBERTS INTERCHANGE | 2,200 | 19,200 | 17,400 | 2,200 | 21,900 | 16,700 | |
| 05 | 101 | MON | R | 2.153 | EAST GARRISON INTERCHANGE | 2,200 | 21,900 | 16,700 | 2,100 | 21,500 | 16,200 | |
| 05 | 101 | MON | R | 7.937 | NORTH BRADLEY INTERCHANGE | 2,100 | 21,500 | 16,200 | 2,050 | 21,000 | 15,600 | |
| 05 | 101 | MON | R | 9.667 | JOLON RD | 2,050 | 21,000 | 15,600 | 1,100 | 18,500 | 14,900 | |
| 05 | 101 | MON | R | 15.465 | SAN BERNARDO INTERCHANGE | 1,100 | 18,500 | 14,900 | 1,500 | 20,100 | 14,300 | |

| Location No | Road Name | Nearest Cross Stree | Date | ADT | AM Peak | AM Peak Volume | PM Peak | PM Peak Volume | Peak Da | Peak Day Volume |
|-------------|---------------------|--------------------------|-----------|-------|---------|----------------|---------|----------------|---------|-----------------|
| 2020 | Main St (Cambria) | E of Highway 1 | 14-Aug-07 | 3771 | 1100 | 344 | 1400 | 359 | Wed | 3850 |
| 2100 | Main St (Cambria) | E of Windsor Blvd | 17-Jun-10 | 6041 | 1100 | 497 | 1400 | 668 | Fri | 7050 |
| 2100 | Main St (Cambria) | E of Windsor Blvd | 14-Aug-07 | 6858 | 1100 | 578 | 1200 | 595 | Tues | 6980 |
| 2460 | Main St (Cambria) | W of Cambria Dr | 14-Aug-07 | 8855 | 1100 | 721 | 1200 | 772 | Thurs | 8985 |
| 2500 | Main St (Cambria) | W of Santa Rosa Creek Rd | 14-Aug-07 | 3545 | 1100 | 299 | 1200 | 369 | Thurs | 3666 |
| 2510 | Main St (Cambria) | E of Santa Rosa Creek Rd | 14-Aug-07 | 3509 | 1100 | 303 | 1500 | 355 | Wed | 3577 |
| 2520 | Main St (Cambria) | E of Burton Dr | 21-Aug-07 | 6483 | 1100 | 576 | 1200 | 601 | Wed | 6681 |
| 6200 | Main St (Cambria) | N of Eton Rd | 09-Sep-08 | 3385 | 800 | 375 | 1500 | 348 | Thurs | 3538 |
| 6800 | Main St (Cambria) | E of Pineknolls Dr | 30-Jul-06 | 10852 | 1130 | 994 | 1545 | 1257 | Fri | 12269 |
| 6800 | Main St (Cambria) | E of Pineknolls Dr | 12-Aug-07 | 10884 | 1100 | 1006 | 1500 | 1212 | Fri | 12202 |
| 6800 | Main St (Cambria) | E of Pineknolls Dr. | 07-Sep-08 | 7358 | 800 | 773 | 1500 | 903 | Fri | 8433 |
| 6800 | Main St (Cambria) | E of Pine Knolls Dr | 17-Jun-10 | 7483 | 1100 | 680 | 1500 | 924 | Fri | 8903 |
| 6800 | Main St (Cambria) | E of Pineknolls Dr. | 13-Sep-09 | 6970 | 1100 | 590 | 1500 | 892 | Fri | 8672 |
| 6810 | Main St (Cambria) | W of Burton Dr | 14-Aug-07 | 7780 | 1100 | 729 | 1200 | 769 | Tues | 7853 |
| 8611 | Main St (Cambria) | 0.20 mi N of Eton Rd | 12-Aug-07 | 1651 | 1100 | 96 | 1800 | 168 | Thurs | 1716 |
| 5390 | Main St (Templeton) | N of Creekside Ranch | 07-Jun-06 | 7700 | 700 | 667 | 1700 | 587 | Wed | 7700 |
| 5390 | Main St (Templeton) | S of Ramada Dr | 20-Sep-09 | 6836 | 1100 | 536 | 1500 | 717 | Tues | 7306 |
| 5750 | Main St (Templeton) | S of Vineyard Dr | 11-Sep-07 | 2687 | 700 | 697 | 1500 | 382 | Wed | 2988 |
| 5770 | Main St (Templeton) | N of Vineyard Dr | 15-Aug-06 | 6737 | 1115 | 596 | 1645 | 613 | Thurs | 6881 |
| 5770 | Main St (Templeton) | N of Vineyard Dr | 23-Sep-08 | 6479 | 800 | 616 | 1400 | 700 | Wed | 6608 |
| 5940 | Main St (Templeton) | N of Second St | 11-Sep-07 | 6874 | 700 | 529 | 1700 | 658 | Wed | 7229 |
| 7260 | Mallagh St | N of Tefft St | 26-Aug-08 | 868 | 800 | 143 | 1700 | 88 | Thurs | 962 |
| 7180 | Mary Ave | N of Tefft St | 30-Aug-09 | 4501 | 1100 | 330 | 1600 | 429 | Tues | 4600 |
| 7200 | Mary Ave | S of Tefft St | 03-Aug-09 | 2169 | 700 | 220 | 1700 | 242 | Fni | 2536 |
| 7210 | Mary Ave | N of Hill St | 06-Jun-10 | 1397 | 800 | 178 | 1200 | 176 | Fri | 1638 |
| 1150 | McMillan Canyon Rd | S of Highway 46 | 09-Sep-08 | 2086 | 600 | 294 | 1600 | 156 | Tues | 2239 |
| 7520 | McMillan Canyon Rd | N of SR (Highway) 46 | 08-Aug-06 | 252 | 006 | 32 | 1230 | 23 | Thurs | 292 |

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| Location No | Road Name | Nearest Cross Stree | Date | ADT | AM Peak | AM Peak Volume | PM Peak | PM Peak Volume | Peak Da | Peak Day Volume |
|-------------|-------------------|-----------------------------------|-----------|-------|---------|----------------|---------|----------------|---------|-----------------|
| 7000 | Pomeroy Rd | N of Willow Rd | 06-Jun-06 | 2135 | 700 | 242 | 1700 | 219 | Tues | 2135 |
| 9720 | Pomeroy Rd | N of Sandydale Dr | 06-Jun-06 | 11040 | 800 | 698 | 500 | 920 | Tues | 11040 |
| 5070 | Pozo Rd | E of Calf Canyon Highway | 25-Jul-06 | 1022 | 930 | 91 | 1600 | 26 | Wed | 1076 |
| 5070 | Pozo Rd | E of Calf Canyon Highway | 17-Jun-10 | 1112 | 1100 | 133 | 1600 | 124 | Sat | 1533 |
| 6880 | Pozo Rd | W of Carissa Highway | 01-Aug-06 | 47 | 1030 | 6 | 1445 | 8 | Thurs | 54 |
| 6880 | Pozo Rd | N of Santa Margarita Rd | 01-Aug-06 | 787 | 1115 | 66 | 1730 | 80 | Wed | 805 |
| 3580 | Prefumo Canyon Rd | 1.5 miles W of Los Osos Valley Rd | 11-Sep-07 | 298 | 700 | 30 | 1700 | 29 | Thurs | 323 |
| 3580 | Prefumo Canyon Rd | 1.5 miles W of Los Osos Valley Rd | 17-Jun-10 | 300 | 1100 | 30 | 1400 | 43 | Sun | 332 |
| 2000 | Price Canyon Rd | E of Lemoore St | 21-Aug-07 | 8416 | 700 | 686 | 1700 | 814 | Thurs | 8425 |
| 6560 | Price Canyon Rd | S of Highway 227 | 12-Aug-07 | 7256 | 700 | 677 | 1700 | 821 | Wed | 8525 |
| 6560 | Price Canyon Rd | S of Highway 227 | 17-Jun-10 | 6964 | 700 | 674 | 1700 | 805 | Thurs | 8222 |
| 6560 | Price Canyon Rd | S of Highway 227 | 13-Sep-09 | 6902 | 800 | 672 | 1700 | 810 | Fri | 8731 |
| 6560 | Price Canyon Rd | W of Ormande Rd | 25-Jul-06 | 8153 | 715 | 735 | 1630 | 854 | Wed | 8234 |
| 6560 | Price Canyon Rd | S of Highway 227 | 07-Sep-08 | 6652 | 800 | 700 | 1700 | 792 | Fri | 7117 |
| 6560 | Price Canyon Rd | S of Highway 227 | 30-Jul-06 | 7104 | 715 | 743 | 1630 | 852 | Thurs | 8308 |
| 2380 | Price St (Nipomo) | E of Thompson Ave | 28-Aug-07 | 1635 | 800 | 321 | 1500 | 245 | Thurs | 1882 |
| 4400 | Printz Rd | W of Highway 227 | 15-Aug-06 | 1020 | 1145 | 95 | 1700 | 76 | Wed | 1049 |
| 5000 | Quintana Rd | W of Chorro Creek Rd | 26-Sep-06 | 434 | 930 | 44 | 1400 | 52 | Tues | 447 |
| 7050 | Railroad St | S of Air Park Dr | 28-Aug-07 | 828 | 1100 | 66 | 1200 | 79 | Tues | 843 |
| 1350 | Ramada Dr | N of Main St | 28-Aug-07 | 4673 | 1000 | 416 | 1400 | 467 | Tues | 4727 |
| 1350 | Ramada Dr | N of Main St | 15-Sep-09 | 4835 | 1000 | 436 | 1200 | 444 | Wed | 5066 |
| 5400 | Ramada Dr | S of Highway 46 | 23-May-10 | 4115 | 1100 | 452 | 1200 | 514 | Fri | 5266 |
| 5400 | Ramada Dr | S of Highway 46 W | 08-Jun-06 | 3913 | 1100 | 348 | 1600 | 359 | Wed | 3913 |
| 5400 | Ramada Dr | S of Highway 46 | 13-Sep-09 | 3378 | 1100 | 387 | 1200 | 413 | TuesTu | TuesTues 4322 |
| 5400 | Ramada Dr | S of Highway 46 | 30-Jul-06 | 4014 | 1145 | 565 | 1200 | 520 | Mon | 5133 |
| 5400 | Ramada Dr | S of Highway 46 | 07-Sep-08 | 3907 | 1100 | 446 | 1200 | 475 | Thurs | 4943 |
| 5400 | Ramada Dr | S of Highway 46 | 19-Aug-07 | 3769 | 1100 | 472 | 1400 | 450 | Thurs | 4713 |
| | | | | | | | | | | |

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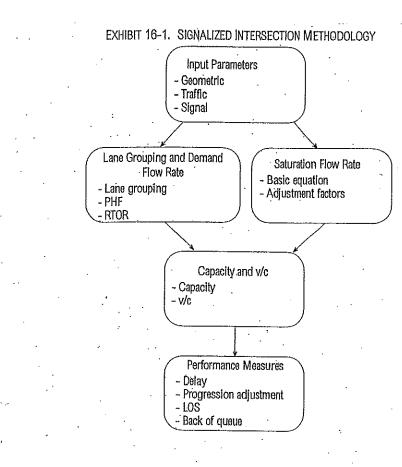
| Location No | Road Name | Nearest Cross Stree | Date | ADT | AM Peak | AM Peak Volume | PM Peak | PM Peak Volume | Peak Da | Peak Day Volume |
|-------------|----------------------------|-----------------------------|-----------|------|---------|----------------|---------|----------------|---------|-----------------|
| 3200 | Tenth St (Los Osos) | N of LOVR | 06-Jun-10 | 3293 | 1000 | 291 | 1400 | 338 | Fri | 3708 |
| 1260 | Tenth St (San Miguel) | W of Highway 101 | 15-Aug-06 | 517 | 645 | 57 | 1600 | 60 | Tues | 544 |
| 1480 | Tenth St (San Miguel) | E of K St | 28-Aug-07 | 1198 | 1100 | 83 | 1700 | 117 | Tues | 1320 |
| 1480 | Tenth St (San Miguel) | E of K St | 06-Jun-10 | 1070 | 1100 | 110 | 1500 | 103 | Fri | 1193 |
| 5030 | Theater Dr | S of Cemetery Rd | 11-Sep-07 | 7601 | 1100 | 580 | 1300 | 730 | Wed | 7663 |
| 5030 | Theater Dr | S of Cemetery Rd | 15-Sep-09 | 7857 | 1100 | 639 | 1500 | 744 | Tues | 7975 |
| 4520 | Thirteenth St (Oceano) | S of The Pike | 17-Jun-10 | 4985 | 1100 | 378 | 1600 | 485 | Fri | 5523 |
| 4810 | Thirteenth St (Oceano) | N of Highway 1 | 15-Aug-06 | 3058 | 1145 | 230 | 1630 | 288 | Tues | 3161 |
| 4290 | Thompson Ave | N of Highway 166 | 06-Jun-06 | 2589 | 700 | 322 | 1700 | 286 | Tues | 2589 |
| 4290 | Thompson Ave | N of Hwy 166 | 06-Jun-10 | 2698 | 700 | 246 | 1600 | 337 | Fri | 3305 |
| 4310 | Thompson Ave | E of northbound Highway 101 | 06-Jun-10 | 4834 | 700 | 571 | 1500 | 657 | Fri | 5914 |
| 4310 | Thompson Ave | E of northbound Highway 101 | 06-Jun-06 | 4688 | 700 | 674 | 1700 | 556 | Tues | 4688 |
| 4530 | Thompson Ave | N of Rancho Rd | 28-Aug-07 | 3260 | 700 | 309 | 1700 | 315 | Thurs | 3367 |
| 4660 | Thompson Ave | N of Tefft St | 30-Aug-09 | 5834 | 700 | 935 | 1200 | 661 | Fri | 7396 |
| 8600 | Thompson Ave | 150' N of Sheehy Rd | 15-Oct-06 | 4691 | 700 | 588 | 1700 | 425 | Thurs | 4999 |
| 3820 | Tiffany Ranch Rd | W of Orcutt Rd | 25-Jul-06 | 858 | 715 | 103 | 1630 | 98 | Wed | 875 |
| 1270 | Toro Creek Rd | N of Highway 41 | 25-Jul-06 | 341 | 800 | 33 | 1645 | 35 | Wed | 346 |
| 2750 | Toro Creek Rd | E of Highway 1 | 14-Aug-07 | 247 | 700 | 29 | 1700 | 26 | Tues | 267 |
| 8110 | Truesdale Rd | S of Clark Rd | 08-Aug-06 | 208 | 930 | 35 | 1445 | 24 | Tues | 247 |
| 3270 | Turri Rd | N of Los Osos Valley Rd | 25-Jul-06 | 414 | 1000 | 49 | 1445 | 50 | Tues | 449 |
| 4460 | Twenty-First St (Oceano) | N of SR-1 (Highway 1) | 25-Jul-06 | 851 | 1045 | 50 | 1715 | 107 | Wed | 874 |
| 9380 | Twenty-First St (Oceano) | N of Paso Robles St | 28-Aug-07 | 987 | 800 | 61 | 1400 | 105 | Thurs | 1018 |
| 7800 | Twenty-Second St (Oceano) | S of the Pike | 28-Aug-07 | 3002 | 800 | 204 | 1700 | 284 | Thurs | 3043 |
| 7800 | Twenty-Second St (Oceano) | S of the Pike | 26-Aug-08 | 2948 | 800 | 173 | 1700 | 283 | Tues | 2956 |
| 4090 | Twenty-Second St (Oceano) | N of Highway 1 | 10-Oct-06 | 1216 | 1130 | 96 | 1645 | 142 | Thurs | 1259 |
| 9180 | Twenty-Third St (Oceano) | N of Paso Robles St | 03-Oct-06 | 1394 | 800 | 151 | 1715 | 153 | Thurs | 1430 |
| 1080 | Union Rd | S of Highway 46 | 07-Jun-06 | 5032 | 700 | 407 | 1700 | 435 | Wed | 5032 |
| | | | | | | | | | | |

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APPENDIX B

2000 HCM LOS METHODOLOGY

Highway Capacity Manual 2000



LOS

The average control delay per vehicle is estimated for each lane group and aggregated for each approach and for the intersection as a whole. LOS is directly related to the control delay value. The criteria are listed in Exhibit 16-2.

| EXHIBIT 16-2. | LOS CRITERIA | FOR SIGNALIZED | INTERSECTIONS |
|---------------|--------------|----------------|---------------|
|---------------|--------------|----------------|---------------|

| . " | LOS · | Control Delay per Vehicle (s/veh) |
|-----|-------|-----------------------------------|
| · . | A | ≤ 10 |
| • | Β | > 10–20 |
| | C | > 2035 |
| | D | > 3555 |
| | E | > 55-80 |
| | F | > 80 |

LOS criteria

Chapter 16 - Signalized Intersections Methodology 16-2

Highway Capacity Manual 2000

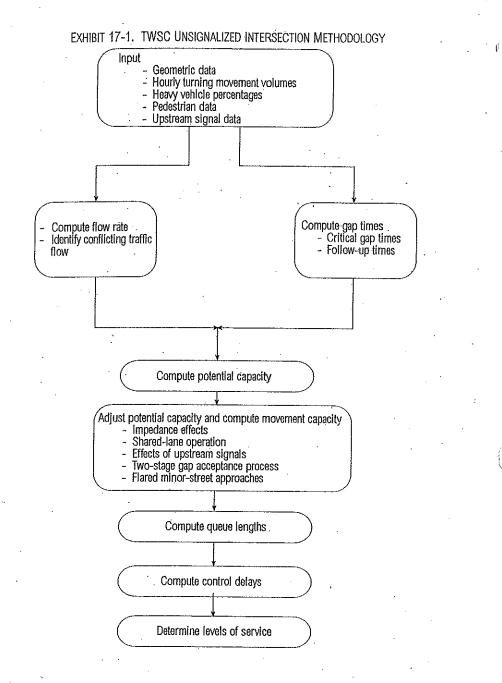
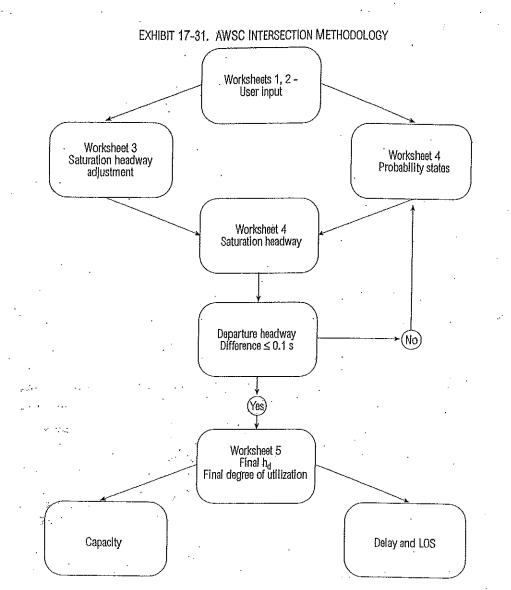


EXHIBIT 17-2. LEVEL-OF-SERVICE CRITERIA FOR TWSC INTERSECTIONS

| Level of Service | Average Control Delay (s/veh) |
|------------------|-------------------------------|
| A | 0–10 |
| . В | > 1015 |
| C C | > 15-25 |
| • D • | > 15–25 > 25–35 |
| . E | > 35–50 . |
| . F | > 50 |

Chapter 17 - Unsignalized Intersections Methodology - TWSC Intersections 17-2

Highway Capacity Manual 2000



LEVEL-OF-SERVICE CRITERIA

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The level-of-service criteria are given in Exhibit 17-22. The criteria for AWSC intersections have different threshold values than do those for signalized intersections primarily because drivers expect different levels of performance from distinct types of transportation facilities. The expectation is that a signalized intersection is designed to carry higher traffic volumes than an AWSC intersection. Thus a higher level of control delay is acceptable at a signalized intersection for the same LOS.

| Level of Service | Control Delay (s/veh) |
|------------------|-----------------------|
| A | 010 |
| В | > 10–15 |
| C · | >,1525 |
| D | > 25-35 |
| · E | > 3550 |
| . F | > 50 |

FXHIBIT 17-22 | EVEL-OF-SERVICE CRITERIA FOR AWSC INTERSECTIONS

APPENDIX C

SYNCHRO LOS DATA: EXISTING CONDITIONS

Existing AM Conditions 1: Main St. & Theatre Dr.

| | ٦ | - | \mathbf{r} | 4 | + | • | • | Ť | 1 | 1 | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | 4 | 1 | | 4 | |
| Volume (veh/h) | 5 | 28 | 0 | 2 | 21 | 198 | 0 | 2 | 5 | 229 | 1 | 8 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 6 | 31 | 0 | 2 | 23 | 220 | 0 | 2 | 6 | 254 | 1 | 9 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 243 | | | 31 | | | 189 | 290 | 31 | 184 | 180 | 133 |
| vC1, stage 1 conf vol | 2.10 | | | 0. | | | | 270 | 0. | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 243 | | | 31 | | | 189 | 290 | 31 | 184 | 180 | 133 |
| tC, single (s) | 4.2 | | | 4.2 | | | 7.2 | 6.6 | 6.3 | 7.2 | 6.6 | 6.3 |
| tC, 2 stage (s) | | | | | | | 7.2 | 0.0 | 0.0 | 7.2 | 0.0 | 0.0 |
| tF (s) | 2.3 | | | 2.3 | | | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free % | 100 | | | 100 | | | 100 | 100 | 99 | 66 | 100 | 99 |
| cM capacity (veh/h) | 1261 | | | 1513 | | | 735 | 599 | 1012 | 744 | 690 | 887 |
| | | | | | | | 100 | 0,77 | 1012 | , | 070 | 007 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 37 | 246 | 8 | 264 | | | | | | | | |
| Volume Left | 6 | 2 | 0 | 254 | | | | | | | | _ |
| Volume Right | 0 | 220 | 6 | 9 | | | | | | | | |
| cSH | 1261 | 1513 | 1417 | 748 | | | | | | | | |
| Volume to Capacity | 0.00 | 0.00 | 0.01 | 0.35 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0 | 0 | 40 | | | | | | | | |
| Control Delay (s) | 1.2 | 0.1 | 9.3 | 12.4 | | | | | | | | |
| Lane LOS | А | А | А | В | | | | | | | | |
| Approach Delay (s) | 1.2 | 0.1 | 9.3 | 12.4 | | | | | | | | |
| Approach LOS | | | А | В | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 6.2 | | | | | | | | | _ |
| Intersection Capacity Utiliza | ation | | 40.2% | IC | CU Level d | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing AM Conditions 2: Main St. & SB 101 Offramp

| | ٦ | - | \mathbf{r} | 4 | + | • | ٩. | Ť | 1 | 1 | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4Î | | | र्भ | | | | | | ર્સ | 1 |
| Volume (veh/h) | 0 | 121 | 141 | 82 | 207 | 0 | 0 | 0 | 0 | 168 | 0 | 14 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 134 | 157 | 91 | 230 | 0 | 0 | 0 | 0 | 187 | 0 | 16 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | 2 |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 230 | | | 291 | | | 633 | 625 | 213 | 625 | 703 | 230 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 230 | | | 291 | | | 633 | 625 | 213 | 625 | 703 | 230 |
| tC, single (s) | 4.2 | | | 4.2 | | | 7.2 | 6.6 | 6.3 | 7.2 | 6.6 | 6.3 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.3 | | | 2.3 | | | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free % | 100 | | | 92 | | | 100 | 100 | 100 | 48 | 100 | 98 |
| cM capacity (veh/h) | 1276 | | | 1210 | | | 349 | 358 | 800 | 360 | 322 | 783 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | | | | | | |
| Volume Total | 291 | 321 | 202 | | | | | | | | | |
| Volume Left | 0 | 91 | 187 | | | | | | | | | |
| Volume Right | 157 | 0 | 16 | | | | | | | | | |
| cSH | 1700 | 1210 | 390 | | | | | | | | | |
| Volume to Capacity | 0.17 | 0.08 | 0.52 | | | | | | | | | |
| Queue Length 95th (ft) | 0 | 6 | 72 | | | | | | | | | |
| Control Delay (s) | 0.0 | 2.8 | 24.1 | | | | | | | | | |
| Lane LOS | | А | С | | | | | | | | | |
| Approach Delay (s) | 0.0 | 2.8 | 24.1 | | | | | | | | | |
| Approach LOS | | | С | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.1 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 49.7% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing AM Conditions 3: Main St. & NB 101 Onramp

| | ٦ | - | \mathbf{i} | 4 | ← | • | 1 | t | 1 | 1 | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|--------------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्च | | | 4Î | | | ب | 1 | | | |
| Volume (veh/h) | 95 | 194 | 0 | 0 | 178 | 68 | 111 | 0 | 94 | 0 | 0 | 0 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 106 | 216 | 0 | 0 | 198 | 76 | 123 | 0 | 104 | 0 | 0 | 0 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 273 | | | 216 | | | 662 | 700 | 216 | 714 | 662 | 236 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 273 | | | 216 | | | 662 | 700 | 216 | 714 | 662 | 236 |
| tC, single (s) | 4.2 | | | 4.2 | | | 7.2 | 6.6 | 6.3 | 7.2 | 6.6 | 6.3 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.3 | | | 2.3 | | | 3.6 | 4.1 | 3.4 | 3.6 | 4.1 | 3.4 |
| p0 queue free % | 92 | | | 100 | | | 64 | 100 | 87 | 100 | 100 | 100 |
| cM capacity (veh/h) | 1256 | | | 1319 | | | 343 | 326 | 809 | 276 | 343 | 789 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | | | | | | | |
| Volume Total | 321 | 273 | 228 | | | | | | | | | |
| Volume Left | 106 | 0 | 123 | | | | | | | | | |
| Volume Right | 0 | 76 | 104 | | | | | | | | | |
| cSH | 1256 | 1700 | 634 | | | | | | | | | |
| Volume to Capacity | 0.08 | 0.16 | 0.36 | | | | | | | | | |
| Queue Length 95th (ft) | 7 | 0 | 41 | | | | | | | | | |
| Control Delay (s) | 3.2 | 0.0 | 16.1 | | | | | | | | | |
| Lane LOS | А | | С | | | | | | | | | |
| Approach Delay (s) | 3.2 | 0.0 | 16.1 | | | | | | | | | |
| Approach LOS | | | С | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 5.7 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 45.1% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing AM Conditions 4: Main St. & Ramada Dr.

| | ٦ | + | Ļ | × | * | ~ |
|------------------------------|-------|------|-------|------|-----------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | र्स | eî. | | ٦ | 1 |
| Volume (veh/h) | 111 | 177 | 186 | 122 | 40 | 60 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 123 | 197 | 207 | 136 | 44 | 67 |
| Pedestrians | 120 | .,, | 207 | 100 | •• | 01 |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | 2 |
| Median type | | None | None | | | 2 |
| Median storage veh) | | NULL | NULL | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 342 | | | | 718 | 274 |
| vC1, stage 1 conf vol | 342 | | | | /10 | 274 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 342 | | | | 718 | 274 |
| | 4.2 | | | | 6.4 | 6.2 |
| tC, single (s) | 4.Z | | | | 0.4 | 0.2 |
| tC, 2 stage (s) | 1 1 | | | | ЭΓ | 1 1 |
| tF (s) | 2.3 | | | | 3.5 | 3.3 |
| p0 queue free % | 90 | | | | 87 | 91 |
| cM capacity (veh/h) | 1184 | | | | 351 | 757 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 320 | 342 | 111 | | | |
| Volume Left | 123 | 0 | 44 | | | |
| Volume Right | 0 | 136 | 67 | | | |
| cSH | 1184 | 1700 | 877 | | | |
| Volume to Capacity | 0.10 | 0.20 | 0.13 | | | |
| Queue Length 95th (ft) | 9 | 0 | 11 | | | |
| Control Delay (s) | 3.8 | 0.0 | 12.8 | | | |
| Lane LOS | А | | В | | | |
| Approach Delay (s) | 3.8 | 0.0 | 12.8 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 3.4 | | | |
| Intersection Capacity Utiliz | ation | | 46.0% | IC | U Level o | of Service |
| Analysis Period (min) | | | 15 | | | 2 |
| | | | 10 | | | |

Existing PM Conditions 1: Main St. & Theatre Dr.

| | ۶ | - | * | • | + | • | • | 1 | 1 | * | ţ | ~ |
|-------------------------------|-------|------|-------|------|------------|-----------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | र्भ | 1 | | 4 | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 54 | 100 | 99 |
| cM capacity (veh/h) | 1196 | | | 1580 | | | 710 | 540 | 1052 | 707 | 666 | 850 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | 0.10 | | | | |
| | | | | | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| Volume Left | 7 | 3 | 0 | 326 | | | | | | | | _ |
| Volume Right | 0 | 323 | 11 | 6 | | | | | | | | |
| cSH Valuma ta Canasitu | 1196 | 1580 | 1157 | 709 | | | | | | | | _ |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.47 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0 | 1 | 63 | | | | | | | | _ |
| Control Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 | | | | | | | | |
| Lane LOS | A | A | A | B | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 | | | | | | | | |
| Approach LOS | | | А | В | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.0 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 49.3% | IC | CU Level o | f Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions 2: Main St. & SB 101 Offramp

| | ٦ | - | \mathbf{r} | 4 | - | • | ٩. | 1 | 1 | 1 | Ŧ | ~ |
|-----------------------------------|------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | eî 👘 | | | र्भ | | | | | | स | 1 |
| Volume (veh/h) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | 2 |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 85 | | | 100 | 100 | 100 | 44 | 100 | 96 |
| cM capacity (veh/h) | 1219 | | | 1188 | | | 203 | 223 | 786 | 215 | 192 | 710 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | | | | | | |
| Volume Total | 354 | 506 | 146 | | | | | | | | | |
| Volume Left | 0 | 181 | 120 | | | | | | | | | |
| Volume Right | 219 | 0 | 26 | | | | | | | | | |
| cSH | 1700 | 1188 | 261 | | | | | | | | | |
| Volume to Capacity | 0.21 | 0.15 | 0.56 | | | | | | | | | |
| Queue Length 95th (ft) | 0 | 13 | 78 | | | | | | | | | |
| Control Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Lane LOS | | А | Е | | | | | | | | | |
| Approach Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Approach LOS | | | E | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.2 | | | | | | | | | |
| Intersection Capacity Utilization | tion | | 58.9% | IC | CU Level c | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions 3: Main St. & NB 101 Onramp

| | ٨ | - | \mathbf{r} | 4 | + | * | • | 1 | 1 | * | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | | | ef 🗧 | | | र्भ | 1 | | | |
| Volume (veh/h) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 97 | | | 100 | | | 37 | 99 | 88 | 100 | 100 | 100 |
| cM capacity (veh/h) | 1076 | | | 1335 | | | 367 | 324 | 809 | 298 | 371 | 667 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | | | | | | | |
| Volume Total | 256 | 481 | 329 | | | | | | | | | |
| Volume Left | 28 | 0 | 231 | | | | | | | | | |
| Volume Right | 0 | 207 | 94 | | | | | | | | | |
| cSH | 1076 | 1700 | 488 | | | | | | | | | |
| Volume to Capacity | 0.03 | 0.28 | 0.67 | | | | | | | | | |
| Queue Length 95th (ft) | 2 | 0 | 124 | | | | | | | | | |
| Control Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Lane LOS | А | | D | | | | | | | | | |
| Approach Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Approach LOS | | | D | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 8.4 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 50.1% | IC | CU Level c | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions 4: Main St. & Ramada Dr.

| | ٦ | + | t | * | * | 4 |
|-----------------------------------|-------|------|-------|------|-----------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | स | 4 | | ٦ | 1 |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | 2 |
| Median type | | None | None | | | - |
| Median storage veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 359 | | | | 785 | 334 |
| vC1, stage 1 conf vol | 007 | | | | | 001 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 359 | | | | 785 | 334 |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | | | 0.1 | 0.2 |
| tF (s) | 2.2 | | | | 3.5 | 3.3 |
| p0 queue free % | 89 | | | | 72 | 76 |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 |
| Direction, Lane # | | | SB 1 | | 021 | , 00 |
| | EB 1 | WB 1 | | | | |
| Volume Total | 322 | 359 | 262 | | | |
| Volume Left | 129 | 0 | 90 | | | |
| Volume Right | 0 | 50 | 172 | | | |
| cSH | 1194 | 1700 | 936 | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Lane LOS | A | | В | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.5 | | | |
| Intersection Capacity Utilization | ation | | 47.4% | IC | U Level c | of Service |
| Analysis Period (min) | | | 15 | | | |

APPENDIX D

ACCIDENT DATA

| | Killed | 0 | 0 |
|---|--|---|---|
| | Injured | 1 | 0 |
| | Motor VehicleDir. ofMovement Prior toMovement Prior toPrimary ContributingInjuredKilledInvolved WithTravel 1Collision 1Travel 2Collision 2Factor | Influence of Alcohol 1 | Speeding |
| | Movement Prior to Collision 2 | | |
| | Dir. of Travel 2 | | |
| id Ramps: | Movement Prior to Collision 1 | Ran off road | Right turn |
| uthbour | Dir. of Travel 1 | South | South |
| North Main St. / US 101 Southbound Ramps: | | Overturn Fixed Object (Curb) South Ran off road | Hit Object Fixed Object (Curb) South Right turn |
| North Ma | Type of Collision | Overturn | Hit Object |
| | Dir. | 25' North | In int. |
| | Dist. | 25' | 0' In int. |
| | Cross Street | N. Main Street | N. Main Street |
| | Primary Street | 5/07 SB 101 Offramp | 10/07 SB 101 Onramp |
| | Date | 5/07 | 10/07 |
| | Accident Number | 1 | 2 |

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| Summation: | | | |
|-------------|-----|-------------|--|
| Broadside: | 0 | PDO: 1 | |
| Head on: | 0 | Injury: 1 | |
| Hit Object: | 1 | Fatality: 0 | |
| Overtumed: | - | Total: 2 | |
| Rear End: | . 0 | | |
| Sideswipe: | 0 | | |
| Total: | 2 | | |

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North Main St. / US 101 Northbound Ramps:

| | ğ | | | | | | | |
|--|--|-----------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|------------------------------------|------------------------------------|
| | d Kille | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Injure | 0 | 0 | 0 | | 1 | 0 | 0 |
| | Dir. of Movement Prior to Dir. of Movement Prior to Primary Contributing Injured Killed Travel 1 Collision 1 Travel 2 Collision 2 Factor | Improper Turn | Failure to Yield | Failure to Yield | Failure to Yield | Failure to Yield | Failure to Stop | Failure to Stop |
| | Movement Prior to Collision 2 | Straight | Straight | Straight | Straight | Straight | North Stopped in Road | North Stopped in Road |
| | Dir. of I Travel 2 | West | East | West | East | East | North | North |
| - | Movement Prior to Collision 1 | Left Turn | Right Turn | Left Tum | Left Turn | Left Tum | Straight | Straight |
| | Dir. of Travel 1 | East | North | North | North | North | North | North |
| * | Motor Vehicle Involved With | Sideswipe Other Motor Vehicle | Sideswipe Other Motor Vehicle North | Broadside Other Motor Vehicle North | Broadside Other Motor Vehicle North | Broadside Other Motor Vehicle North | Rear End Other Motor Vehicle North | Rear End Fixed Object (Curb) North |
| | Type of Collision | Sideswipe | Sideswipe | Broadside | Broadside | Broadside | Rear End | Rear End |
| | Dir. | In int. | In int. | 0' In int. | In int. | In int. | South | South |
| | Dist. | 0' In int. | 0' In int. | 0, | 0° In int. | 0 [°] In int. | 50' South | 50' South |
| | Cross Street | NB 101 Onramp | N. Main Street | N. Main Street | N. Main Street | N. Main Street | N. Main Street | N. Main Street |
| | Primary Street | Unk* N. Main Street NB 101 Onramp | Unk* NB 101 Offramp N. Main Street | Unk* NB 101 Offramp N. Main Street | Unk* NB 101 Offramp N. Main Street |
| And the state of t | Date | Unk* | Unk* | Unk* | Unk* | Unk* | Unk* | Unk* |
| | Accident Number | 3 | 4 | 5 | 6 | 7 | 8 | 6 |

* Date of individual accidents is unable to be known from data provided by Caltrans.

| | PDO: | Injury: | Fatality: | Total: | | | |
|------------|------------|----------|-------------|-------------|-----------|------------|--------|
| | ŝ | 0 | 0 | 0 | 7 | 2 | 7 |
| Summation: | Broadside: | Head on: | Hit Object: | Overturned: | Rear End: | Sideswipe: | Total: |

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| Killed | 0 | 0 | |
|---|-------------------|----------------------|---|
| Injured | 0 | 0 | |
| Dir. of Movement Prior to Dir. of Movement Prior to Primary Contributing Injured Killed Travel 1 Collision 1 Travel 2 Collision 2 Factor | Other than driver | Other than driver | |
| Dir. of Movement Prior to Travel 2 Collision 2 | | | |
| Dir. of Travel 2 | | | |
| Movement Prior to Collision 1 | Ran off road | Ran off road | |
| Dir. of Ma Travel 1 | South | West | |
| Motor Vehicle Involved With | Fixed Object | Fixed Object | |
| Type of Collision | Hit Object | Hit Object | |
| Dir. | North | West | |
| Dist. Dir. | 0' North | 8' West | |
| Cross Street | N. Main Street | Theatre Drive | |
| Primary Street | Theatre Drive | 10/09 N. Main Street | |
| Date | 1/02 | 10/09 | • |
| Accident Date F | 10 | 11 | C |

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| <u>Summation:</u> | | | |
|-------------------|---|-----------|-----|
| Broadside: | 0 | PDO: | 2 |
| Head on: | 0 | Injury: | 0 |
| Hit Object: | 6 | Fatality: | 0 |
| Overturned: | 0 | Total: | 2 |
| Rear End: | 0 | | • ! |
| Sideswipe: | 0 | | |
| Total: | 5 | | |
| | | | |

North Main St. / Ramada Drive:

| : | Killed | 0 | 0 | 0 | 0 | 0 |
|---|---|--|--|-------------------------------------|--|---|
| | Injured | 0 | 0 | 0 | 0 | 0 |
| | Dir. of Travel 1 Movement Prior to Collision 1 Movement Prior to Travel 2 Movement Prior to Collision 2 Primary Contributing Factor Injured Killed | Failure to Yield | Failure to Stop | Failure to Stop | Crossed Centerline | Unsafe Speed |
| | Movement Prior to Collision 2 | Straight | Left Tum | Left Turn | Straight | Left Turn |
| | Dir. of Travel 2 | West | East | East | South | East |
| | Dir. of Movement Prior to Dir. of Movement Prior Travel 1 Collision 1 Travel 2 Collision 2 | Left Turn | Straight | Straight | Cross Centerline | East Slowing/Stopping |
| | Dir. of Travel 1 | South | East | East | North | East |
| | Motor Vehicle Involved With | Broadside Other Motor Vehicle South | Rear End Other Motor Vehicle | Rear End Other Motor Vehicle | Sideswipe Other Motor Vehicle North Cross Centerline South | Rear End Other Motor Vehicle |
| | Type of Collision | Broadside | Rear End | Rear End | Sideswipe | Rear End |
| | Dir. | In int. | In int. | In int. | North | West |
| | Dist. Dir. | ,0 | .0 | 0' In int. | 267 | 20' |
| | Cross Street | N. Main Street | Ramada Drive | Ramada Drive | N. Main Street | Ramada Drive |
| | Primary Street | 12 5/07 Ramada Drive N. Main Street 0' In int. | 10/07 N. Main Street Ramada Drive 0' In int. | 14 3/09 N. Main Street Ramada Drive | 4/09 Ramada Drive N. Main Street 26' North | 16 11/09 N. Main Street Ramada Drive 20' West |
| | Date | 5/07 | 10/07 | 3/09 | 4/09 | 11/09 |
| | Accident Number | 12 | 13 | 14 | 15 | 16 |

| Summation: | Broadside: | Head on: | Hit Object: | Overturned: | Rear End: | Sideswipe: | Total: |
|------------|------------|----------|-------------|-------------|-----------|------------|--------|
|------------|------------|----------|-------------|-------------|-----------|------------|--------|

| S | 0 | 0 | Ś |
|------|---------|-----------|--------|
| PDO: | Injury: | Fatality: | Total: |
| | | | |
| | | | |
| | | | |

2 N N O O O I

North Main St. / Theatre Drive:

2/9/2011 Date 711 Tank Farm Road, Suite 110 San Luis Obispo, CA 93401 16128 Job No. Page Tel: (805) 544-0707 THEATRE DR/MAIN ST. ENGINEERING COMPANY RYAN HAYES Fax: (805) 544-2052 Done By ACCIDENT RATE Checked By THEATRE TRIVE! ACCIDENT RATE = # OF ACCIDENTS × (1×10) ENTERING VEHICLES & 365 PANE , # OF YEARS NUMBER & ACCIDENTS: 2 ENTERING VEHICLES: ASSUMED 10 × MAX PEAK HOUR VOLUMES UNLESS KNOWN *- 1/2 OF TOTAL COUNTED ADT THEATER DR. SB: 12(7857)=3930* THEATER DR. NE: 10×10 = 100 TOTAL = 7,760/DAY. MAIN ST. EFS: 33 × 10 = 3310 Main St. Was; 42×10 = 420 STUDY PERIOD: 1/1/07 -> 12/31/09 ACCIDENT RATE: 2×(1×10) = 0.23 ACC/MEV 7,760×366×3

2/9/2011 711 Tank Farm Road, Suite 110 Date San Luis Obispo, CA 93401 Job No. MAIN ST./SB 101 RAMPS Page Tel: (805) 544-0707 'ngineering Compan' Fax: (805) 544-2052 Done By EYAN HAYES ACCIDENT PATE Checked By SB 101 RAMPS: NUMBER OF ACCIDENTS: 2 ENTERING VEHICLES: ASSUMED 10 × MAX PEAK HOUR VOLUME UNLESS KNOWN MAIN ST. EB: 350 x10 = 3,500 TOTAL > 10,150 VEH. MAIN SF. WB! 451×10=4,510 101 SB OFFRAMP: 2,140 (FROM CALTRANS COUNTS) STUDY PERIOD: 1/1/07 -> 12/31/09 ACCIDENT RATE: 2× (1×106) = 0.18 Acc/MEV 10,100 × 365 × 3

2/9/2011 Date 711 Tank Farm Road, Suite 110 San Luis Obispo, CA 93401 Job No. 16128 MAIN ST/NB IOI RAMPS Page Tel: (805) 544-0707 Ingineering Company EMAN HAVES Fax: (805) 544-2052 Done By ACCIDENT RATE Checked By NB 101 RAMPS ! NUMBER OF ACCIDENTS: 7 ENTERING VEHICLES: ASSUMED 10 MAX PEAK HOUR VOLUME UNLESS KNOWN, MAIN ST. EB: 289×10 = 2,890 MAINS ST. WES 431 × 10 = 4,310 TOTAL = 11,470 VEH. 101 NB OFFRAME: 4,270 (FROM CAURANS COUNTS) STUDY PERIOD: 1/1/07 -> 12/31/09 ACCIDENT RATE: 7×(1×106) 0.56 Acc/MEN 11,470×365×3

2/9/2011 Date 711 Tank Farm Road, Suite 110 San Luis Obispo, CA 93401 Job No. RAMADA DR/MAIN ST. Page Tel: (805) 544-0707 ENGINEERING COMPAN RYAN HAYES Fax: (805) 544-2052 Done By ACCIDENT RATE Checked By RAMADA DR: NUMBER OF ACCIDENTS: 5 ENTERING VEHICLES : 10 x MAX PEAK HOUR UME UNLESS KAGUN * 1/2 OF TOTAL COUNTED ADT Ranada Dz: $\frac{1}{2}(4,835)^{*} = 2,420$ Main ST WB: $\frac{1}{2}(6,836)^{*} = 3,420$ (8,720 VEH. MAIN OF ER: 288×10 = 2,880 STUDY PERIOD: 1/1/07 -> 12/31/09 ACCIDENT RATE: 5× (1×106) = 0.52 ACC/MEV 8,720,365 × 3

APPENDIX E

SYNCHRO LOS DATA: NEAR-TERM MITIGATION MEASURES

Existing PM Conditions - STM #1 1: Main St. & Theatre Dr.

| | ۶ | - | \mathbf{i} | • | + | • | • | 1 | 1 | * | ţ | ~ |
|-------------------------------|-------|------|--------------|------|-----------|------------|------|------------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | <u>स</u> ् | 1 | | 4 | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.2 | 6.6 | 6.2 | 7.2 | 6.6 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 54 | 100 | 99 |
| cM capacity (veh/h) | 1196 | | | 1580 | | | 710 | 540 | 1052 | 707 | 666 | 850 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| Volume Left | 7 | 3 | 0 | 326 | | | | | | | | |
| Volume Right | 0 | 323 | 11 | 6 | | | | | | | | |
| cSH | 1196 | 1580 | 1157 | 709 | | | | | | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.47 | | | | | | | | |
| Queue Length 95th (ft) | 0.01 | 0.00 | 0.01 | 63 | | | | | | | | |
| Control Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 | | | | | | | | |
| Lane LOS | Α.2 | A | 0.0 A | В | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 | | | | | | | | |
| Approach LOS | 2.2 | 0.1 | A | B | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.0 | | | | | | | | | |
| Intersection Capacity Utiliza | ition | | 49.3% | IC | U Level r | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | 1 | | | |
| | | | 10 | | | | | | | | | |

Existing PM Conditions - STM #1 2: Main St. & SB 101 Offramp

| | ٨ | - | \mathbf{i} | • | + | • | • | 1 | 1 | 1 | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ¢Î | | | ŧ | | | | | | ŧ | 1 |
| Volume (veh/h) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | 2 |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.2 | 6.6 | 6.2 | 7.2 | 6.6 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 85 | | | 100 | 100 | 100 | 44 | 100 | 96 |
| cM capacity (veh/h) | 1219 | | | 1188 | | | 203 | 223 | 786 | 215 | 192 | 710 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | | | | | | |
| Volume Total | 354 | 506 | 146 | | | | | | | | | |
| Volume Left | 0 | 181 | 120 | | | | | | | | | |
| Volume Right | 219 | 0 | 26 | | | | | | | | | |
| cSH | 1700 | 1188 | 261 | | | | | | | | | |
| Volume to Capacity | 0.21 | 0.15 | 0.56 | | | | | | | | | |
| Queue Length 95th (ft) | 0 | 13 | 78 | | | | | | | | | |
| Control Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Lane LOS | 0.0 | A | E | | | | | | | | | |
| Approach Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Approach LOS | 0.0 | | E | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.2 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 58.9% | IC | CU Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions - STM #1 3: Main St. & NB 101 Onramp

| 6/27/2011 |
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|----------------------------------|------|----------|--------------|-------|-----------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ŧ | | | et. | | | र्स | 1 | | | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | | | | | | | | |
| Volume Total (vph) | 256 | 481 | 234 | 94 | | | | | | | | |
| Volume Left (vph) | 28 | 0 | 231 | 0 | | | | | | | | |
| Volume Right (vph) | 0 | 207 | 0 | 94 | | | | | | | | |
| Hadj (s) | 0.07 | -0.21 | 0.54 | -0.65 | | | | | | | | |
| Departure Headway (s) | 5.7 | 5.1 | 7.0 | 5.8 | | | | | | | | |
| Degree Utilization, x | 0.41 | 0.69 | 0.45 | 0.15 | | | | | | | | |
| Capacity (veh/h) | 593 | 681 | 482 | 584 | | | | | | | | |
| Control Delay (s) | 12.6 | 18.7 | 14.4 | 8.6 | | | | | | | | |
| Approach Delay (s) | 12.6 | 18.7 | 12.8 | | | | | | | | | |
| Approach LOS | В | С | В | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 15.4 | | | | | | | | | |
| HCM Level of Service | | | С | | | | | | | | | |
| Intersection Capacity Utilizatio | n | | 50.1% | IC | U Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #1 4: Main St. & Ramada Dr.

| | ٠ | → | Ļ | • | 1 | | |
|--------------------------------|------|------|-------|------|-----------|------------|--|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | | र्भ | f, | | 7 | 1 | |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 | |
| Sign Control | | Free | Free | | Stop | | |
| Grade | | 0% | 0% | | 0% | | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | 2 | |
| Median type | | None | None | | | _ | |
| Median storage veh) | | | | | | | |
| Upstream signal (ft) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 359 | | | | 785 | 334 | |
| vC1, stage 1 conf vol | 007 | | | | ,00 | 001 | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 359 | | | | 785 | 334 | |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | 0.1 | 0.2 | |
| tF (s) | 2.2 | | | | 3.5 | 3.3 | |
| p0 queue free % | 89 | | | | 72 | 76 | |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 | |
| | | | 05.4 | | 021 | , | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | |
| Volume Total | 322 | 359 | 262 | | | | |
| Volume Left | 129 | 0 | 90 | | | | |
| Volume Right | 0 | 50 | 172 | | | | |
| cSH | 1194 | 1700 | 936 | | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Lane LOS | А | | В | | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Approach LOS | | | В | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 5.5 | | | | |
| Intersection Capacity Utilizat | tion | | 47.4% | IC | U Level c | of Service | |
| Analysis Period (min) | | | 15 | | | | |

Existing PM Conditions - STM #2 1: Main St. & Theatre Dr.

| Movement Lane Configurations Volume (veh/h) | EBL | EBT | | | | | - | | - | | • | |
|---|----------|------|---------|------------|------------|------------|------|------|------|------|------|------|
| | | | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/h) | | \$ | | | \$ | | | र्स | 1 | | \$ | |
| | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.2 | 6.6 | 6.2 | 7.2 | 6.6 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 54 | 100 | 99 |
| cM capacity (veh/h) | 1196 | | | 1580 | | | 710 | 540 | 1052 | 707 | 666 | 850 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| | | | | | | | | | | | | |
| Volume Left | 7 | 3 | 0 11 | 326 | | | | | | | | _ |
| Volume Right | 0 | 323 | | 6 | | | | | | | | |
| cSH Volume te Canacitu | 1196 | 1580 | 1157 | 709 | | | | | | | | _ |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.47 | | | | | | | | |
| Queue Length 95th (ft) | 0 2.2 | 0 | 1 | 63 14 5 | | | | | | | | |
| Control Delay (s) | | 0.1 | 8.8 | 14.5 P | | | | | | | | |
| Lane LOS | A | A | A | B | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 P | | | | | | | | |
| Approach LOS | | | А | В | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.0 | | | | | | | | | |
| Intersection Capacity Utilization | | | 49.3% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #2 2: Main St. & SB 101 Offramp

| 6/27/2011 |
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|---------------------------------|-------|------|--------------|-------|-----------|------------|------|------|------|--------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ę. | | | ÷ | | | | | | र्स | 1 |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | SB 2 | | | | | | | | |
| Volume Total (vph) | 354 | 506 | 120 | 26 | | | | | | | | |
| Volume Left (vph) | 0 | 181 | 120 | 0 | | | | | | | | |
| Volume Right (vph) | 219 | 0 | 0 | 26 | | | | | | | | |
| Hadj (s) | -0.29 | 0.16 | 0.59 | -0.62 | | | | | | | | |
| Departure Headway (s) | 4.8 | 5.0 | 7.2 | 5.9 | | | | | | | | |
| Degree Utilization, x | 0.47 | 0.71 | 0.24 | 0.04 | | | | | | | | |
| Capacity (veh/h) | 718 | 703 | 452 | 543 | | | | | | | | |
| Control Delay (s) | 12.0 | 19.1 | 11.2 | 8.0 | | | | | | | | |
| Approach Delay (s) | 12.0 | 19.1 | 10.6 | | | | | | | | | |
| Approach LOS | В | С | В | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 15.4 | | | | | | | | | |
| HCM Level of Service | | | С | | | | | | | | | |
| Intersection Capacity Utilizati | on | | 58.9% | IC | U Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #2 3: Main St. & NB 101 Onramp

| | ٨ | - | \mathbf{F} | • | + | * | • | 1 | 1 | * | ţ | ~ |
|-------------------------------|-------|------|--------------|------|------------|------------|------|--------------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | 1 | | | |
| Volume (veh/h) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 97 | | | 100 | | | 37 | 99 | 88 | 100 | 100 | 100 |
| cM capacity (veh/h) | 1076 | | | 1335 | | | 367 | 324 | 809 | 298 | 371 | 667 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | | | | | | | |
| Volume Total | 256 | 481 | 329 | | | | | | | | | |
| Volume Left | 28 | 0 | 231 | | | | | | | | | |
| Volume Right | 0 | 207 | 94 | | | | | | | | | |
| cSH | 1076 | 1700 | 488 | | | | | | | | | |
| Volume to Capacity | 0.03 | 0.28 | 0.67 | | | | | | | | | |
| Queue Length 95th (ft) | 2 | 0 | 124 | | | | | | | | | |
| Control Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Lane LOS | А | | D | | | | | | | | | |
| Approach Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Approach LOS | | | D | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 8.4 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 50.1% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions - STM #2 4: Main St. & Ramada Dr.

| | ≯ | - | + | × | 1 | 4 |
|------------------------------|-----------|------|-------|------|-----------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | र्स | ¢Î | | ۲ | 1 |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | 2 |
| Median type | | None | None | | | 2 |
| Median storage veh) | | None | None | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 359 | | | | 785 | 334 |
| vC1, stage 1 conf vol | JJ7 | | | | 705 | 554 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 359 | | | | 785 | 334 |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 |
| | 4.1 | | | | 0.4 | 0.2 |
| tC, 2 stage (s) | 2.2 | | | | 3.5 | 3.3 |
| tF (s) | 2.2 89 | | | | 3.5 72 | 3.3 76 |
| p0 queue free % | | | | | | |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 322 | 359 | 262 | | | |
| Volume Left | 129 | 0 | 90 | | | |
| Volume Right | 0 | 50 | 172 | | | |
| cSH | 1194 | 1700 | 936 | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Lane LOS | А | | В | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.5 | | | |
| Intersection Capacity Utiliz | zation | | 47.4% | IC | U Level c | of Service |
| Analysis Period (min) | | | 15 | | | |
| | | | 10 | | | |

Existing PM Conditions - STM #3 1: Main St. & Theatre Dr.

| Movement Lane Configurations | EBL | | | | | | • | • | · · | | • | • |
|-----------------------------------|------|------|---------|-----------|------------|------------|------|------|------|------|------|------|
| Lane Configurations | | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| | | \$ | | | \$ | | | र्स | 1 | | \$ | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.2 | 6.6 | 6.2 | 7.2 | 6.6 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 54 | 100 | 99 |
| cM capacity (veh/h) | 1196 | | | 1580 | | | 710 | 540 | 1052 | 707 | 666 | 850 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | 0.10 | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| | | | | | | | | | | | | |
| Volume Left | 7 | 3 | 0 11 | 326 | | | | | | | | _ |
| Volume Right | 0 | 323 | | 6 | | | | | | | | |
| cSH Volume to Conseitu | 1196 | 1580 | 1157 | 709 | | | | | | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.47 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0 | 1 | 63 | | | | | | | | |
| Control Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 P | | | | | | | | |
| Lane LOS | A | A | A | B | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.8 | 14.5 P | | | | | | | | |
| Approach LOS | | | А | В | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.0 | | | | | | | | | |
| Intersection Capacity Utilization | l | | 49.3% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #3 2: Main St. & SB 101 Offramp

| 6/27/2011 |
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|---------------------------------|-------|------|--------------|-------|-----------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ę | | | र्च | | | | | | र्च | 1 |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | SB 2 | | | | | | | | |
| Volume Total (vph) | 354 | 506 | 120 | 26 | | | | | | | | |
| Volume Left (vph) | 0 | 181 | 120 | 0 | | | | | | | | |
| Volume Right (vph) | 219 | 0 | 0 | 26 | | | | | | | | |
| Hadj (s) | -0.29 | 0.16 | 0.59 | -0.62 | | | | | | | | |
| Departure Headway (s) | 4.8 | 5.0 | 7.2 | 5.9 | | | | | | | | |
| Degree Utilization, x | 0.47 | 0.71 | 0.24 | 0.04 | | | | | | | | |
| Capacity (veh/h) | 718 | 703 | 452 | 543 | | | | | | | | |
| Control Delay (s) | 12.0 | 19.1 | 11.2 | 8.0 | | | | | | | | |
| Approach Delay (s) | 12.0 | 19.1 | 10.6 | | | | | | | | | |
| Approach LOS | В | С | В | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 15.4 | | | | | | | | | |
| HCM Level of Service | | | С | | | | | | | | | |
| Intersection Capacity Utilizati | on | | 58.9% | IC | U Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #3 3: Main St. & NB 101 Onramp

| 6/27/2011 |
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|---------------------------------|------|-------|--------------|-------|-----------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ę | | | el 🕴 | | | Ę | 1 | | | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | | | | | | | | |
| Volume Total (vph) | 256 | 481 | 234 | 94 | | | | | | | | |
| Volume Left (vph) | 28 | 0 | 231 | 0 | | | | | | | | |
| Volume Right (vph) | 0 | 207 | 0 | 94 | | | | | | | | |
| Hadj (s) | 0.07 | -0.21 | 0.54 | -0.65 | | | | | | | | |
| Departure Headway (s) | 5.7 | 5.1 | 7.0 | 5.8 | | | | | | | | |
| Degree Utilization, x | 0.41 | 0.69 | 0.45 | 0.15 | | | | | | | | |
| Capacity (veh/h) | 593 | 681 | 482 | 584 | | | | | | | | |
| Control Delay (s) | 12.6 | 18.7 | 14.4 | 8.6 | | | | | | | | |
| Approach Delay (s) | 12.6 | 18.7 | 12.8 | | | | | | | | | |
| Approach LOS | В | С | В | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 15.4 | | | | | | | | | |
| HCM Level of Service | | | С | | | | | | | | | |
| Intersection Capacity Utilizati | on | | 50.1% | IC | U Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #3 4: Main St. & Ramada Dr.

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|------------------------------|-----------|------|-------|------|-----------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | र्स | ¢Î | | ۲ | 1 |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | 2 |
| Median type | | None | None | | | 2 |
| Median storage veh) | | None | None | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 359 | | | | 785 | 334 |
| vC1, stage 1 conf vol | JJ7 | | | | 705 | 554 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 359 | | | | 785 | 334 |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 |
| | 4.1 | | | | 0.4 | 0.2 |
| tC, 2 stage (s) | 2.2 | | | | 3.5 | 3.3 |
| tF (s) | 2.2 89 | | | | 3.5 72 | 3.3 76 |
| p0 queue free % | | | | | | |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 322 | 359 | 262 | | | |
| Volume Left | 129 | 0 | 90 | | | |
| Volume Right | 0 | 50 | 172 | | | |
| cSH | 1194 | 1700 | 936 | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Lane LOS | А | | В | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.5 | | | |
| Intersection Capacity Utiliz | zation | | 47.4% | IC | U Level c | of Service |
| Analysis Period (min) | | | 15 | | | |
| | | | 10 | | | |

Existing PM Conditions - STM #4 1: Main St. & Theatre Dr.

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|---|----------|------|--------------|------------|-----------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | ŧ | 1 | | \$ | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | 542 | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 54 | 100 | 99 |
| cM capacity (veh/h) | 1196 | | | 1580 | | | 710 | 540 | 1052 | 707 | 666 | 850 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| Volume Left | 7 | 300 | 0 | 332 326 | | | | | | | | |
| Volume Right | 0 | 323 | 11 | 520 | | | | | | | | |
| cSH | 1196 | 1580 | 1157 | 709 | | | | | | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.47 | | | | | | | | |
| 1 3 | 0.01 | 0.00 | | 63 | | | | | | | | |
| Queue Length 95th (ft) Control Delay (s) | 2.2 | 0.1 | 1 8.8 | 14.5 | | | | | | | | |
| Lane LOS | | A | | 14.5 B | | | | | | | | |
| Approach Delay (s) | A 2.2 | 0.1 | A 8.8 | ь 14.5 | | | | | | | | |
| Approach LOS | ۷.۷ | 0.1 | 0.0 A | 14.5 B | | | | | | | | |
| | | | ~ | | | | | | | | | |
| Intersection Summary | | | 7.0 | | | | | | | | | |
| Average Delay | tion | | | | | of Convios | | | ٨ | | | |
| Intersection Capacity Utiliza | | | 49.3% 15 | IC | O Level (| of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #4 2: Main St. & SB 101 Offramp

6/27/2011

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|-----------------------------------|------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | et | | | ŧ | | | | | | ŧ | 1 |
| Volume (veh/h) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | 2 |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | 409 | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 324 | | | 354 | | | 944 | 932 | 245 | 932 | 1041 | 324 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 100 | | | 85 | | | 100 | 100 | 100 | 44 | 100 | 96 |
| cM capacity (veh/h) | 1219 | | | 1188 | | | 203 | 223 | 786 | 215 | 192 | 710 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | | | | | | |
| Volume Total | 354 | 506 | 146 | | | | | | | | | |
| Volume Left | 0 | 181 | 120 | | | | | | | | | |
| Volume Right | 219 | 0 | 26 | | | | | | | | | |
| cSH | 1700 | 1188 | 261 | | | | | | | | | |
| Volume to Capacity | 0.21 | 0.15 | 0.56 | | | | | | | | | |
| Queue Length 95th (ft) | 0 | 13 | 78 | | | | | | | | | |
| Control Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Lane LOS | | А | E | | | | | | | | | |
| Approach Delay (s) | 0.0 | 4.1 | 35.5 | | | | | | | | | |
| Approach LOS | | | E | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 7.2 | | | | | | | | | |
| Intersection Capacity Utilization | tion | | 58.9% | IC | CU Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #4 3: Main St. & NB 101 Onramp

| 7/1/2011 |
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|-----------------------------------|------|--------------|--------------|------|-------------|------------|-------|-------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ् | | | ef 👘 | | | र्भ | 1 | | | |
| Volume (vph) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 15 | 15 | 15 | 16 | 16 | 16 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | | |
| Frt | | 1.00 | | | 0.94 | | | 1.00 | 0.85 | | | |
| Flt Protected | | 0.99 | | | 1.00 | | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | | 2018 | | | 1969 | | | 1758 | 1568 | | | |
| Flt Permitted | | 0.93 | | | 1.00 | | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | | 1896 | | | 1969 | | | 1758 | 1568 | | | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 61 | 0 | 0 | 0 | 71 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 256 | 0 | 0 | 420 | 0 | 0 | 234 | 23 | 0 | 0 | 0 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Turn Type | Perm | | | | | | Split | | Perm | | | |
| Protected Phases | | 2 | | | 2 | | 4 | 4 | | | | |
| Permitted Phases | 2 | | | | | | | | 4 | | | |
| Actuated Green, G (s) | | 16.6 | | | 16.6 | | | 7.9 | 7.9 | | | |
| Effective Green, g (s) | | 16.6 | | | 16.6 | | | 7.9 | 7.9 | | | |
| Actuated g/C Ratio | | 0.51 | | | 0.51 | | | 0.24 | 0.24 | | | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 968 | | | 1006 | | | 427 | 381 | | | |
| v/s Ratio Prot | | | | | c0.21 | | | c0.13 | | | | |
| v/s Ratio Perm | | 0.14 | | | | | | | 0.01 | | | |
| v/c Ratio | | 0.26 | | | 0.42 | | | 0.55 | 0.06 | | | |
| Uniform Delay, d1 | | 4.5 | | | 4.9 | | | 10.7 | 9.4 | | | |
| Progression Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.1 | | | 0.3 | | | 1.4 | 0.1 | | | |
| Delay (s) | | 4.6 | | | 5.2 | | | 12.2 | 9.5 | | | |
| Level of Service | | A | | | A | | | B | А | | 0.0 | _ |
| Approach Delay (s) | | 4.6 | | | 5.2 | | | 11.4 | | | 0.0 | |
| Approach LOS | | A | | | A | | | В | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 7.0 | Н | CM Level | of Service | • | | А | | | |
| HCM Volume to Capacity ratio | | | 0.46 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 32.5 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization | 1 | | 50.1% | IC | CU Level of | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Existing PM Conditions - STM #4 4: Main St. & Ramada Dr.

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|------------------------------|--------|------|-------|------|----------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | र्स | 4Î | | ሻ | 1 |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | 2 |
| Median type | | None | None | | | _ |
| Median storage veh) | | | | | | |
| Upstream signal (ft) | | 110 | | | | |
| pX, platoon unblocked | | 110 | | | 0.94 | |
| vC, conflicting volume | 359 | | | | 785 | 334 |
| vC1, stage 1 conf vol | 007 | | | | 700 | 001 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 359 | | | | 741 | 334 |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 |
| tC, 2 stage (s) | т. і | | | | 0.4 | 0.2 |
| tF (s) | 2.2 | | | | 3.5 | 3.3 |
| p0 queue free % | 89 | | | | 72 | 76 |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 |
| | | | | | JZT | 700 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 322 | 359 | 262 | | | |
| Volume Left | 129 | 0 | 90 | | | |
| Volume Right | 0 | 50 | 172 | | | |
| cSH | 1194 | 1700 | 936 | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Lane LOS | А | | В | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.5 | | | |
| Intersection Capacity Utiliz | vation | | 47.4% | IC | Ulevelo | of Service |
| Analysis Period (min) | | | 15 | | 0 201010 | |
| | | | 15 | | | |

Existing PM Conditions - STM #5 1: Main St. & Theatre Dr.

6/27/2011

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|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | र्भ | 1 | | \$ | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | 133 | | | | | | | |
| pX, platoon unblocked | 0.91 | | | | | | 0.91 | 0.91 | | 0.91 | 0.91 | 0.91 |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 237 | | | 18 | | | 108 | 278 | 18 | 108 | 101 | 60 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 58 | 100 | 99 |
| cM capacity (veh/h) | 1199 | | | 1580 | | | 778 | 566 | 1052 | 775 | 710 | 910 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| Volume Left | 7 | 3 | 0 | 326 | | | | | | | | |
| Volume Right | 0 | 323 | 11 | 6 | | | | | | | | |
| cSH | 1199 | 1580 | 1157 | 776 | | | | | | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.43 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0 | 1 | 54 | | | | | | | | |
| Control Delay (s) | 2.2 | 0.1 | 8.7 | 13.1 | | | | | | | | |
| Lane LOS | А | А | А | В | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.7 | 13.1 | | | | | | | | |
| Approach LOS | | | А | В | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 6.3 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 49.3% | IC | CU Level c | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions - STM #5 2: Main St. & SB 101 Offramp

| 7/1 | /2011 |
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|---|------|-------------|--------------|------|---------------|------------|------|----------|------|-------|-----------|--------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | | | र्भ | | | | | | र्च | 1 |
| Volume (vph) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 16 | 16 | 16 | 15 | 15 | 15 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | 4.0 |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | 1.00 |
| Frt | | 0.92 | | | 1.00 | | | | | | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 0.98 | | | | | | 0.95 | 1.00 |
| Satd. Flow (prot) | | 1880 | | | 1955 | | | | | | 1719 | 1538 |
| Flt Permitted | | 1.00 | | | 0.77 | | | | | | 0.95 | 1.00 |
| Satd. Flow (perm) | | 1880 | | | 1526 | | | | | | 1719 | 1538 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| RTOR Reduction (vph) | 0 | 86 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| Lane Group Flow (vph) | 0 | 269 | 0 | 0 | 505 | 0 | 0 | 0 | 0 | 0 | 120 | 4 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% |
| Turn Type | | - | | Perm | - | | | | | Split | - | Perm |
| Protected Phases | | 2 | | | 2 | | | | | 8 | 8 | |
| Permitted Phases | | 10.0 | | 2 | 10.0 | | | | | | | 8 |
| Actuated Green, G (s) | | 19.0 | | | 19.0 | | | | | | 4.3 | 4.3 |
| Effective Green, g (s) | | 19.0 | | | 19.0 | | | | | | 4.3 | 4.3 |
| Actuated g/C Ratio | | 0.61 | | | 0.61 | | | | | | 0.14 | 0.14 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 1141 | | | 926 | | | | | | 236 | 211 |
| v/s Ratio Prot | | 0.14 | | | -0.22 | | | | | | c0.07 | 0.00 |
| v/s Ratio Perm | | 0.24 | | | c0.33 0.55 | | | | | | 0.51 | 0.00 0.02 |
| v/c Ratio | | 0.24 2.8 | | | 0.55 3.6 | | | | | | 12.5 | 11.7 |
| Uniform Delay, d1 Progression Factor | | 2.8 | | | 3.0 1.00 | | | | | | 12.5 | 1.00 |
| Incremental Delay, d2 | | 0.1 | | | 0.7 | | | | | | 1.00 | 0.0 |
| Delay (s) | | 2.9 | | | 4.3 | | | | | | 14.2 | 11.7 |
| Level of Service | | 2.9 A | | | 4.3 A | | | | | | 14.2 B | B |
| Approach Delay (s) | | 2.9 | | | 4.3 | | | 0.0 | | | 13.8 | D |
| Approach LOS | | Α | | | ч.5 А | | | 0.0 A | | | 13.0 B | |
| Intersection Summary | | | | | | | | | | | _ | |
| HCM Average Control Delay | | | 5.2 | H | CM Level | of Servic | e | | А | | | |
| HCM Volume to Capacity ratio | | | 0.54 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 31.3 | S | um of lost | t time (s) | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 58.9% | | | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |
| | | | | | | | | | | | | |

Existing PM Conditions - STM #5 3: Main St. & NB 101 Onramp

6/27/2011

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|-------------------------------|-------|------|--------------|------|------------|------------|------|--------------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | 4 | 1 | | | |
| Volume (veh/h) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | 409 | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 481 | | | 228 | | | 661 | 764 | 228 | 710 | 661 | 378 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 97 | | | 100 | | | 37 | 99 | 88 | 100 | 100 | 100 |
| cM capacity (veh/h) | 1076 | | | 1335 | | | 367 | 324 | 809 | 298 | 371 | 667 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | | | | | | | | | |
| Volume Total | 256 | 481 | 329 | | | | | | | | | |
| Volume Left | 28 | 0 | 231 | | | | | | | | | |
| Volume Right | 0 | 207 | 94 | | | | | | | | | |
| cSH | 1076 | 1700 | 488 | | | | | | | | | |
| Volume to Capacity | 0.03 | 0.28 | 0.67 | | | | | | | | | |
| Queue Length 95th (ft) | 2 | 0 | 124 | | | | | | | | | |
| Control Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Lane LOS | А | | D | | | | | | | | | |
| Approach Delay (s) | 1.1 | 0.0 | 26.4 | | | | | | | | | |
| Approach LOS | | | D | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 8.4 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 50.1% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
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Existing PM Conditions - STM #5 4: Main St. & Ramada Dr.

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|------------------------------|-------|------|-------|------|------------|------------|--|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | | र्स | ¢Î | | ኘ | 1 | |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 | |
| Sign Control | | Free | Free | | Stop | | |
| Grade | | 0% | 0% | | 0% | | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | 2 | |
| Median type | | None | None | | | | |
| Median storage veh) | | | | | | | |
| Upstream signal (ft) | | 519 | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 359 | | | | 785 | 334 | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 359 | | | | 785 | 334 | |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 2.2 | | | | 3.5 | 3.3 | |
| p0 queue free % | 89 | | | | 72 | 76 | |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | |
| Volume Total | 322 | 359 | 262 | | | | |
| Volume Left | 129 | 0 | 90 | | | | |
| Volume Right | 0 | 50 | 172 | | | | |
| cSH | 1194 | 1700 | 936 | | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | | |
| Queue Length 95th (ft) | 9 | 0 | 29 | | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Lane LOS | А | | В | | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Approach LOS | | | В | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 5.5 | | | | |
| Intersection Capacity Utiliz | ation | | 47.4% | IC | CU Level o | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| 5 / | | | | | | | |

Existing PM Conditions - STM #6 1: Main St. & Theatre Dr.

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|-------------------------------|-------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | र्भ | 1 | | \$ | |
| Volume (veh/h) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | 2 | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | 133 | | | | | | | |
| pX, platoon unblocked | 0.94 | | | | | | 0.94 | 0.94 | | 0.94 | 0.94 | 0.94 |
| vC, conflicting volume | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 271 | | | 18 | | | 146 | 312 | 18 | 146 | 139 | 99 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 57 | 100 | 99 |
| cM capacity (veh/h) | 1197 | | | 1580 | | | 756 | 557 | 1052 | 752 | 695 | 890 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| Volume Left | 7 | 3 | 0 | 326 | | | | | | | | |
| Volume Right | 0 | 323 | 11 | 6 | | | | | | | | |
| cSH | 1197 | 1580 | 1157 | 754 | | | | | | | | |
| Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.44 | | | | | | | | |
| Queue Length 95th (ft) | 0 | 0.00 | 1 | 57 | | | | | | | | |
| Control Delay (s) | 2.2 | 0.1 | 8.7 | 13.5 | | | | | | | | |
| Lane LOS | A | A | A | В | | | | | | | | |
| Approach Delay (s) | 2.2 | 0.1 | 8.7 | 13.5 | | | | | | | | |
| Approach LOS | | | A | B | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 6.5 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 49.3% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | 10 | | | | | | | | | |

Existing PM Conditions - STM #6 2: Main St. & SB 101 Offramp

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|------------------------------------|------|------|--------------|------|------------|------------|------|------|------|-------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | | | र्भ | | | | | | र्च | 1 |
| Volume (vph) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 16 | 16 | 16 | 15 | 15 | 15 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | 4.0 |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | 1.00 |
| Frt | | 0.92 | | | 1.00 | | | | | | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 0.98 | | | | | | 0.95 | 1.00 |
| Satd. Flow (prot) | | 1880 | | | 1955 | | | | | | 1719 | 1538 |
| Flt Permitted | | 1.00 | | | 0.76 | | | | | | 0.95 | 1.00 |
| Satd. Flow (perm) | | 1880 | | | 1521 | | | | | | 1719 | 1538 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| RTOR Reduction (vph) | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 |
| Lane Group Flow (vph) | 0 | 286 | 0 | 0 | 505 | 0 | 0 | 0 | 0 | 0 | 120 | 4 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% |
| Turn Type | | | | Perm | | | | | | Split | | Perm |
| Protected Phases | | 2 | | | 2 | | | | | 4 | 4 | |
| Permitted Phases | | | | 2 | | | | | | | | 4 |
| Actuated Green, G (s) | | 34.3 | | | 34.3 | | | | | | 7.7 | 7.7 |
| Effective Green, g (s) | | 34.3 | | | 34.3 | | | | | | 7.7 | 7.7 |
| Actuated g/C Ratio | | 0.69 | | | 0.69 | | | | | | 0.15 | 0.15 |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | | | | 4.0 | 4.0 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 1290 | | | 1043 | | | | | | 265 | 237 |
| v/s Ratio Prot | | 0.15 | | | | | | | | | c0.07 | |
| v/s Ratio Perm | | 0.00 | | | c0.33 | | | | | | 0.45 | 0.00 |
| v/c Ratio | | 0.22 | | | 0.48 | | | | | | 0.45 | 0.02 |
| Uniform Delay, d1 | | 2.9 | | | 3.7 | | | | | | 19.2 | 17.9 |
| Progression Factor | | 1.00 | | | 0.94 | | | | | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.4 | | | 1.5 | | | | | | 1.2 | 0.0 |
| Delay (s) Level of Service | | 3.3 | | | 5.0 | | | | | | 20.5 | 18.0 |
| | | A | | | A | | | 0.0 | | | C | В |
| Approach Delay (s) Approach LOS | | 3.3 | | | 5.0 | | | 0.0 | | | 20.0 C | |
| •• | | А | | | A | | | A | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 6.6 | Н | CM Level | of Service | е | | А | | | |
| HCM Volume to Capacity ratio | | | 0.48 | _ | . . | | | | | | | |
| Actuated Cycle Length (s) | | | 50.0 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization | | | 58.9% | IC | U Level (| of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Existing PM Conditions - STM #6 3: Main St. & NB 101 Onramp

| 7/1 | /2011 |
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|-----------------------------------|------|------|--------------|------|------------|------------|----------|-------|------|------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | | | 4 | | | र्भ | 1 | | | |
| Volume (vph) | 25 | 205 | 0 | 0 | 247 | 186 | 208 | 3 | 85 | 0 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 15 | 15 | 15 | 16 | 16 | 16 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | | |
| Frt | | 1.00 | | | 0.94 | | | 1.00 | 0.85 | | | |
| Flt Protected | | 0.99 | | | 1.00 | | | 0.95 | 1.00 | | | |
| Satd. Flow (prot) | | 2018 | | | 1969 | | | 1758 | 1568 | | | |
| Flt Permitted | | 0.94 | | | 1.00 | | | 0.95 | 1.00 | | | |
| Satd. Flow (perm) | | 1904 | | | 1969 | | | 1758 | 1568 | | | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 28 | 228 | 0 | 0 | 274 | 207 | 231 | 3 | 94 | 0 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 43 | 0 | 0 | 0 | 72 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 256 | 0 | 0 | 438 | 0 | 0 | 234 | 22 | 0 | 0 | 0 |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% | 3% |
| Turn Type | Perm | | | | | | Split | | Perm | | | |
| Protected Phases | | 2 | | | 2 | | 4 | 4 | | | | |
| Permitted Phases | 2 | | | | | | | | 4 | | | |
| Actuated Green, G (s) | | 30.1 | | | 30.1 | | | 11.9 | 11.9 | | | |
| Effective Green, g (s) | | 30.1 | | | 30.1 | | | 11.9 | 11.9 | | | |
| Actuated g/C Ratio | | 0.60 | | | 0.60 | | | 0.24 | 0.24 | | | |
| Clearance Time (s) | | 4.0 | | | 4.0 | | | 4.0 | 4.0 | | | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | | |
| Lane Grp Cap (vph) | | 1146 | | | 1185 | | | 418 | 373 | | | |
| v/s Ratio Prot | | | | | c0.22 | | | c0.13 | | | | |
| v/s Ratio Perm | | 0.13 | | | | | | | 0.01 | | | |
| v/c Ratio | | 0.22 | | | 0.37 | | | 0.56 | 0.06 | | | |
| Uniform Delay, d1 | | 4.6 | | | 5.1 | | | 16.7 | 14.7 | | | |
| Progression Factor | | 1.07 | | | 1.00 | | | 1.00 | 1.00 | | | |
| Incremental Delay, d2 | | 0.4 | | | 0.9 | | | 1.6 | 0.1 | | | |
| Delay (s) | | 5.3 | | | 6.0 | | | 18.4 | 14.8 | | | |
| Level of Service | | A | | | A | | | B | В | | 0.0 | _ |
| Approach Delay (s) | | 5.3 | | | 6.0 | | | 17.4 | | | 0.0 | |
| Approach LOS | | A | | | A | | | В | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 9.3 | Н | CM Level | of Service | <u>;</u> | | А | | | |
| HCM Volume to Capacity ratio | | | 0.42 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 50.0 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utilization | 1 | | 50.1% | IC | U Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Existing PM Conditions - STM #6 4: Main St. & Ramada Dr.

| | ≯ | + | ł | • | * | ~ | |
|------------------------------|----------|------|----------|------|-----------|------------|--|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | | र्स | el el | | ٦ | 1 | |
| Volume (veh/h) | 116 | 174 | 278 | 45 | 81 | 155 | |
| Sign Control | | Free | Free | | Stop | | |
| Grade | | 0% | 0% | | 0% | | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Hourly flow rate (vph) | 129 | 193 | 309 | 50 | 90 | 172 | |
| Pedestrians | | | | | | | |
| Lane Width (ft) | | | | | | | |
| Walking Speed (ft/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | 2 | |
| Median type | | None | None | | | | |
| Median storage veh) | | | | | | | |
| Upstream signal (ft) | | 110 | | | | | |
| pX, platoon unblocked | | | | | 0.96 | | |
| vC, conflicting volume | 359 | | | | 785 | 334 | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 359 | | | | 755 | 334 | |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 2.2 | | | | 3.5 | 3.3 | |
| p0 queue free % | 89 | | | | 72 | 76 | |
| cM capacity (veh/h) | 1194 | | | | 321 | 706 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | |
| Volume Total | 322 | 359 | 262 | | | | |
| Volume Left | 129 | 0 | 90 | | | | |
| Volume Right | 0 | 50 | 172 | | | | |
| cSH | 1194 | 1700 | 935 | | | | |
| Volume to Capacity | 0.11 | 0.21 | 0.28 | | | | |
| Queue Length 95th (ft) | 9 | 0.21 | 29 | | | | |
| Control Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Lane LOS | 4.0 A | 0.0 | В | | | | |
| Approach Delay (s) | 4.0 | 0.0 | 14.8 | | | | |
| Approach LOS | | 0.0 | B | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 5.5 | | | | |
| Intersection Capacity Utiliz | zation | | 47.4% | IC | U Level o | of Service | |
| Analysis Period (min) | | | 15 | 10 | 2 2010/1 | | |
| | | | 10 | | | | |

Existing PM Conditions - STM #7 1: Main St. & Theatre Dr.

| | ≯ | - | \mathbf{r} | 1 | + | * | 1 | Ť | 1 | 1 | ţ | ~ |
|-----------------------------------|-------|--------------|--------------|-------|-------------|------------|--------|--------------|-----------|-------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | ÷ | | | ا | 1 | | \$ | |
| Volume (vph) | 6 | 16 | 0 | 3 | 21 | 291 | 0 | 1 | 10 | 293 | 1 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 10 | 10 | 10 | 16 | 16 | 16 | 13 | 13 | 13 | 13 | 13 | 13 |
| Total Lost time (s) | | 6.5 | | | 6.5 | | | 6.5 | 6.5 | | 6.5 | |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | 1.00 | 1.00 | | 1.00 | |
| Frt | | 1.00 | | | 0.88 | | | 1.00 | 0.85 | | 1.00 | |
| Flt Protected | | 0.99 | | | 1.00 | | | 1.00 | 1.00 | | 0.95 | |
| Satd. Flow (prot) | | 1666 | | | 1794 | | | 1870 | 1589 | | 1778 | |
| Flt Permitted | | 0.99 | | | 1.00 | | | 1.00 | 1.00 | | 0.95 | |
| Satd. Flow (perm) | | 1666 | | | 1794 | | | 1870 | 1589 | | 1778 | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 220 | 0 | 0 | 0 | 10 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 0 | 25 | 0 | 0 | 129 | 0 | 0 | 1 | 1 | 0 | 332 | 0 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% |
| Turn Type | Split | | | Split | | | Split | | Perm | Split | | |
| Protected Phases | 2 | 2 | | 8 | 8 | | 6 6 | 6 | 1 01111 | 4 | 4 | |
| Permitted Phases | _ | - | | U | U | | Ŭ | Ū | 6 | • | • | |
| Actuated Green, G (s) | | 14.4 | | | 35.1 | | | 9.7 | 9.7 | | 24.8 | |
| Effective Green, g (s) | | 14.4 | | | 35.1 | | | 9.7 | 9.7 | | 24.8 | |
| Actuated g/C Ratio | | 0.13 | | | 0.32 | | | 0.09 | 0.09 | | 0.23 | |
| Clearance Time (s) | | 6.5 | | | 6.5 | | | 6.5 | 6.5 | | 6.5 | |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | 3.0 | 3.0 | | 3.0 | |
| Lane Grp Cap (vph) | | 218 | | | 572 | | | 165 | 140 | | 401 | |
| v/s Ratio Prot | | c0.02 | | | c0.07 | | | 0.00 | 140 | | c0.19 | |
| v/s Ratio Perm | | 0.02 | | | 00.07 | | | 0.00 | c0.00 | | 00.17 | |
| v/c Ratio | | 0.11 | | | 0.23 | | | 0.01 | 0.01 | | 0.83 | |
| Uniform Delay, d1 | | 42.2 | | | 27.5 | | | 45.8 | 45.8 | | 40.6 | |
| Progression Factor | | 1.00 | | | 0.07 | | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | | 1.1 | | | 0.0 | | | 0.0 | 0.0 | | 13.2 | |
| Delay (s) | | 43.2 | | | 2.1 | | | 45.8 | 45.8 | | 53.8 | |
| Level of Service | | ч <u></u> .2 | | | A | | | 43.0 D | 43.0 D | | D | |
| Approach Delay (s) | | 43.2 | | | 2.1 | | | 45.8 | U | | 53.8 | |
| Approach LOS | | 43.2 D | | | A | | | 43.0 D | | | 00.0 D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 28.2 | Н | CM Level | of Service | e | | С | | | |
| HCM Volume to Capacity ratio | | | 0.36 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | S | um of losi | time (s) | | | 26.0 | | | |
| Intersection Capacity Utilization | | | 53.5% | IC | CU Level of | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Existing PM Conditions - STM #7 2: Main St. & SB 101 Offramp

| 6/29/ | 201 | 1 |
|-------|-----|---|
| 01271 | 201 | |

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|-----------------------------------|------|-------|---------------|------|-------------|------------|------|------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ef 👘 | | | र्भ | | | | | | र्च | 1 |
| Volume (vph) | 0 | 122 | 197 | 163 | 292 | 0 | 0 | 0 | 0 | 108 | 0 | 23 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 16 | 16 | 16 | 15 | 15 | 15 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | 6.5 | | | 6.5 | | | | | | 6.5 | 6.5 |
| Lane Util. Factor | | 1.00 | | | 1.00 | | | | | | 1.00 | 1.00 |
| Frt | | 0.92 | | | 1.00 | | | | | | 1.00 | 0.85 |
| Flt Protected | | 1.00 | | | 0.98 | | | | | | 0.95 | 1.00 |
| Satd. Flow (prot) | | 1880 | | | 1955 | | | | | | 1719 | 1538 |
| Flt Permitted | | 1.00 | | | 0.74 | | | | | | 0.95 | 1.00 |
| Satd. Flow (perm) | | 1880 | | | 1469 | | | | | | 1719 | 1538 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 0 | 136 | 219 | 181 | 324 | 0 | 0 | 0 | 0 | 120 | 0 | 26 |
| RTOR Reduction (vph) | 0 | 54 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 0 | 301 | 0 | 0 | 505 | 0 | 0 | 0 | 0 | 0 | 120 | 5 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% | 5% |
| Turn Type | | | | Perm | | | | | | Split | | Perm |
| Protected Phases | | 4 | | | 8 | | | | | 6 | 6 | |
| Permitted Phases | | 8 | | 8 | 8 | | | | | | | 6 |
| Actuated Green, G (s) | | 59.9 | | | 35.1 | | | | | | 9.7 | 9.7 |
| Effective Green, g (s) | | 59.9 | | | 35.1 | | | | | | 9.7 | 9.7 |
| Actuated g/C Ratio | | 0.54 | | | 0.32 | | | | | | 0.09 | 0.09 |
| Clearance Time (s) | | 6.5 | | | 6.5 | | | | | | 6.5 | 6.5 |
| Vehicle Extension (s) | | 3.0 | | | 3.0 | | | | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | | 1024 | | | 469 | | | | | | 152 | 136 |
| v/s Ratio Prot | | c0.07 | | | | | | | | | c0.07 | |
| v/s Ratio Perm | | 0.09 | | | c0.34 | | | | | | | 0.00 |
| v/c Ratio | | 0.29 | | | 1.08 | | | | | | 0.79 | 0.04 |
| Uniform Delay, d1 | | 13.6 | | | 37.4 | | | | | | 49.1 | 45.9 |
| Progression Factor | | 0.20 | | | 0.81 | | | | | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | | | 61.2 | | | | | | 23.2 | 0.1 |
| Delay (s) | | 2.9 | | | 91.4 | | | | | | 72.4 | 46.0 |
| Level of Service | | А | | | F | | | | | | E | D |
| Approach Delay (s) | | 2.9 | | | 91.4 | | | 0.0 | | | 67.7 | |
| Approach LOS | | А | | | F | | | А | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 56.7 | Н | CM Level | of Servic | e | | E | | | |
| HCM Volume to Capacity ratio | | | 0.76 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | S | um of lost | time (s) | | | 40.4 | | | |
| Intersection Capacity Utilization | | | 65.1% | IC | CU Level of | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Existing PM Conditions - STM #7 3: Main St. & Ramada Dr.

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|-----------------------------------|-------|-------|-------|-------|-----------|--------------|-------|--------------|------|------|-------|-------|
| Movement | EBL2 | EBL | EBT | WBT | WBR | WBR2 | NBL | NBT | NBR | NBR2 | SWL2 | SWL |
| Lane Configurations | | | र्भ | eî | | | | ب | 12 | | | ۳ |
| Volume (vph) | 25 | 48 | 157 | 215 | 63 | 45 | 208 | 3 | 67 | 18 | 81 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 15 | 12 | 15 | 16 | 16 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | | 6.5 | 6.5 | | | | 6.5 | 6.5 | | | 6.5 |
| Lane Util. Factor | | | 1.00 | 1.00 | | | | 1.00 | 1.00 | | | 1.00 |
| Frt | | | 1.00 | 0.96 | | | | 1.00 | 0.85 | | | 1.00 |
| Flt Protected | | | 0.98 | 1.00 | | | | 0.95 | 1.00 | | | 0.95 |
| Satd. Flow (prot) | | | 1960 | 1971 | | | | 1725 | 1568 | | | 1752 |
| Flt Permitted | | | 0.98 | 1.00 | | | | 0.95 | 1.00 | | | 0.95 |
| Satd. Flow (perm) | | | 1960 | 1971 | | | | 1725 | 1568 | | | 1752 |
| Peak-hour factor, PHF | 0.90 | 0.92 | 0.90 | 0.90 | 0.90 | 0.92 | 0.90 | 0.90 | 0.92 | 0.90 | 0.92 | 0.92 |
| Adj. Flow (vph) | 28 | 52 | 174 | 239 | 70 | 49 | 231 | 3 | 73 | 20 | 88 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 254 | 351 | 0 | 0 | 0 | 234 | 85 | 0 | 0 | 88 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 3% | 3% | 5% | 3% | 3% | 3% | 3% | 3% |
| Turn Type | Split | Split | | | | | Split | | Perm | | Split | |
| Protected Phases | 2 | 2 | 2 | 4 | | | 6 | 6 | | | 8 | 8 |
| Permitted Phases | _ | _ | _ | | | | - | - | 6 | | - | - |
| Actuated Green, G (s) | | | 22.4 | 25.7 | | | | 26.1 | 26.1 | | | 9.8 |
| Effective Green, g (s) | | | 22.4 | 25.7 | | | | 26.1 | 26.1 | | | 9.8 |
| Actuated g/C Ratio | | | 0.20 | 0.23 | | | | 0.24 | 0.24 | | | 0.09 |
| Clearance Time (s) | | | 6.5 | 6.5 | | | | 6.5 | 6.5 | | | 6.5 |
| Vehicle Extension (s) | | | 3.0 | 3.0 | | | | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | | | 399 | 460 | | | | 409 | 372 | | | 156 |
| v/s Ratio Prot | | | c0.13 | c0.18 | | | | c0.14 | 072 | | | c0.05 |
| v/s Ratio Perm | | | 00.10 | 00.10 | | | | 00.11 | 0.05 | | | 00.00 |
| v/c Ratio | | | 0.64 | 0.76 | | | | 0.57 | 0.23 | | | 0.56 |
| Uniform Delay, d1 | | | 40.1 | 39.3 | | | | 37.0 | 33.8 | | | 48.1 |
| Progression Factor | | | 1.34 | 1.00 | | | | 1.00 | 1.00 | | | 1.00 |
| Incremental Delay, d2 | | | 6.5 | 7.4 | | | | 1.9 | 0.3 | | | 4.6 |
| Delay (s) | | | 60.0 | 46.7 | | | | 39.0 | 34.2 | | | 52.7 |
| Level of Service | | | E | D | | | | D | C | | | D |
| Approach Delay (s) | | | 60.0 | 46.7 | | | | 37.6 | Ű | | | 49.9 |
| Approach LOS | | | E | D | | | | D | | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 47.7 | H | CM Leve | l of Service | | | D | | | |
| HCM Volume to Capacity ratio | | | 0.65 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.0 | S | um of los | t time (s) | | | 26.0 | | | |
| Intersection Capacity Utilization | ו | | 73.1% | | | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |
| | | | | | | | | | | | | |

6/29/2011

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| Movement | SWR | SWR2 |
|----------------------------|------|------|
| Lane Configurations | đ. | |
| Volume (vph) | 32 | 123 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Lane Width | 12 | 12 |
| Total Lost time (s) | 6.5 | |
| Lane Util. Factor | 1.00 | |
| Frt | 0.85 | |
| Flt Protected | 1.00 | |
| Satd. Flow (prot) | 1562 | |
| Flt Permitted | 1.00 | |
| Satd. Flow (perm) | 1562 | |
| Peak-hour factor, PHF | 0.92 | 0.92 |
| Adj. Flow (vph) | 35 | 134 |
| RTOR Reduction (vph) | 122 | 0 |
| Lane Group Flow (vph) | 47 | 0 |
| Heavy Vehicles (%) | 5% | 3% |
| Turn Type | Perm | |
| Protected Phases | | |
| Permitted Phases | 8 | |
| Actuated Green, G (s) | 9.8 | |
| Effective Green, g (s) | 9.8 | |
| Actuated g/C Ratio | 0.09 | |
| Clearance Time (s) | 6.5 | |
| Vehicle Extension (s) | 3.0 | |
| Lane Grp Cap (vph) | 139 | |
| v/s Ratio Prot | | |
| v/s Ratio Perm | 0.03 | |
| v/c Ratio | 0.34 | |
| Uniform Delay, d1 | 47.1 | |
| Progression Factor | 1.00 | |
| Incremental Delay, d2 | 1.4 | |
| Delay (s) | 48.5 | |
| Level of Service | D | |
| Approach Delay (s) | | |
| Approach LOS | | |
| · · | | |
| Intersection Summary | | |

Existing PM Conditions - STM #8 1: Main St. & Theatre Dr.

| Movement EBL EBT EBR WBL WBT WBL NBL NBL NBR SBL SBT Lane Configurations - | | ٦ | - | \mathbf{i} | 4 | ← | • | 1 | Ť | ۲ | 1 | ţ | ~ |
|---|-------------------------------|------|------|--------------|------|------------|------------|------|------|------|------|------|------|
| Volume (veh/n) 6 16 0 3 21 291 0 1 10 293 1 Sign Control Free Stop Stop Stop Stop O% | Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Volume (veh/n) 6 16 0 3 21 291 0 1 10 293 1 Sign Control Free Stop Stop Stop Stop O% | Lane Configurations | | \$ | | | \$ | | | र्स | 1 | | \$ | |
| Sign Control Free Free Stop Stop Grade 0% 111 326 1 1 1 326 1 1 1 326 1 1 1 326 1 1 1 326 1 1 1 326 1 1 1 326 1 1 1 326 1 1 3 1 1 1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | 6 | | 0 | 3 | 21 | 291 | 0 | | | 293 | | 5 |
| Grade 0% 0% 0% 0% 0% 0% Peak Hour Factor 0.90 Pedestrians Eare Width (ft) Walking Speed (ft/s) Percent Blockage T 133 T 18 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 0.94 <td></td> <td></td> <td>Free</td> <td></td> <td></td> <td>Free</td> <td></td> <td></td> <td>Stop</td> <td></td> <td></td> <td>Stop</td> <td></td> | | | Free | | | Free | | | Stop | | | Stop | |
| Hourly flow rate (vph) 7 18 0 3 23 323 0 1 11 326 1 Pedestrians Lane Width (ft) Walking Speed (ft/s) - <td></td> <td></td> <td>0%</td> <td></td> <td></td> <td>0%</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | 0% | | | 0% | | | | | | | |
| Pedestrians Lane Width (ft) Walking Speed (ft/s) Percent Blockage Right turn flare (veh) 2 Median storage veh) Upstream Signal (ft) Upstream Signal (ft) 133 pX, platoon unblocked 0.94 0.94 0.94 0.94 VC2, stage 1 conf vol vC2, stage 2 conf vol vC2 stage 2 conf vol vC2 stage 2 conf vol vC2 vC2, stage 2 conf vol vC2 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB1 WB1 SB1 Volume Left 7 3.0 326 Volume Right 0 323 11 6 cSH 157 Control 0.44 Queue Length 95th (ft) 0.00 0.01 157 Control 0.44 Queue Length 95th (ft) 0 0 1 57 Control 0.44 Queue Length 95th (ft) 0 0 1 <td< td=""><td>Peak Hour Factor</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td><td>0.90</td></td<> | Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Lane Width (ft) Walking Speed (ft/s) Percent Blockage Right turn flare (veh) Protein Lane (veh) None None None None None None None None | Hourly flow rate (vph) | 7 | 18 | 0 | 3 | 23 | 323 | 0 | 1 | 11 | 326 | 1 | 6 |
| Walking Speed (ft/s) Percent Blockage 2 Right rum flare (veh) 0.94 None 2 Median storage veh) 133 5 4 0.94 | Pedestrians | | | | | | | | | | | | |
| Percent Blockage None 2 Right turn flare (veh) None None Median storage veh) 133 0.94 | Lane Width (ft) | | | | | | | | | | | | |
| Percent Blockage None 2 Right turn flare (veh) None None Median storage veh) 133 0.94 | Walking Speed (ft/s) | | | | | | | | | | | | |
| Median type None None Median storage veh) 133 Upstream signal (II) 133 pX, platoon unblocked 0.94 0.94 0.94 0.94 0.94 vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage (S) 147 313 18 147 141 tC, single (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tF (s) 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 VSB VSB< | | | | | | | | | | | | | |
| Median type None None Median storage veh) 133 Upstream signal (ft) 133 pX, platoon unblocked 0.94 0.94 0.94 0.94 0.94 vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 3 18 147 313 18 147 141 tC, single (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tF (s) 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 V V Volume total 24 350 12 332 V V V V V V V V V V </td <td>Right turn flare (veh)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>2</td> <td></td> <td></td> <td></td> | Right turn flare (veh) | | | | | | | | | 2 | | | |
| Upstream signal (ft) 133 pX, platoon unblocked 0.94 0.94 0.94 0.94 0.94 0.94 vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vc2, stage 2 conf vol vc1, stage 1 conf vol vc2, stage 2 conf vol vc1, stage 1 conf vol </td <td></td> <td></td> <td>None</td> <td></td> <td></td> <td>None</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | | | None | | | None | | | | | | | |
| Upstream signal (ft) 133 pX, platoon unblocked 0.94 0.94 0.94 0.94 0.94 0.94 vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vc2, stage 2 conf vol vc1, stage 1 conf vol vc2, stage 2 conf vol vc1, stage 1 conf vol </td <td>Median storage veh)</td> <td></td> | Median storage veh) | | | | | | | | | | | | |
| vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, unblocked vol 273 18 147 313 18 147 141 tC, stage (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tC, 2 stage (s) 100 100 100 100 99 57 100 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 VOlume Total 24 350 12 332 Volume Total 24 350 12 332 1 6 5 Volume Right 0 323 11 6 5 Volume Right 0 13.5 Volume Right 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Volum | | | | | | 133 | | | | | | | |
| vC, conflicting volume 347 18 229 384 18 229 223 vC1, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC2, unblocked vol 273 18 147 313 18 147 141 tC, stage (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tC, 2 stage (s) 100 100 100 100 99 57 100 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 VOlume Total 24 350 12 332 Volume Total 24 350 12 332 1 6 5 Volume Right 0 323 11 6 5 Volume Right 0 13.5 Volume Right 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Volum | pX, platoon unblocked | 0.94 | | | | | | 0.94 | 0.94 | | 0.94 | 0.94 | 0.94 |
| vC2, stage 2 conf vol vCu, unblocked vol 273 18 147 313 18 147 141 tC, single (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tC, 2 stage (s) . <t< td=""><td></td><td>347</td><td></td><td></td><td>18</td><td></td><td></td><td>229</td><td>384</td><td>18</td><td>229</td><td>223</td><td>185</td></t<> | | 347 | | | 18 | | | 229 | 384 | 18 | 229 | 223 | 185 |
| vCu, unblocked vol 273 18 147 313 18 147 141 tC, single (s) 4.1 4.1 7.2 6.6 6.2 7.2 6.6 tC, 2 stage (s) . </td <td>vC1, stage 1 conf vol</td> <td></td> | vC1, stage 1 conf vol | | | | | | | | | | | | |
| tC, single (s) 4.1 7.2 6.6 6.2 7.2 6.6 tC, 2 stage (s) tF (s) 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 Volume Total 24 350 12 332 Volume Total 24 350 12 332 Volume Left 7 3 0 326 Volume Right 0 323 11 6 5 | | | | | | | | | | | | | |
| tC, 2 stage (s) tF (s) 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 Volume Total 24 350 12 332 Volume Total 24 350 12 332 Volume Left 7 3 0 326 Volume Right 0 323 11 6 - </td <td>vCu, unblocked vol</td> <td>273</td> <td></td> <td></td> <td>18</td> <td></td> <td></td> <td>147</td> <td>313</td> <td>18</td> <td>147</td> <td>141</td> <td>101</td> | vCu, unblocked vol | 273 | | | 18 | | | 147 | 313 | 18 | 147 | 141 | 101 |
| IF (s) 2.2 2.2 3.5 4.0 3.3 3.5 4.0 p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 Volume Total 24 350 12 332 Volume Total 24 350 12 332 | tC, single (s) | 4.1 | | | 4.1 | | | 7.2 | 6.6 | 6.2 | 7.2 | 6.6 | 6.2 |
| p0 queue free % 99 100 100 100 99 57 100 cM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 | tC, 2 stage (s) | | | | | | | | | | | | |
| CM capacity (veh/h) 1197 1580 755 557 1052 751 694 Direction, Lane # EB 1 WB 1 NB 1 SB 1 Volume Total 24 350 12 332 Volume Left 7 3 0 326 Volume Right 0 323 11 6 CSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B Intersection Summary 6.5 5 | tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| Direction, Lane # EB 1 WB 1 NB 1 SB 1 Volume Total 24 350 12 332 Volume Left 7 3 0 326 Volume Right 0 323 11 6 cSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B 11 13.5 Approach LOS A B B 11 13.5 Approach LOS A B B 11 13.5 Approach LOS A B B 14 15 | p0 queue free % | 99 | | | 100 | | | 100 | 100 | 99 | 57 | 100 | 99 |
| Volume Total 24 350 12 332 Volume Left 7 3 0 326 Volume Right 0 323 11 6 CSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B 1157 13.5 Approach LOS A B B 13.5 13.5 Approach LOS A B B 13.5 13.5 Approach LOS A B 13.5 13.5 Average Delay 6.5 6.5 13.5 | cM capacity (veh/h) | 1197 | | | 1580 | | | 755 | 557 | 1052 | 751 | 694 | 890 |
| Volume Left 7 3 0 326 Volume Right 0 323 11 6 cSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A A B Intersection Summary 6.5 6.5 | Direction, Lane # | EB 1 | WB 1 | NB 1 | SB 1 | | | | | | | | |
| Volume Right 0 323 11 6 cSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach Delay (s) 2.2 0.1 8.7 13.5 Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B Intersection Summary 6.5 5 | Volume Total | 24 | 350 | 12 | 332 | | | | | | | | |
| cSH 1197 1580 1157 753 Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A A B Intersection Summary 6.5 6.5 | Volume Left | 7 | 3 | 0 | 326 | | | | | | | | |
| Volume to Capacity 0.01 0.00 0.01 0.44 Queue Length 95th (ft) 0 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A A Approach Delay (s) 2.2 0.1 8.7 13.5 Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B Intersection Summary 6.5 6.5 | Volume Right | 0 | 323 | 11 | 6 | | | | | | | | |
| Queue Length 95th (ft) 0 1 57 Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B Intersection Summary 6.5 | cSH | 1197 | 1580 | 1157 | 753 | | | | | | | | |
| Control Delay (s) 2.2 0.1 8.7 13.5 Lane LOS A A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B B Intersection Summary 6.5 6.5 | Volume to Capacity | 0.01 | 0.00 | 0.01 | 0.44 | | | | | | | | |
| Lane LOS A A B Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B Intersection Summary 6.5 | Queue Length 95th (ft) | 0 | 0 | 1 | 57 | | | | | | | | |
| Approach Delay (s) 2.2 0.1 8.7 13.5 Approach LOS A B Intersection Summary 6.5 | Control Delay (s) | 2.2 | 0.1 | 8.7 | 13.5 | | | | | | | | |
| Approach LOS A B Intersection Summary Average Delay 6.5 | Lane LOS | А | А | А | В | | | | | | | | |
| Intersection Summary Average Delay 6.5 | | 2.2 | 0.1 | 8.7 | 13.5 | | | | | | | | |
| Average Delay 6.5 | Approach LOS | | | А | В | | | | | | | | |
| | Intersection Summary | | | | | | | | | | | | |
| Intersection Connective Utilization 40.20/ ICUL available Convice | Average Delay | | | | | | | | | | | | |
| | Intersection Capacity Utiliza | tion | | 49.3% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) 15 | Analysis Period (min) | | | 15 | | | | | | | | | |

Existing PM Conditions - STM #8 2: Main St. & SB 101 Offramp

| Volume (vph) 0 122 197 163 292 0 0 0 108 Ideal Flow (vphpl) 1900 < | Image: constraint of the system Image: constraint of the system 0 23 1900 2 12 0 5.0 0 5.0 1.00 0 0.85 0 1.00 0 0.85 5 1.00 9 1538 9 1538 15 1.00 9 1538 |
|---|--|
| Volume (vph) 0 122 197 163 292 0 0 0 108 Ideal Flow (vphpl) 1900 < | 0 23 0 1900 2 12 0 5.0 00 1.00 00 0.85 05 1.00 9 1538 9 1538 9 1538 |
| Ideal Flow (vphpl) 1900 <td>0 1900 2 12 0 5.0 00 1.00 00 0.85 05 1.00 9 1538 9 1538 9 1538</td> | 0 1900 2 12 0 5.0 00 1.00 00 0.85 05 1.00 9 1538 9 1538 9 1538 |
| Lane Width 16 16 16 15 15 12 13 13 13 13 13 13 14 14 | 2 12 0 5.0 0 1.00 0 0.85 5 1.00 9 1538 9 1538 9 1538 |
| Total Lost time (s) 5.0 5.0 5 Lane Util. Factor 1.00 1.00 1.0 Frt 0.92 1.00 1.0 Flt Protected 1.00 0.98 0.9 Satd. Flow (prot) 1880 1955 171 Flt Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 0 5.0 0 1.00 0 0.85 95 1.00 9 1538 95 1.00 9 1538 |
| Lane Util. Factor 1.00 1.00 1.00 Frt 0.92 1.00 1.00 Flt Protected 1.00 0.98 0.9 Satd. Flow (prot) 1880 1955 171 Flt Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 1.00 1.00 0 0.85 15 1.00 9 1538 15 1.00 9 1538 15 1.00 9 1538 |
| Frt 0.92 1.00 1.0 Flt Protected 1.00 0.98 0.9 Satd. Flow (prot) 1880 1955 171 Flt Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 0 0.85 95 1.00 9 1538 95 1.00 9 1538 |
| Flt Protected 1.00 0.98 0.9 Satd. Flow (prot) 1880 1955 171 Flt Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 25 1.00 9 1538 25 1.00 9 1538 |
| Satd. Flow (prot) 1880 1955 171 Flt Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 9 1538 9 1.00 9 1538 |
| Fit Permitted 1.00 0.75 0.9 Satd. Flow (perm) 1880 1492 171 | 9 1538 |
| Satd. Flow (perm) 1880 1492 171 | 9 1538 |
| | |
| | 0 0 0 0 |
| Peak-hour factor, PHF 0.90 0.90 0.90 0.90 0.90 0.90 0.90 0.9 | 0 0.90 |
| Adj. Flow (vph) 0 136 219 181 324 0 0 0 120 | 0 26 |
| RTOR Reduction (vph) 0 53 0 0 0 0 0 0 0 0 | 0 23 |
| Lane Group Flow (vph) 0 302 0 0 505 0 0 0 0 12 | 0 3 |
| Heavy Vehicles (%) 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% 5% | % 5% |
| Turn Type Perm Split | Perm |
| | 2 |
| Permitted Phases 8 | 2 |
| Actuated Green, G (s) 60.5 60.5 9 | .5 9.5 |
| Effective Green, g (s) 60.5 60.5 9 | .5 9.5 |
| Actuated g/C Ratio 0.76 0.76 0.1 | 2 0.12 |
| Clearance Time (s) 5.0 5.0 5 | .0 5.0 |
| Vehicle Extension (s) 3.0 3.0 3 | .0 3.0 |
| Lane Grp Cap (vph) 1422 1128 20 | 4 183 |
| v/s Ratio Prot 0.16 c0.0 | |
| v/s Ratio Perm c0.34 | 0.00 |
| v/c Ratio 0.21 0.45 0.5 | 0.02 |
| Uniform Delay, d1 2.8 3.6 33 | 4 31.1 |
| Progression Factor 1.00 1.22 1.0 | 0 1.00 |
| Incremental Delay, d2 0.1 0.9 4 | .3 0.0 |
| Delay (s) 2.9 5.3 37 | .7 31.2 |
| Level of Service A A | D C |
| Approach Delay (s) 2.9 5.3 0.0 36 | .5 |
| | D |
| Intersection Summary | |
| HCM Average Control Delay 9.0 HCM Level of Service A | |
| HCM Volume to Capacity ratio 0.47 | |
| Actuated Cycle Length (s) 80.0 Sum of lost time (s) 10.0 | |
| Intersection Capacity Utilization 61.4% ICU Level of Service B | |
| Analysis Period (min) 15 | |
| c Critical Lane Group | |

Existing PM Conditions - STM #8 3: Main St. & Ramada Dr.

| | ۶ | _# | - | + | • | ۲ | 1 | 1 | ۲ | 1 | 6 | ¥ |
|----------------------------------|-------|-------|-------|-------|-----------|--------------|-------|-------|------|------|-------|-------|
| Movement | EBL2 | EBL | EBT | WBT | WBR | WBR2 | NBL | NBT | NBR | NBR2 | SWL2 | SWL |
| Lane Configurations | | | र्स | ef 👘 | | | | र्स | 1 | | | - ከ |
| Volume (vph) | 25 | 48 | 157 | 215 | 63 | 45 | 208 | 3 | 67 | 18 | 81 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 15 | 12 | 15 | 16 | 16 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Total Lost time (s) | | | 6.5 | 6.5 | | | | 6.5 | 6.5 | | | 6.5 |
| Lane Util. Factor | | | 1.00 | 1.00 | | | | 1.00 | 1.00 | | | 1.00 |
| Frt | | | 1.00 | 0.95 | | | | 1.00 | 0.85 | | | 1.00 |
| Flt Protected | | | 0.98 | 1.00 | | | | 0.95 | 1.00 | | | 0.95 |
| Satd. Flow (prot) | | | 1959 | 1971 | | | | 1725 | 1568 | | | 1752 |
| Flt Permitted | | | 0.98 | 1.00 | | | | 0.95 | 1.00 | | | 0.95 |
| Satd. Flow (perm) | | | 1959 | 1971 | | | | 1725 | 1568 | | | 1752 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 28 | 53 | 174 | 239 | 70 | 50 | 231 | 3 | 74 | 20 | 90 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 0 | 255 | 352 | 0 | 0 | 0 | 234 | 82 | 0 | 0 | 90 |
| Heavy Vehicles (%) | 5% | 5% | 5% | 5% | 3% | 3% | 5% | 3% | 3% | 3% | 3% | 3% |
| Turn Type | Split | Split | | | | | Split | | Prot | | Split | |
| Protected Phases | 2 | 2 | 2 | 8 | | | 6 | 6 | 6 | | 4 | 4 |
| Permitted Phases | | | | | | | | | | | | |
| Actuated Green, G (s) | | | 13.5 | 18.6 | | | | 14.5 | 14.5 | | | 7.4 |
| Effective Green, g (s) | | | 13.5 | 18.6 | | | | 14.5 | 14.5 | | | 7.4 |
| Actuated g/C Ratio | | | 0.17 | 0.23 | | | | 0.18 | 0.18 | | | 0.09 |
| Clearance Time (s) | | | 6.5 | 6.5 | | | | 6.5 | 6.5 | | | 6.5 |
| Vehicle Extension (s) | | | 3.0 | 3.0 | | | | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | | | 331 | 458 | | | | 313 | 284 | | | 162 |
| v/s Ratio Prot | | | c0.13 | c0.18 | | | | c0.14 | 0.05 | | | c0.05 |
| v/s Ratio Perm | | | | | | | | | | | | |
| v/c Ratio | | | 0.77 | 0.77 | | | | 0.75 | 0.29 | | | 0.56 |
| Uniform Delay, d1 | | | 31.8 | 28.7 | | | | 31.0 | 28.3 | | | 34.7 |
| Progression Factor | | | 0.69 | 1.00 | | | | 1.00 | 1.00 | | | 1.00 |
| Incremental Delay, d2 | | | 10.3 | 11.7 | | | | 9.4 | 0.6 | | | 4.1 |
| Delay (s) | | | 32.2 | 40.4 | | | | 40.4 | 28.9 | | | 38.8 |
| Level of Service | | | С | D | | | | D | С | | | D |
| Approach Delay (s) | | | 32.2 | 40.4 | | | | 37.1 | | | | 36.6 |
| Approach LOS | | | С | D | | | | D | | | | D |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 36.9 | Н | CM Leve | I of Service | e | | D | | | |
| HCM Volume to Capacity ratio |) | | 0.73 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 80.0 | S | um of los | t time (s) | | | 26.0 | | | |
| Intersection Capacity Utilizatio | n | | 73.1% | IC | CU Level | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

6/29/2011

* t

| Movement | SWR | SWR2 |
|------------------------|----------|-------|
| Lane Configurations | <u> </u> | 01112 |
| Volume (vph) | 32 | 123 |
| Ideal Flow (vphpl) | 1900 | 1900 |
| Lane Width | 12 | 12 |
| Total Lost time (s) | 6.5 | |
| Lane Util. Factor | 1.00 | |
| Frt | 0.85 | |
| Flt Protected | 1.00 | |
| Satd. Flow (prot) | 1562 | |
| Flt Permitted | 1.00 | |
| Satd. Flow (perm) | 1562 | |
| Peak-hour factor, PHF | 0.90 | 0.90 |
| Adj. Flow (vph) | 36 | 137 |
| RTOR Reduction (vph) | 124 | 0 |
| Lane Group Flow (vph) | 49 | 0 |
| Heavy Vehicles (%) | 5% | 3% |
| Turn Type | Prot | |
| Protected Phases | 4 | |
| Permitted Phases | | |
| Actuated Green, G (s) | 7.4 | |
| Effective Green, g (s) | 7.4 | |
| Actuated g/C Ratio | 0.09 | |
| Clearance Time (s) | 6.5 | |
| Vehicle Extension (s) | 3.0 | |
| Lane Grp Cap (vph) | 144 | |
| v/s Ratio Prot | 0.03 | |
| v/s Ratio Perm | | |
| v/c Ratio | 0.34 | |
| Uniform Delay, d1 | 34.0 | |
| Progression Factor | 1.00 | |
| Incremental Delay, d2 | 1.4 | |
| Delay (s) | 35.4 | |
| Level of Service | D | |
| Approach Delay (s) | | |
| Approach LOS | | |
| Intersection Summary | | |
| intersection outfindly | | |

APPENDIX F

PEAK HOUR SIGNAL WARRANT ANALYSIS

Page 4C-9

California MUTCD (FHWA's MUTCD 2003 including Revisions 1 and 2, as amended for use in California)

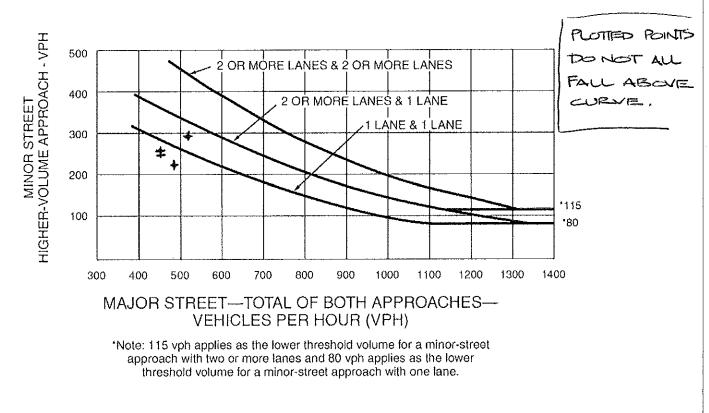
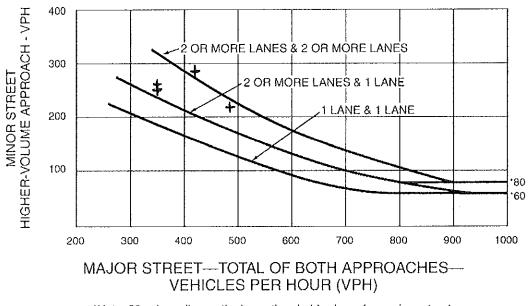


Figure 4C-1. Warrant 2, Four-Hour Vehicular Volume

Figure 4C-2. Warrant 2, Four-Hour Vehicular Volume (70% Factor)

(COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 70 64 km/h OR ABOVE 40 mph ON MAJOR STREET)



*Note: 80 vph applies as the lower threshold volume for a minor-street approach with two or more lanes and 60 vph applies as the lower threshold volume for a minor-street approach with one lane.

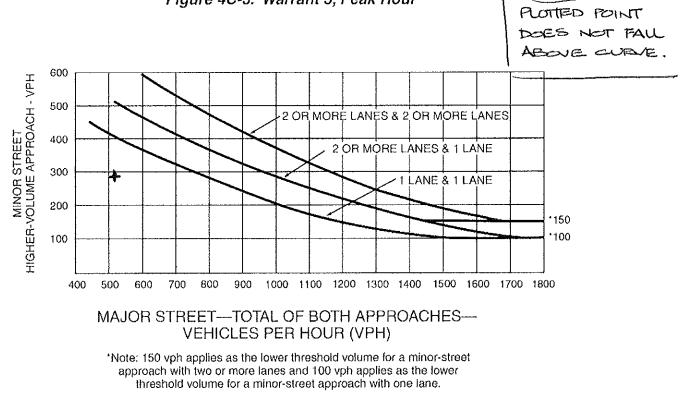
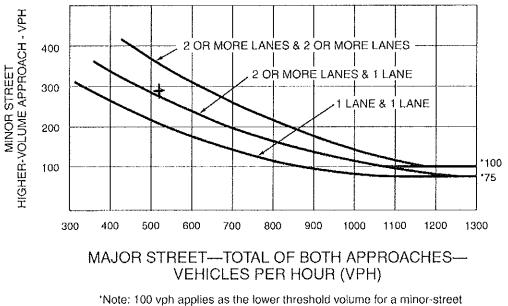


Figure 4C-3. Warrant 3, Peak Hour

Figure 4C-4. Warrant 3, Peak Hour (70% Factor)

(COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 70 64 km/h OR ABOVE 40 mph ON MAJOR STREET)



Note: 100 vph applies as the lower threshold volume for a minor-stree approach with two or more lanes and 75 vph applies as the lower threshold volume for a minor-street approach with one lane.

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 1 of 4)

| | ······································ | <u>01</u> 52.5 RTE PM | 2 | | GEPT, 2009 (ES DATE 1/25/11 DATE | | |
|---|--|--|----------------------------|--|--|--|--|
| | Major St: <u>MAIN</u> Minor St: <u>HWY IC</u> | | MPS | Critical Approach Spe Critical Approach Spe | | | |
| | | . , | | • 64 km/h (40 mph) or population | RURAL (R) | | |
| NO B. HOR CONTS | WARRANT 1 - Eig (Condition A or Co | | | e SATI n of A and B must be s | SFIED YES 🗌 NO 🖾 atisfied) | | |
| Cants | Condition A - Mini | mum Vehicle | e Volume | 100% SAT | | | |
| | | | QUIREMENTS IN BRACKETS) | 80% SAT | ISFIED YES 🗌 NO 🗌 | | |
| | | U R | UR | | , , , , , , | | |
| | APPROACH LANES | 1 | 2 or More | | Hour | | |
| | Both Approaches Major Street | 500 350 (400) (280) | 600 420 (480) (336) | | | | |
| | Highest Approach Minor Street | 160 105 (120) (84) | 200 140 (160) (112) | | | | |
| | Condition B - Inte | rruption of C | ontinuous Ti | | | | |
| | | | QUIREMENTS IN BRACKETS) | 80% SAT | ISFIED YES 🗌 NO 🗌 | | |
| | | UR | UR | | | | |
| | APPROACH LANES | 1 | 2 or More | | Hour | | |
| | Both Approaches Major Street | 750 525 (600) (420) | 900 630 (720) (504) | | | | |
| | Highest Approach Minor Street | 75 53 (60) (42) | 100 70 (80) (56) | | | | |
| | Combination of C | onditions A & | ЪВ | SAT | SFIED YES 🗌 NO 🗌 | | |
| | REQUIREMENT | | CONDIT | ION 🗸 | FULFILLED | | |
| | TWO CONDITION SATISFIED 80% | s | IM VEHICULAR | VOLUME | Yes 🗌 No 🗔 | | |
| | SATISFIED 00% | 1, | RUPTION OF CO | NTINUOUS TRAFFIC | | | |
| | AND, AN ADEQUA CAUSE LESS DEI TO SOLVE THE T | LAY AND INCON | IVENIENCE TO | ATIVES THAT COULD TRAFFIC HAS FAILED | Yes 🗌 No 🗍 | | |
| The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic contro | | | | | | | |

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 2 of 4)

ø

| | D* YES 🗌 | NO 🖾 |
|---|----------------------|----------------|
| Record hourly vehicular volumes for any four hours of an average day. | | |
| APPROACH LANES One More | ur | |
| Both Approaches - Major Street X 468 509 454 452 | | |
| Higher Approach - Minor Street X 213 299 246 264 | | |
| *All plotted points fall above the applicable curve in Figure 4C-1. (URBAN AREAS) | Yes 🗆 | No 🛛 |
| <u>QR</u> , All plotted points fall above the applicable curve in Figure 4C-2. (RURAL AREAS) | Yes 🗆 | No 🗌 |
| WARRANT 3 - Peak Hour SATISFIED (Part A or Part B must be satisfied) |) YES 🗌 | NO 🕅 |
| PART A SATISFIED (All parts 1, 2, and 3 below must be satisfied for the same one hour, for any four consecutive 15-minute periods) SATISFIED |) YES 🗌 | NO 🖾 |
| The total delay experienced by traffic on one minor street approach (one direction on controlled by a STOP sign equals or exceeds four vehicle-hours for a one-lane approach, or five vehicle-hours for a two-lane approach; <u>AND</u> | ^{Iy)} Yes □ | No 🕱 |
| The volume on the same minor street approach (one direction only) equals or exceed 100 vph for one moving lane of traffic or 150 vph for two moving lanes; <u>AND</u> | ds Yes 🖾 | No 🗌 |
| The total entering volume serviced during the hour equals or exceeds 800 vph for intersections with four or more approaches or 650 vph for intersections with three approaches. | Yes 🖾 | No 🗍 |
| PART B SATISFIED |) YES 🗌 | NO 🖾 |
| | | |
| Both Approaches - Major Street X 501 | | |
| Higher Approach - Minor Street X 299 | | |
| The plotted point falls above the applicable curve in Figure 4C-3. (URBAN AREAS) | Yes 🗌 | No 🗖 |
| OR, The plotted point falls above the applicable curve in Figure 4C-4. (RURAL AREAS | S) Yes 🗆 | No 🔲 |
| The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation | n of a traffic co | ontrol signal. |

"RURAL"

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California MUTCD (FHWA's MUTCD 2003 including Revisions 1 and 2, as amended for use in California)

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 2 of 4)

| | SATISFIED* | YES 🖾 | NO 🗆 |
|--|-----------------------------|-------|------|
| Record hourly vehicular volumes for any four hours of an average day. | an di | | |
| Record hourly vehicular volumes for any four hours of an average day. | B Cit Hour | | |
| Both Approaches - Major Street X 488 509 454 | | | |
| Higher Approach - Minor Street X 243 299-246 | 264 | | |
| *All plotted points fall above the applicable curve in Figure 4C-1. (URBAN | AREAS) | Yes 🗌 | No 🗌 |
| QR, All plotted points fall above the applicable curve in Figure 4C-2. (RUF | RAL AREAS) | Yes 📉 | No 🗌 |
| WARRANT 3 - Peak Hour S (Part A or Part B must be satisfied) | ATISFIED | YES 🛛 | NO 🗆 |
| · · | SATISFIED | YES 🗌 | NO 🛛 |
| The total delay experienced by traffic on one minor street approach (one controlled by a STOP sign equals or exceeds four vehicle-hours for a on approach, or five vehicle-hours for a two-lane approach; <u>AND</u> | direction only) e-lane | Yes 🗌 | No 🖾 |
| The volume on the same minor street approach (one direction only) equally 100 vph for one moving lane of traffic or 150 vph for two moving lanes; <u>A</u> | als or exceeds <u>ND</u> | Yes 🛛 | No 🗌 |
| The total entering volume serviced during the hour equals or exceeds 80 for intersections with four or more approaches or 650 vph for intersection | 10 vph ns with | Yes 🛛 | No 🗍 |
| three approaches. | | L | |
| three approaches. | SATISFIED | YES 🗌 | № 🗆 |
| three approaches. | SATISFIED | YES 🗌 | NO 🗌 |
| 2 or ACT Hours | SATISFIED | YES 🗌 | NO 🗌 |
| Three approaches. | SATISFIED | YES 🗌 | NO 🗌 |
| PART B 2 or APPROACH LANES One Both Approaches - Major Street X | | YES 🗌 | NO 🗌 |

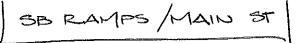
| | Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 3 of 4) | | | | | | | |
|--|--|--------------------------------------|---------------|-----------------------|----------------|---|-----------------|--------------|
| | NO OBSERVED | | | | | | | |
| | | edestrian Volum Aust Be Satisfied | | ED. TR | NFFIC | SATISFIED | YES 🗌 | NO 🖾 |
| | Part A (Parts 1 Hours> | or 2 must be satisf | ied) | / / | / / | SATISFIED | YES 🗌 | NO 🗌 |
| 1. | Pedestrian V | olume | | | | iy hour ≥ 190 <u>R</u> any 4 hours ≥ 100 | Yes 🗋 Yes 🗖 | No 🗌 No 🗌 |
| | Adequate Cr | ossing Gaps | | | <u>AN</u> | <u>\D</u> < 60 gaps/hr | Yes 🗌 | No 🗌 |
| 2. | Pedestrian V | olume | | Any hour | <u>></u> 95 | ····· | Yes 🗌 | No 🗌 |
| | | | | And the second second | hours ≥ 50 | | Yes 🗌 | |
| | | | | | | ed < 1.2m/s (4 ft/sec) | | |
| | | | | <u>AND</u> < 60 | gaps/hr | | Yes 🗌 | No 🗌 |
| | Part B | | | | | SATISFIED | YES 🗌 | NO 🗌 |
| | AND, The dista than 90 m (300 | ance to the nearest tra) ft) | affic signal | along the m | ajor street i | is greater | Yes 🗌 | No 🗌 |
| | OR, The propo | sed traffic signal will n | ot restrict p | rogressive t | affic flow al | ong the major street | . Yes 🔲 | No 🗌 |
| | | | | | | · · · · · · · · · · · · · · · · · · · | | <u></u> |
| | | chool Crossing Aust Be Satisfied | ۰ · | to scho Sross | | SATISFIED | YES 🗌 | NO 🕱 |
| | art A ap/Minutes and | # of Children | | | Hour | SATISFIED | YES 🗌 | NO 🗌 |
| | Gaps | Minutes Children Using | Crossing | | | | | |
| | vs Minutes | Number of Adequate | Gaps | | Gaps < | < Minutes | YES 🗌 | NO 🗌 |
| School Age Pedestrians Crossing Street / hr AND Children > 20/hr | | | | | | | YES 🗌 | NO 🗌 |
| | AND, Consideration has been given to less restrictive remedial measures. | | | | | | · · · · · · · · | |
| | AND, Conside | ration has been given | to less res | strictive rem | edial measi | ures. | Yes 🗌 | No 🗌 |
| Ра | <u>AND</u> , Conside | ration has been given | to less res | strictive rem | edial measu | SATISFIED | Yes YES | No 🗌 |
| Pa | art B | o the nearest traffic si | | | | SATISFIED | | |

The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

| All Parts Must Be | | ed Signal System ied) | UA1 | | | ES 🗌 NO 🛛 | |
|--|---|--|-------------------------------------|-----------------------|---------------|------------|--|
| MINIMUM REQUIREI | MENTS | DISTANCE TO NEA | REST SIGNAL | | | | |
| ≥ 300 m (1000 f | :) | N ft, S ft, E | ft, W_ | ft | | Yes 🗌 No 🗍 | |
| traffic control signals vehicular platooning. | are so fa | et that has traffic predominantly in in apart that they do not provide the | ne necessary de | egree of | ent | Yes 🗌 No 🗍 | |
| OR. On a two-way sti degree of platooning provide a progressive | and the | acent traffic control signals do nol proposed and adjacent traffic cor on. | provide the ne trol signals will | cessary collective | ly | | |
| VARRANT 7 - Cra All Parts Must Be | | perience Warrant ied) | SAT | ISFIED | Y | ES 🗆 NO | |
| Adequate trial of alter reduce the crash freq | natives i uency. | with satisfactory observance and | enforcement ha | as failed to | 0 | Yes 🗌 No 🔀 | |
| REQUIREMENTS Number of crashes reported within a 12 month per susceptible to correction by a traffic signal, and invol- or damage exceeding the requirements for a reporta | | | | ivolving in | ijury ash. | Yes 🗌 No 🗌 | |
| 5 OR MORE | | | | | | | |
| REQUIREMENT | `S | CONDITIONS | | | | | |
| | | Warrant 1, Condition A - Minimum Vehicular Volume | | | | | |
| ONE CONDITIC SATISFIED 809 | | <u>OR</u> , Warrant 1, Condition B - Interruption of Continuous Traffi | | Yes 🗌 No 🔀 | | | |
| | | <u>OR</u> , Warrant 4, Pedestrian Volume Condition Ped Vol \geq 152 for any hour <u>OR</u> , Ped Vol \geq 80 for any 4 hours | | | | | |
| VARRANT 8 - Roa | adway Satisf | Network ied) | SAT | ISFIED | Y | ES 🗌 NO [| |
| MINIMUM VOLUME REQUIREMENTS | | ENTERING VOLUMES - ALL A | PPROACHES | | \checkmark | FULFILLED | |
| 1000 Veh/Hr | During and ha of War | Typical Weekday Peak Hour s 5-year projected traffic volume: rants 1, 2, and 3 during an avera | that meet one ge weekday. | veh/Hr or more | | Yes 🗌 No 🔀 | |
| | During | OR Each of Any 5 Hrs. of a Sat. or Sun Veh/Hr | | | | | |
| CHARACTERISTICS OF MAJOR ROUTES MAJOR ROUTE A ROUTE B | | | | | | | |
| Hwy. System Serving | as Princ | pipal Network for Through Traffic | | | | | |
| Rural or Suburban Highway C | utside O | f, Entering, or Traversing a City | | | | | |
| Appears as Major Ro | ute on a | n Official Plan | | | | | |
| | Any Major Route Characteristics Met, Both Streets | | | | | | |

The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

| | | ([*] . | | |
|---|--|------------------|---------------------------------------|--|
| RICK ENGINEERING COMPANY | 711 Tank Farm Road, Suite 110 San Luis Obispo, CA 93401 Tel: (805) 544-0707 Fax: (805) 544-2052 | | | 1/25/11 6128 |
| | : · · · · · · · · · · · · · · · · · · · | | Checked By | • |
| WARRANT Z: | | | | |
| 1- Terrau I | ZELAY = 299 VEH/12× 21.9 S | =c/veн = 6,54 | 18 <u>sec</u> = | 1.82 VEH HES |
| | 16 = 299 VEH./HR > 100 VP | | | |
| | | | | |
| 3, IOTAL | ENTERING VOLUME = 299 V | 'eh † 509 veh = | = BOB VEH | > GED VEH YES |
| · · · · · · · · · · · · · · · · · · · | | | | |
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California MUTCD (FHWA's MUTCD 2003 including Revisions 1 and 2, as amended for use in California)

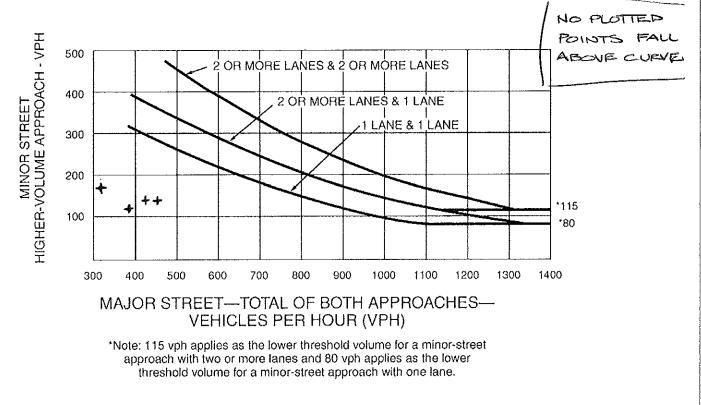
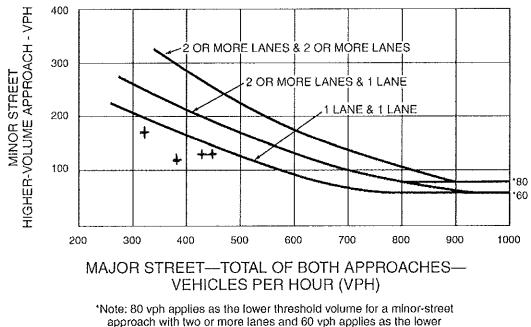




Figure 4C-2. Warrant 2, Four-Hour Vehicular Volume (70% Factor)

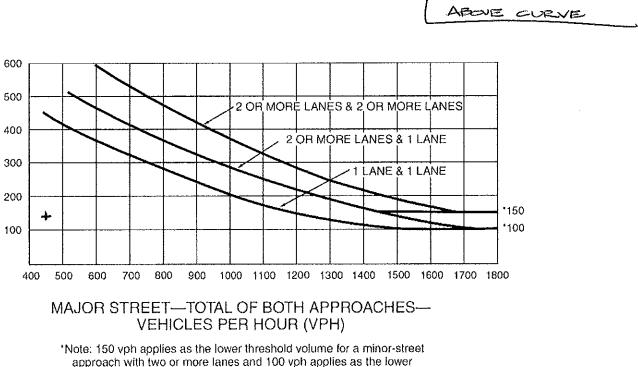
(COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 70 64 km/h OR ABOVE 40 mph ON MAJOR STREET)



threshold volume for a minor-street approach with one lane.

PLOTTED POINT NOT

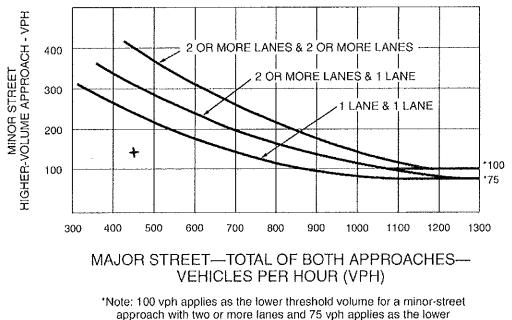
Figure 4C-3. Warrant 3, Peak Hour



threshold volume for a minor-street approach with one lane.

Figure 4C-4. Warrant 3, Peak Hour (70% Factor)

(COMMUNITY LESS THAN 10,000 POPULATION OR ABOVE 70 64 km/h OR ABOVE 40 mph ON MAJOR STREET)



threshold volume for a minor-street approach with one lane.

HIGHER-VOLUME APPROACH - VPH

MINOR STREET

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 1 of 4)

| | | RTE PM | 2 | САLС <u>. К. н</u> СНК | E SEPT, 2009 19465 DATE 1/25/11 DATE | | | |
|---------------------|---|------------------------|----------------------------|--|--|--|--|--|
| | Major St: <u>MAIN</u> Minor St: <u>HWY</u> . | | amps | Critical Approach \$ Critical Approach \$ | · | | | |
| | | | | opulation | Dr RURAL (R) URBAN (U) | | | |
| | WARRANT 1 - Eig (Condition A or C | | | n of A and B must be | ATISFIED YES 🗌 NO 🖾 e satisfied) | | | |
| | Condition A - Min | imum Vehicle | e Volume | 100% S/ | ATISFIED YES 🗌 NO 🗌 | | | |
| NO B-HOR COUNTS. | | | QUIREMENTS IN BRACKETS) | 80% S/ | ATISFIED YES 🗆 NO 🗔 | | | |
| | ~ | UR | UR | | | | | |
| | APPROACH LANES | 1 | 2 or More | | Hour | | | |
| | Both Approaches Major Street | 500 350 (400) (280) | 600 420 (480) (336) | | | | | |
| | Highest Approach Minor Street | 150 105 (120) (84) | 200 140 (160) (112) | | | | | |
| | Condition B - Inte | rruption of C | ontinuous Tr | | | | | |
| | | | QUIREMENTS IN BRACKETS) | 80% S <i>i</i> | ATISFIED YES 🗌 NO 🗌 | | | |
| | | UR | UR | | | | | |
| | APPROACH LANES | 1 | 2 or More | | Hour | | | |
| | Both Approaches Major Street | 750 525 (600) (420) | 900 630 (720) (504) | | | | | |
| | Highest Approach Minor Street | 75 53 (60) (42) | 100 70 (80) (56) | | | | | |
| | Combination of Conditions A & B SATISFIED YES INO | | | | | | | |
| | REQUIREMENT | | CONDIT | ION | ✓ FULFILLED | | | |
| | TWO CONDITION | IS | JM VEHICULAR | VOLUME | Yes No | | | |
| | SATISFIED 80% | 1 | | NTINUOUS TRAFFIC | | | | |
| | | LAY AND INCON | VENIENCE TO | ATIVES THAT COULD TRAFFIC HAS FAILED | Yes 🗌 No 🗍 | | | |

The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

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California MUTCD (FHWA's MUTCD 2003 including Revisions 1 and 2, as amended for use in California)

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 2 of 4)

| WARRANT 2 - Four Hour Vehicular Volume | SATISFIED* | YES 🗌 | NO 🛛 |
|--|--------------------------------|----------------|---------------|
| Record hourly vehicular volumes for any four hours of an average day. | | | |
| APPROACH LANES One More | K Hour | | |
| Both Approaches - Major Street X. 308 457 42 | | | |
| Higher Approach - Minor Street X 180 132 14 | | | |
| *All plotted points fall above the applicable curve in Figure 4C-1. (URBA | N AREAS) | Yes 🗌 | No 🗹 |
| <u>OR</u> , All plotted points fall above the applicable curve in Figure 4C-2. (R | URAL AREAS) | Yes 🗌 | No 🗌 |
| | | | |
| WARRANT 3 - Peak Hour (Part A or Part B must be satisfied) | SATISFIED | YES 🗌 | NO 🛛 |
| PARTA | SATISFIED | YES 🗌 | NO 🛛 |
| (All parts 1, 2, and 3 below must be satisfied for the same one hour, for any four consecutive 15-minute periods) | | | |
| The total delay experienced by traffic on one minor street approach (or controlled by a STOP sign equals or exceeds four vehicle-hours for a approach, or five vehicle-hours for a two-lane approach; <u>AND</u> | ne direction only) one-lane | Yes 🗆 | No 🗹 |
| The volume on the same minor street approach (one direction only) er 100 vph for one moving lane of traffic or 150 vph for two moving lanes | uals or exceeds | Yes 🔀 | No 🗆 |
| The total entering volume serviced during the hour equals or exceeds for intersections with four or more approaches or 650 vph for intersect three approaches. | 800 vph lons with | Yes 🗌 | No 🗹 |
| PART B | SATISFIED | YES 🗆 | |
| | | | |
| APPROACH LANES One More M Hour | | | |
| Both Approaches - Major Street X 457 | | | |
| Higher Approach - Minor Street X 132 | | | |
| The plotted point falls above the applicable curve in Figure 4C-3. (URB | AN AREAS) | Yes 🗆 | No 🛛 |
| OR, The plotted point falls above the applicable curve in Figure 4C-4. (I | RURAL AREAS) | Yes 🗌 | No 🗌 |
| The satisfaction of a traffic signal warrant or warrants shall not in itself require | the installation of | f a traffic co | ntrol signal. |

"RURAL"

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California MUTCD (FHWA's MUTCD 2003 including Revisions 1 and 2, as amended for use in California)

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 2 of 4)

| WARRANT 2 - Four Hour Vehicular | YES 🗌 | NO 🗷 | | |
|---|--|------------------------------------|----------------|--------------|
| Record hourly vehicular volumes for any fo | | | | |
| APPROACH LANES | our hours of an average day. 2 or One More | Hour | | |
| Both Approaches - Major Street | | -27 387 | | |
| Higher Approach - Minor Street | X 180 132 1 | 41 115 | | |
| *All plotted points fall above the applicabl | Yes 🗌 | No 🗌 | | |
| <u>QR</u> , All plotted points fall above the applie | cable curve in Figure 4C-2. (| RURAL AREAS) | Yes 🗌 | No 🖾 |
| WARRANT 3 - Peak Hour (Part A or Part B must be satisfied) | | SATISFIED | YES 🗌 | NO 🗌 |
| PART A (All parts 1, 2, and 3 below must be satistic one hour, for any four consecutive 15- | | SATISFIED | YES 🗌 | NO 🗌 |
| The total delay experienced by traffic or controlled by a STOP sign equals or ex approach, or five vehicle-hours for a tw | ceeds four vehicle-hours for | (one direction only) a one-lane | Yes 🗖 | No 🔀 |
| The volume on the same minor street a 100 vph for one moving lane of traffic or | Yes 🗷 | No 🗌 | | |
| The total entering volume serviced duri for intersections with four or more appro three approaches. | Yes 🗌 | No 🕅 | | |
| PART B | <i>A</i> | SATISFIED | YES 🗌 | NO 🖾 |
| APPROACH LANES | 2 or 59 Hour | | | |
| Both Approaches - Major Street | X 457 | | | |
| Higher Approach - Minor Street | × 132 | | | |
| The plotted point falls above the applicab | Yes 🗌 | No 🗌 | | |
| OR, The plotted point falls above the app | licable curve in Figure 4C-4. | (RURAL AREAS) | Yes 🗖 | No 🔀 |
| The satisfaction of a traffic signal warrant or wa | arrants shall not in itself requ | ire the installation of | f a traffic co | ntrol signal |

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| Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 3 of 4) | | | | | | | | | |
|--|---|------------------------------------|-------------------|--------------|------------------------------------|---------------|---------------------------------|-------------------|----------------------|
| | | edestrian Volu /lust Be Satisfi | me/ | | ERNET | | SATISFIED | YES 🗋 | NO 🕅 |
| l | Part A (Parts 1 Hours> | l or 2 must be sat | isfied) | | | | SATISFIED | YES 🗌 | |
| 1. | Pedestrian V | olume | | | | | hour ≥ 190 any 4 hours ≥ 100 | Yes ∐ Yes □ | No 📙 No 🔲 |
| | Adequate Cro | ossing Gaps | | | | AND |) < 60 gaps/hr | Yes 🗌 | No 🗖 |
| 2. | Pedestrian V | olume | | <u>OR</u> Ar | our ≥ 95 ny 4 hou ned crossi | | d < 1.2m/s (4 îl/sec) | Yes Yes Yes | No 🗌 No 🗌 No 🗌 |
| | 1 | | | AND · | < 60 gap | s/hr | | Yes 🗌 | No 🗌 |
| l | Part B | | | | | | SATISFIED | YES 🗌 | |
| | AND. The dista than 90 m (300 | ance to the neares 0 ft) | t traffic signal | along th | e major | street is | greater | Yes 🗆 | No 🔲 |
| | <u>OR</u> , The propo | sed traffic signal wi | ll not restrict p | rogressi | ve traffic | flow alor | ng the major street | Yes 🗆 | No 🗌 |
| • | | . <u></u> . | | | | | | | |
| WA (Pa | RRANT 5 - S rts A and B M | chool Crossin Aust Be Satisfi | <u>Mi</u> | SCH 2058 | 2002 | \mathcal{S} | SATISFIED | YES 🗌 | NO 🕅 |
| | art A p/Minutes and | # of Children | | | Н | / our | SATISFIED | YES 🗌 | NO 🗌 |
| | Gaps | Minutes Children U | sing Crossing | | | | | | |
| | vs Minutes | Number of Adeq | uate Gaps | | | Saps < I | Minutes | YES 🗌 | NO 🗌 |
| School Age Pedestrians Crossing Street / hr AND Children > 20/hr | | | | | | | | | NO 🗌 |
| AND, Consideration has been given to less restrictive remedial measures. | | | | | | | | Yes 🗆 | No 🗌 |
| Pa | irt B | | | | | | SATISFIED | YES 🗌 | |
| | The distance to than 90 m (300 | o the nearest traffic O ft) | signal along | the maj | or street | is greate | ər | Yes 🗆 | No 🗖 |
| l | OR, The proposed signal will not restrict the progressive movement of traffic. Yes I No I | | | | | | | | |

The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

YES 🗌 NO 🖾

Figure 4C-101 (CA). Traffic Signal Warrants Worksheet (Sheet 4 of 4)

| 10 SIGNALS | IN VICINITY |
|------------|-------------|
|------------|-------------|

WARRANT 6 - Coordinated Signal System ______ (All Parts Must Be Satisfied)

| MINIMUM REQUIREMENTS | | DISTANCE TO NEAREST SIGNAL | | | | | |
|--|-----------|----------------------------|---------------|---------------|-------|------------|--|
| ≥ 300 m (1000 ft) | N | ft, S | ft, E | ft, W | ft | Yes 🗌 No 🗌 | |
| On a one-way street or a stree traffic control signals are so far vehicular platooning. <u>OR</u> , On a two-way street, adjac degree of platooning and the p provide a progressive operation | apart tha | t they do not | provide the n | ecessary degr | ee of | Yes 🗌 No 🗍 | |

WARRANT 7 - Crash Experience Warrant (All Parts Must Be Satisfied)

SATISFIED YES 🗌 NO 🖾

SATISFIED

| Adequate trial of alternatives reduce the crash frequency. | Yes 🗌 No 🔀 | | |
|--|--|------------|--|
| REQUIREMENTS | Yes 🗌 No 🗍 | | |
| 5 OR MORE | | | |
| REQUIREMENTS | CONDITIONS | \vee | |
| | Warrant 1, Condition A - Minimum Vehicular Volume | | |
| ONE CONDITION SATISFIED 80% | OR, Warrant 1, Condition B - Interruption of Continuous Traffic | Yes 🗌 No 🛛 | |
| | <u>OR</u> , Warrant 4. Pedestrian Volume Condition Ped Vol \geq 152 for any hour <u>OR</u> , Ped Vol \geq 80 for any 4 hours | | |

WARRANT 8 - Roadway Network (All Parts Must Be Satisfied)

SATISFIED YES 🗌 NO 🖾

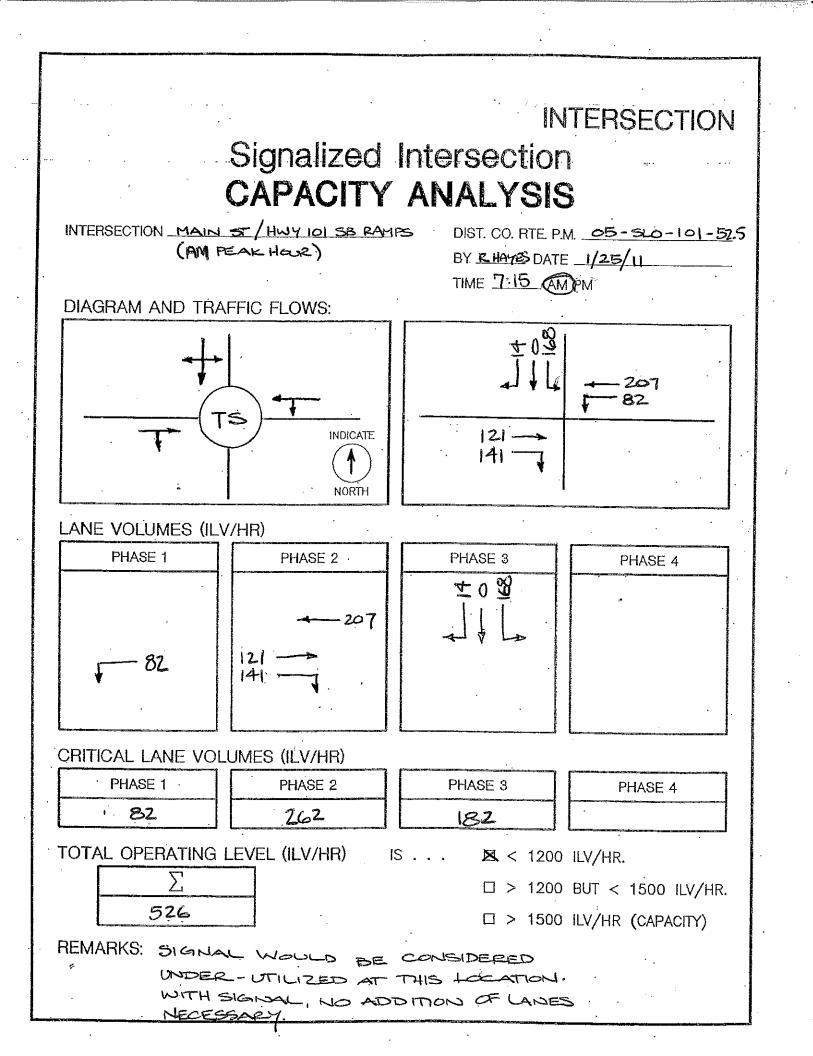
| MINIMUM VOLUME REQUIREMENTS | ENTERING VOLUMES - ALL APF | \checkmark | FULFILLED | | |
|--------------------------------|---|------------------|---------------|--|------------|
| 1000 Veh/Hr | During Typical Weekday Peak Hour Veh/Hr and has 5-year projected traffic volumes that meet one or more of Warrants 1, 2, and 3 during an average weekday. | | | | Yes 🗍 No 🔀 |
| | OR During Each of Any 5 Hrs. of a Sat. or Sur | | | | |
| CHARACT | ERISTICS OF MAJOR ROUTES | MAJOR ROUTE A | MAJO ROUTE | | |
| Hwy. System Serving | |] | | | |
| Rural or Suburban Highway C | | | | | |
| Appears as Major Ro | | | | | |
| A | Yes 🗌 No 🗌 | | | | |

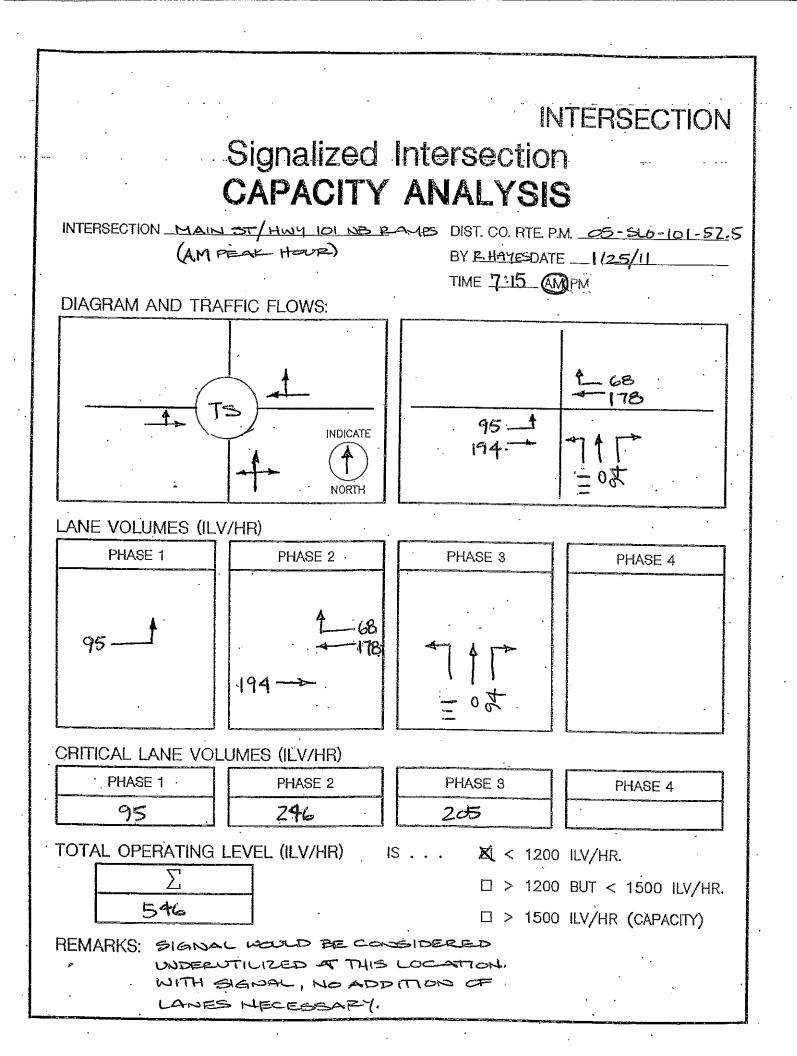
The satisfaction of a traffic signal warrant or warrants shall not in itself require the installation of a traffic control signal.

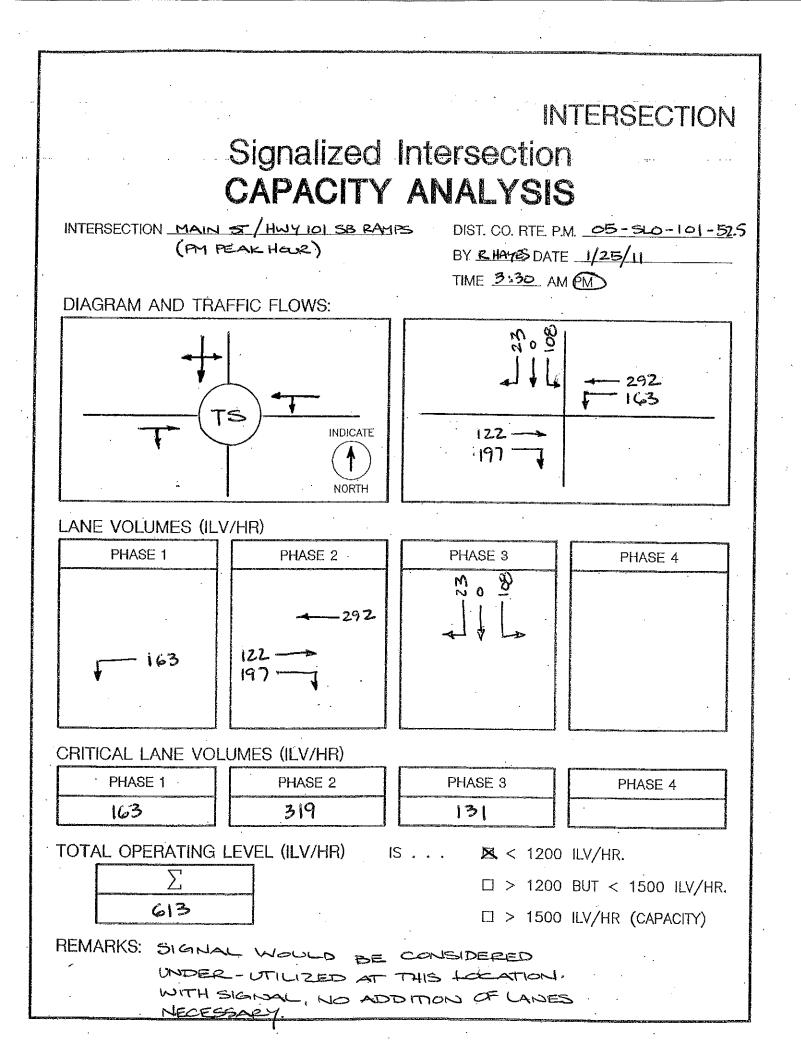
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| RICK ^{sar} | l Tank Fa n Luis Ol | oispo, (| CA 934 | | | | | | | J | Date ob No. | | 1/2 612 | <u>-5/11</u> -8 | | | |
| ENGINEERING COMPANY Tel: (805) 544-0707 Fax: (805) 544-2052 | | | | | | | | | | E | Page Done By Checked B | | R.HAYES | | | | |
| WARRANT Z: | · ····· · | | | | • | | | | | | | | | | | | |
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| I. CAAL JEL | -~7 | · • • • | ••• | 725-7 | /VEH | ידי ' | VEH | /не | | 1002 | . CECAHZ | | | VEH | MR | -74 | |
| 2. MINGE ST. | vou | 51 | e > | 14 | VEA | 1/HR | > 10 | OUF | =+1/+ | 1P- | YES | - | | : | | | |
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| 3. TOTAL ENT | ERIN | SG | VO | しいて | 15. 3 | 589 | VE | н Х | 69 | D VE | 4. <u>i</u> | 40 | | | | | |
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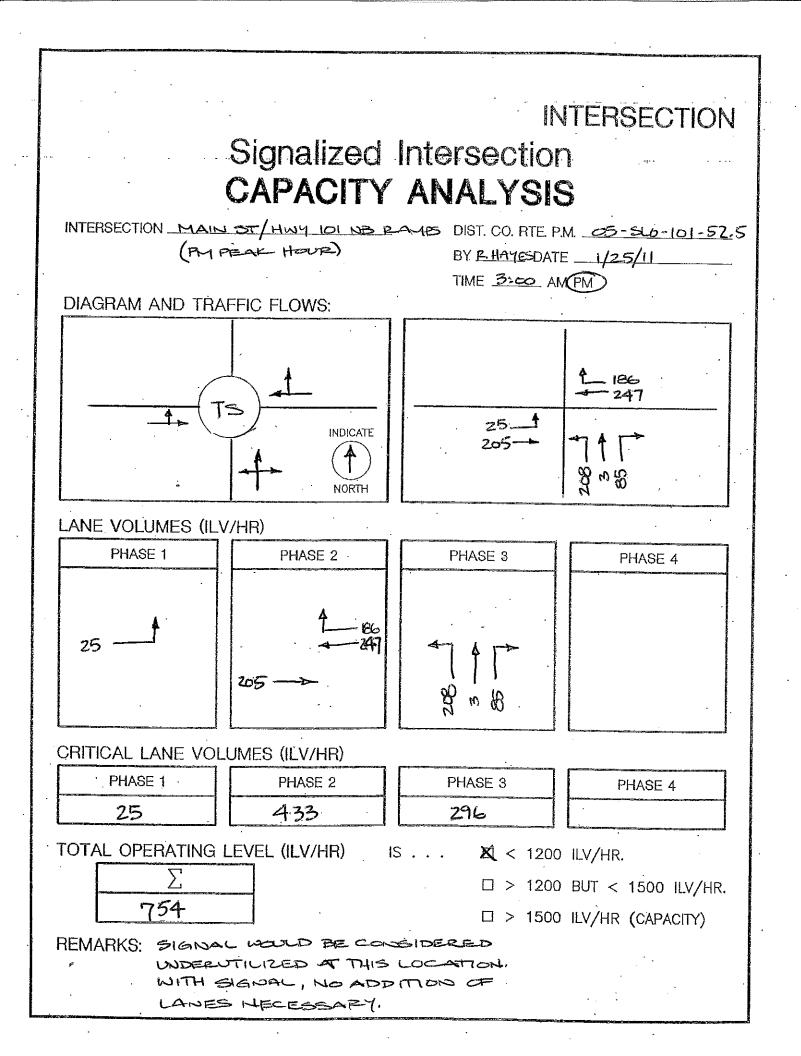
APPENDIX G

SIGNALIZED INTERSECTION CAPACITY ANALYSIS (ILV)









APPENDIX H

QUEUING ANALYSIS: EXISTING CONDITIONS

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 51 | 53 | 120 |
| Average Queue (ft) | 5 | 8 | 65 |
| 95th Queue (ft) | 29 | 34 | 112 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | 0 | |
| Queuing Penalty (veh) | | 0 | |

Intersection: 2: Main St. & SB 101 Offramp

| EB | WB | SB | SB |
|----|--------------------|---|--|
| TR | LT | LT | R |
| 14 | 79 | 118 | 30 |
| 2 | 31 | 62 | 12 |
| 8 | 66 | 102 | 36 |
| 41 | 333 | 600 | |
| | | | |
| | | | |
| | | | 50 |
| | | 13 | |
| | | 2 | |
| | TR 14 2 8 | TR LT 14 79 2 31 8 66 | TR LT LT 14 79 118 2 31 62 8 66 102 41 333 600 |

| | | | NID | ND |
|-----------------------|-----|----|-----|----|
| Movement | EB | WB | NB | NB |
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 221 | 25 | 153 | 75 |
| Average Queue (ft) | 24 | 5 | 48 | 50 |
| 95th Queue (ft) | 113 | 21 | 98 | 78 |
| Link Distance (ft) | 333 | 25 | 780 | |
| Upstream Blk Time (%) | | 0 | | |
| Queuing Penalty (veh) | | 1 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 5 | 5 |
| Queuing Penalty (veh) | | | 5 | 6 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 55 | 31 | 50 | 69 |
| Average Queue (ft) | 26 | 4 | 21 | 31 |
| 95th Queue (ft) | 55 | 20 | 46 | 62 |
| Link Distance (ft) | 25 | 622 | 675 | |
| Upstream Blk Time (%) | 7 | | | |
| Queuing Penalty (veh) | 20 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 0 | 1 |
| Queuing Penalty (veh) | | | 0 | 1 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 30 | 28 | 135 |
| Average Queue (ft) | 4 | 6 | 64 |
| 95th Queue (ft) | 20 | 24 | 103 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 43 | 123 | 93 | 75 |
| Average Queue (ft) | 9 | 49 | 48 | 25 |
| 95th Queue (ft) | 32 | 108 | 78 | 69 |
| Link Distance (ft) | 43 | 333 | 697 | |
| Upstream Blk Time (%) | 0 | | | |
| Queuing Penalty (veh) | 1 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 13 | 2 |
| Queuing Penalty (veh) | | | 3 | 2 |

| | | | ND | |
|-----------------------|-----|----|-----|----|
| Movement | EB | WB | NB | NB |
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 60 | 33 | 115 | 75 |
| Average Queue (ft) | 26 | 12 | 63 | 42 |
| 95th Queue (ft) | 56 | 34 | 99 | 75 |
| Link Distance (ft) | 333 | 26 | 828 | |
| Upstream Blk Time (%) | | 0 | | |
| Queuing Penalty (veh) | | 2 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 11 | 4 |
| Queuing Penalty (veh) | | | 10 | 8 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 32 | 26 | 108 | 75 |
| Average Queue (ft) | 29 | 5 | 44 | 55 |
| 95th Queue (ft) | 42 | 21 | 92 | 88 |
| Link Distance (ft) | 26 | 863 | 649 | |
| Upstream Blk Time (%) | 8 | | | |
| Queuing Penalty (veh) | 22 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 4 | 12 |
| Queuing Penalty (veh) | | | 7 | 9 |

Zone Summary

APPENDIX I

QUEUING ANALYSIS: NEAR-TERM MITIGATION MEASURES

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 28 | 28 | 157 |
| Average Queue (ft) | 2 | 6 | 68 |
| 95th Queue (ft) | 14 | 24 | 116 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 1 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | EB | WB | NB | NB |
|-----------------------|-----|----|-----|----|
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 42 | 51 | 76 | 74 |
| Average Queue (ft) | 37 | 32 | 52 | 35 |
| 95th Queue (ft) | 50 | 49 | 73 | 62 |
| Link Distance (ft) | 333 | 25 | 801 | |
| Upstream Blk Time (%) | | 14 | | |
| Queuing Penalty (veh) | | 60 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 4 | 0 |
| Queuing Penalty (veh) | | | 4 | 0 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 31 | 367 | 739 | 75 |
| Average Queue (ft) | 24 | 106 | 477 | 75 |
| 95th Queue (ft) | 44 | 271 | 711 | 75 |
| Link Distance (ft) | 25 | 800 | 732 | |
| Upstream Blk Time (%) | 3 | | 1 | |
| Queuing Penalty (veh) | 9 | | 0 | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 18 | 94 |
| Queuing Penalty (veh) | | | 29 | 76 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 29 | 28 | 135 |
| Average Queue (ft) | 2 | 6 | 70 |
| 95th Queue (ft) | 14 | 24 | 117 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| | 50 | | <u> </u> | 00 |
|-----------------------|----|-----|----------|----|
| Movement | EB | WB | SB | SB |
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 57 | 140 | 52 | 69 |
| Average Queue (ft) | 41 | 66 | 35 | 22 |
| 95th Queue (ft) | 57 | 110 | 52 | 60 |
| Link Distance (ft) | 40 | 333 | 570 | |
| Upstream Blk Time (%) | 6 | | | |
| Queuing Penalty (veh) | 20 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 1 | 0 |
| Queuing Penalty (veh) | | | 0 | 1 |

| Movement | EB | WB | NB | NB |
|-----------------------|-----|----|-----|----|
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 37 | 34 | 174 | 75 |
| Average Queue (ft) | 19 | 6 | 60 | 43 |
| 95th Queue (ft) | 42 | 25 | 114 | 76 |
| Link Distance (ft) | 333 | 26 | 796 | |
| Upstream Blk Time (%) | | 0 | | |
| Queuing Penalty (veh) | | 1 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 10 | 3 |
| Queuing Penalty (veh) | | | 9 | 6 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 32 | 27 | 86 | 75 |
| Average Queue (ft) | 27 | 8 | 39 | 55 |
| 95th Queue (ft) | 44 | 26 | 69 | 87 |
| Link Distance (ft) | 26 | 663 | 644 | |
| Upstream Blk Time (%) | 6 | | | |
| Queuing Penalty (veh) | 17 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 2 | 12 |
| Queuing Penalty (veh) | | | 3 | 10 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 29 | 28 | 135 |
| Average Queue (ft) | 2 | 6 | 73 |
| 95th Queue (ft) | 14 | 24 | 122 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | ГР | | CD | CD |
|-----------------------|----|-----|-----|----|
| Movement | EB | WB | SB | SB |
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 57 | 117 | 52 | 68 |
| Average Queue (ft) | 38 | 55 | 34 | 22 |
| 95th Queue (ft) | 56 | 99 | 51 | 60 |
| Link Distance (ft) | 40 | 333 | 625 | |
| Upstream Blk Time (%) | 6 | | | |
| Queuing Penalty (veh) | 19 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 1 | 1 |
| Queuing Penalty (veh) | | | 0 | 1 |

| | = 5 | | | NID |
|-----------------------|-----|----|-----|-----|
| Movement | EB | WB | NB | NB |
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 42 | 51 | 94 | 75 |
| Average Queue (ft) | 26 | 34 | 53 | 34 |
| 95th Queue (ft) | 44 | 50 | 80 | 61 |
| Link Distance (ft) | 333 | 25 | 767 | |
| Upstream Blk Time (%) | | 14 | | |
| Queuing Penalty (veh) | | 63 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 5 | 0 |
| Queuing Penalty (veh) | | | 4 | 0 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 31 | 412 | 738 | 75 |
| Average Queue (ft) | 20 | 123 | 397 | 72 |
| 95th Queue (ft) | 44 | 329 | 697 | 82 |
| Link Distance (ft) | 25 | 691 | 725 | |
| Upstream Blk Time (%) | 2 | | 3 | |
| Queuing Penalty (veh) | 6 | | 0 | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 8 | 90 |
| Queuing Penalty (veh) | | | 12 | 73 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 29 | 30 | 157 |
| Average Queue (ft) | 4 | 6 | 65 |
| 95th Queue (ft) | 20 | 25 | 111 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | 0 | |
| Queuing Penalty (veh) | | 0 | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 15 | 106 | 93 | 69 |
| Average Queue (ft) | 3 | 47 | 46 | 22 |
| 95th Queue (ft) | 10 | 102 | 75 | 60 |
| Link Distance (ft) | 41 | 333 | 663 | |
| Upstream Blk Time (%) | | | | |
| Queuing Penalty (veh) | | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 11 | 1 |
| Queuing Penalty (veh) | | | 3 | 2 |

| | | | NID | ND |
|-----------------------|-----|----|-----|----|
| Movement | EB | WB | NB | NB |
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 124 | 36 | 138 | 75 |
| Average Queue (ft) | 57 | 33 | 79 | 43 |
| 95th Queue (ft) | 97 | 40 | 120 | 84 |
| Link Distance (ft) | 333 | 26 | 808 | |
| Upstream Blk Time (%) | | 11 | | |
| Queuing Penalty (veh) | | 47 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 20 | 2 |
| Queuing Penalty (veh) | | | 17 | 4 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 31 | 76 | 221 | 75 |
| Average Queue (ft) | 29 | 30 | 79 | 62 |
| 95th Queue (ft) | 41 | 73 | 179 | 89 |
| Link Distance (ft) | 26 | 533 | 831 | |
| Upstream Blk Time (%) | 5 | | | |
| Queuing Penalty (veh) | 15 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 4 | 26 |
| Queuing Penalty (veh) | | | 7 | 21 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 29 | 29 | 135 |
| Average Queue (ft) | 2 | 6 | 66 |
| 95th Queue (ft) | 14 | 24 | 105 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| | | | ~~ | |
|-----------------------|----|-----|-----|----|
| Movement | EB | WB | SB | SB |
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 57 | 204 | 93 | 75 |
| Average Queue (ft) | 28 | 101 | 55 | 24 |
| 95th Queue (ft) | 54 | 181 | 93 | 71 |
| Link Distance (ft) | 40 | 333 | 578 | |
| Upstream Blk Time (%) | 1 | | | |
| Queuing Penalty (veh) | 5 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 13 | 0 |
| Queuing Penalty (veh) | | | 3 | 0 |

| Movement | EB | WB | NB | NB |
|-----------------------|-----|----|-----|----|
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 59 | 25 | 73 | 73 |
| Average Queue (ft) | 23 | 4 | 55 | 37 |
| 95th Queue (ft) | 53 | 19 | 74 | 65 |
| Link Distance (ft) | 333 | 25 | 910 | |
| Upstream Blk Time (%) | | 0 | | |
| Queuing Penalty (veh) | | 1 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 8 | 1 |
| Queuing Penalty (veh) | | | 7 | 2 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 32 | 30 | 131 | 75 |
| Average Queue (ft) | 29 | 7 | 55 | 54 |
| 95th Queue (ft) | 42 | 25 | 115 | 89 |
| Link Distance (ft) | 25 | 724 | 805 | |
| Upstream Blk Time (%) | 7 | | | |
| Queuing Penalty (veh) | 19 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 4 | 11 |
| Queuing Penalty (veh) | | | 6 | 9 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 30 | 28 | 135 |
| Average Queue (ft) | 4 | 6 | 70 |
| 95th Queue (ft) | 20 | 24 | 114 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 0 | | |
| Queuing Penalty (veh) | 0 | | |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | | |
| Queuing Penalty (veh) | | | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 58 | 167 | 93 | 75 |
| Average Queue (ft) | 36 | 83 | 56 | 19 |
| 95th Queue (ft) | 65 | 144 | 93 | 63 |
| Link Distance (ft) | 41 | 333 | 598 | |
| Upstream Blk Time (%) | 4 | | | |
| Queuing Penalty (veh) | 14 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 19 | 0 |
| Queuing Penalty (veh) | | | 4 | 0 |

| | == | | | |
|-----------------------|-----|----|-----|----|
| Movement | EB | WB | NB | NB |
| Directions Served | LT | TR | LT | R |
| Maximum Queue (ft) | 85 | 51 | 202 | 75 |
| Average Queue (ft) | 50 | 31 | 112 | 53 |
| 95th Queue (ft) | 92 | 47 | 178 | 91 |
| Link Distance (ft) | 333 | 26 | 848 | |
| Upstream Blk Time (%) | | 7 | | |
| Queuing Penalty (veh) | | 28 | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 39 | 3 |
| Queuing Penalty (veh) | | | 33 | 6 |

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | LT | TR | L | R |
| Maximum Queue (ft) | 32 | 65 | 177 | 75 |
| Average Queue (ft) | 29 | 21 | 77 | 62 |
| 95th Queue (ft) | 42 | 53 | 173 | 91 |
| Link Distance (ft) | 26 | 791 | 763 | |
| Upstream Blk Time (%) | 6 | | | |
| Queuing Penalty (veh) | 16 | | | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 10 | 24 |
| Queuing Penalty (veh) | | | 15 | 19 |

Zone Summary

| Movement | EB | WB | NB | SB |
|-----------------------|-----|-----|----|-----|
| Directions Served | LTR | LTR | R | LTR |
| Maximum Queue (ft) | 49 | 73 | 68 | 342 |
| Average Queue (ft) | 10 | 42 | 10 | 211 |
| 95th Queue (ft) | 39 | 72 | 46 | 324 |
| Link Distance (ft) | 4 | 43 | | 443 |
| Upstream Blk Time (%) | 9 | 14 | | |
| Queuing Penalty (veh) | 0 | 44 | | |
| Storage Bay Dist (ft) | | | 50 | |
| Storage Blk Time (%) | | | 1 | |
| Queuing Penalty (veh) | | | 0 | |

Intersection: 2: Main St. & SB 101 Offramp

| FR | W/R | SB | SB |
|----|---------------------------|---|---|
| LD | VVD | 30 | 30 |
| TR | LT | LT | R |
| 73 | 342 | 157 | 75 |
| 38 | 287 | 73 | 29 |
| 77 | 393 | 143 | 75 |
| 43 | 335 | 585 | |
| 3 | 5 | | |
| 11 | 22 | | |
| | | | 50 |
| | | 19 | 8 |
| | | 4 | 8 |
| | 73 38 77 43 3 | TR LT 73 342 38 287 77 393 43 335 3 5 | TR LT LT 73 342 157 38 287 73 77 393 143 43 335 585 3 5 11 22 19 19 |

Intersection: 3: Main St. & Ramada Dr.

| Movement | EB | WB | NB | NB | SW | SW |
|-----------------------|---|-----|-----|-----|-------------------------------|-----|
| wovernent | ED | VVB | ND | ND | 310 | 311 |
| Directions Served | <lt< td=""><td>TR></td><td>LT</td><td>R></td><td><l< td=""><td>R></td></l<></td></lt<> | TR> | LT | R> | <l< td=""><td>R></td></l<> | R> |
| Maximum Queue (ft) | 224 | 289 | 523 | 75 | 475 | 75 |
| Average Queue (ft) | 155 | 203 | 306 | 42 | 244 | 69 |
| 95th Queue (ft) | 232 | 295 | 508 | 100 | 472 | 88 |
| Link Distance (ft) | 335 | 794 | 818 | | 572 | |
| Upstream Blk Time (%) | | | | | | |
| Queuing Penalty (veh) | | | | | | |
| Storage Bay Dist (ft) | | | | 50 | | 50 |
| Storage Blk Time (%) | | | 68 | 17 | 49 | 45 |
| Queuing Penalty (veh) | | | 58 | 36 | 76 | 37 |

Zone Summary

| Movement | EB | NB | SB |
|-----------------------|-----|----|-----|
| Directions Served | LTR | R | LTR |
| Maximum Queue (ft) | 30 | 56 | 456 |
| Average Queue (ft) | 5 | 9 | 171 |
| 95th Queue (ft) | 22 | 37 | 370 |
| Link Distance (ft) | 4 | | 443 |
| Upstream Blk Time (%) | 2 | | 1 |
| Queuing Penalty (veh) | 0 | | 0 |
| Storage Bay Dist (ft) | | 50 | |
| Storage Blk Time (%) | | 3 | |
| Queuing Penalty (veh) | | 0 | |

Intersection: 2: Main St. & SB 101 Offramp

| Movement | EB | WB | SB | SB |
|-----------------------|----|-----|-----|----|
| Directions Served | TR | LT | LT | R |
| Maximum Queue (ft) | 58 | 256 | 224 | 74 |
| Average Queue (ft) | 38 | 145 | 108 | 14 |
| 95th Queue (ft) | 66 | 277 | 210 | 56 |
| Link Distance (ft) | 40 | 335 | 172 | |
| Upstream Blk Time (%) | 25 | | 6 | |
| Queuing Penalty (veh) | 80 | | 0 | |
| Storage Bay Dist (ft) | | | | 50 |
| Storage Blk Time (%) | | | 47 | 0 |
| Queuing Penalty (veh) | | | 11 | 0 |

Intersection: 3: Main St. & Ramada Dr.

| | ГD | | ND | ND | CW | CIM |
|-----------------------|---|------|-----|----|-------------------------------|-----|
| Movement | EB | WB | NB | NB | SW | SW |
| Directions Served | <lt< td=""><td>TR></td><td>LT</td><td>R></td><td><l< td=""><td>R></td></l<></td></lt<> | TR> | LT | R> | <l< td=""><td>R></td></l<> | R> |
| Maximum Queue (ft) | 352 | 437 | 226 | 75 | 241 | 75 |
| Average Queue (ft) | 267 | 204 | 152 | 62 | 84 | 63 |
| 95th Queue (ft) | 401 | 371 | 237 | 98 | 188 | 89 |
| Link Distance (ft) | 335 | 1092 | 879 | | 761 | |
| Upstream Blk Time (%) | 5 | | | | | |
| Queuing Penalty (veh) | 12 | | | | | |
| Storage Bay Dist (ft) | | | | 50 | | 50 |
| Storage Blk Time (%) | | | 56 | 19 | 18 | 26 |
| Queuing Penalty (veh) | | | 47 | 41 | 29 | 21 |

Zone Summary

APPENDIX J

TRAFFIC SPEED SURVEYS

| SAN LUK | S OBIS | SPO (| cou | ΝТΥ | | | | F | N 1. | | ь 13 | r= r | | | | | | | | — — | | | | | | | | 69A1-Ramada | | |
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